

Vehicle Weights and Dimensions Study

Volume 16

**A Comparison of Various Computer
Simulation Models for Predicting the
Lateral Behaviour of Articulated Buses**

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The Technical Steering Committee will be considering the findings of these research investigations in preparing its "Final Technical Report" (Volume 1 & 2), scheduled for completion in December 1986.

PREFACE

The report which follows constitutes one volume in a series of sixteen which have been produced by contract researchers involved in the Vehicle Weights and Dimensions Study. The research procedures and findings contained herein address one or more specific technical objectives in the context of the development of a consistent knowledge base necessary to achieve the overall goal of the Study; improved uniformity in interprovincial weight and dimension regulations.

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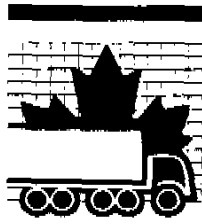
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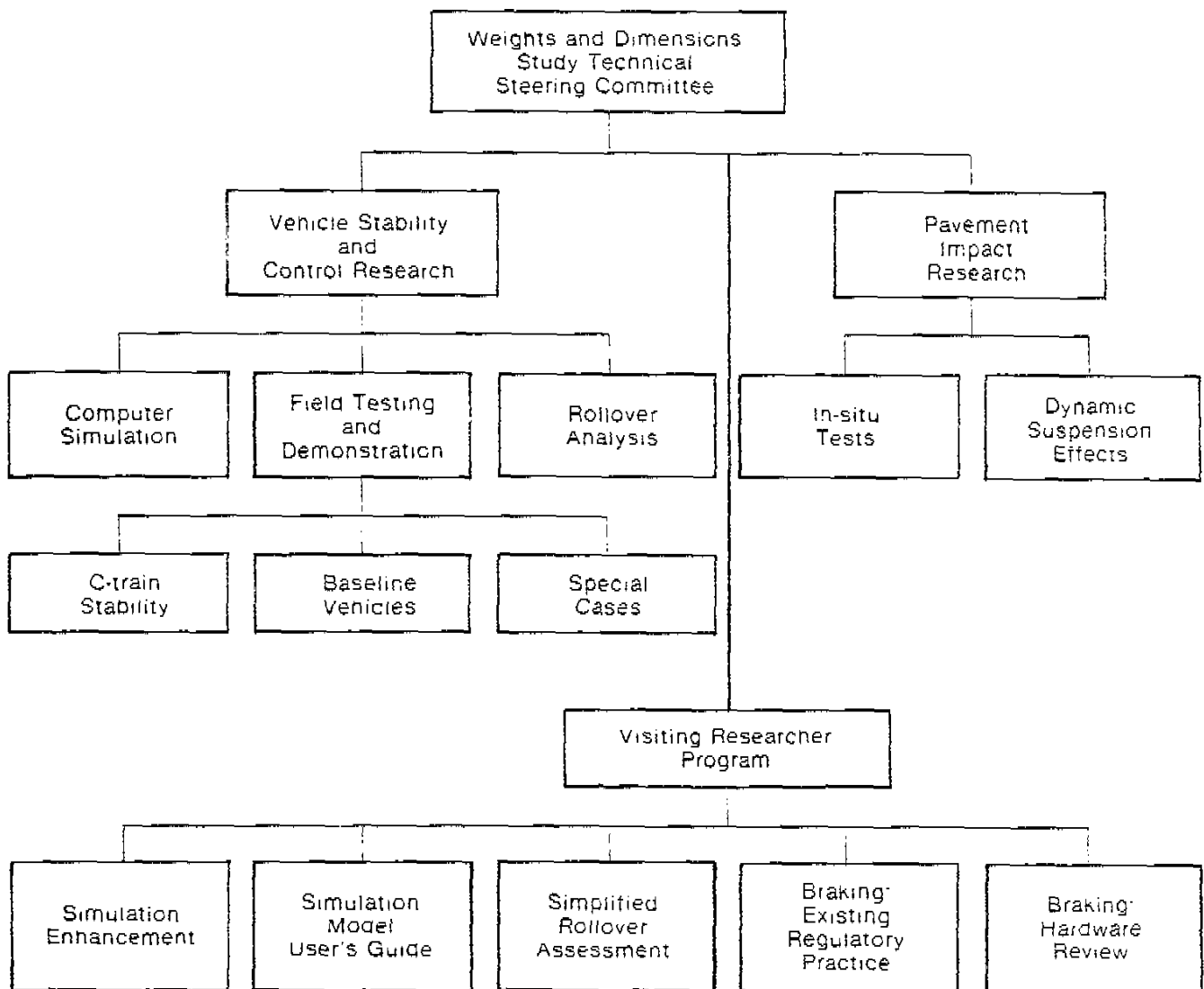
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HEAVY VEHICLE WEIGHTS AND DIMENSIONS STUDY

TECHNICAL WORK ELEMENTS OVERVIEW



Volume 16

**A Comparison of Various Computer Simulation Models for Predicting
the Lateral Dynamic Behaviour of Articulated Vehicles**

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FOREWORD

The work described in this report was performed under the Visiting Researcher Program (Computer Simulation Models) of the RTAC/CCMTA Vehicle Weights and Dimensions Study. This report, together with a previous report entitled "Computer Simulation of Heavy Vehicle Dynamic Behaviour - User's Guide to the UMTRI Models", by J.Y. Wong and M. El-Gindy, June 1985, forms the final Report to RTAC/CCMTA.

The study described in this report was performed by Dr. J.Y. Wong, Director, and Dr. M. El-Gindy, Senior Research Associate, Transport Technology Research Laboratory, Carleton University, Ottawa, Canada.

The guidance provided by the Project Manager and the Technical Steering Committee of the Vehicle Weights and Dimensions Study, and the assistance given by the staff members of the Engineering Research Division, University of Michigan Transportation Research Institute (UMTRI) during the course of the study are appreciated.

April 1986

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SUMMARY

The objective of this study is to compare the capabilities and limitations of various simulation models for the evaluation of the directional behaviour of commercial articulated vehicles. The steady-state steering response and the lateral dynamic behaviour in lane-change (obstacle avoidance) manoeuvres of six articulated vehicles with different design features have been predicted using the Phase 4 model, the yaw/roll model, the TBS model, and the linear yaw plane model, developed by the University of Michigan Transportation Research Institute (UMTRI). A comparison of the predictions made by these models has been performed. These predictions have also been compared with a limited amount of experimental data available. In addition, the static roll model developed by UMTRI has been examined, and a parametric sensitivity study has been performed.

It is believed that the results of this study provide additional quantitative information upon which the appropriate areas of application of various simulation models may be defined.

INTRODUCTION

With the increasing use of commercial articulated vehicles, such as tractor-semitrailers and truck-full trailers, in road transport, concerns for their safety in operation have been growing. This has stimulated intensive studies of the dynamic stability of this type of vehicle.

A variety of analytical (simulation) models for predicting the lateral dynamic behaviour of commercial articulated vehicles have been developed in recent years. These models vary greatly in capability, in complexity, in the number of degrees of freedom considered, and in the amount of input data required. For instance, the Phase 4 model developed by the University of Michigan Transportation Research Institute (UMTRI) incorporates up to 71 degrees of freedom and requires up to approximately 2300 lines of input data, dependent upon the vehicle configuration (1)(2). On the other hand, the linear yaw plane model developed also by UMTRI only includes the lateral and yaw motion of the tractor and articulation in the horizontal plane of the other sprung masses of the articulated vehicle, and only requires up to approximately 35 lines of input data. It should also be mentioned that not only a large amount of input data is required for a sophisticated model, but also special measuring equipment is needed to obtain a number of these input parameters. Quite often, even if the equipment is available, the cost of obtaining the required parameters will be considerable.

When a practising engineer wishes to evaluate the lateral dynamic behaviour of a vehicle, he will undoubtedly be faced with the problem of

how to select an appropriate model for a given task. A recent survey has pointed out that while a wide range of simulation models are available, a systematic evaluation of these models, particularly with respect to their areas of application, has been lacking (3). To fill this gap and to provide guidance for the practising engineer to select an appropriate model for a particular task, a detailed comparison of some of the more widely known simulation models, including the linear yaw plane model, the TBS model, the yaw/roll model, and the Phase 4 model developed at UMTRI has been performed.

The steady-state steering response and the lateral dynamic behaviour in lane-change (obstacle avoidance) type manoeuvres of six commercial articulated vehicles with different design features have been predicted using the four UMTRI computer simulation models. A comparison of the predictions made using these models and with a limited amount of experimental data available has been made. In addition, the static roll model developed by UMTRI has been examined, and a parametric sensitivity study has been performed.

The objective of this study is to compare the capabilities and limitations of various simulation models for the evaluation of the directional behaviour of commercial articulated vehicles. The results of the study will provide quantitative information upon which the appropriate areas of application of various models may be defined.

1. A BRIEF DESCRIPTION OF THE VARIOUS SIMULATION MODELS USED IN THE STUDY

A brief description of the basic features of the five simulation models used in the study, namely, the linear yaw plane model, the TBS model, the yaw/roll model, the Phase 4 model, and the static roll model developed at UMTRI, is given below (1)(2)(4).

1.1 The Linear Yaw Plane Model

The yaw plane model is a linear mathematical model for studying the directional behaviour of multiple articulated vehicles. The model was developed in 1978, originally for the purpose of analyzing the directional behaviour of double-bottom tankers.

Computer programs based on the model permit the evaluation of the following directional properties which are useful for studying a vehicle's directional stability and performance: (1) natural frequency and damping ratios of the natural modes of yaw motion (eigenvalues), (2) transient and steady-turning responses of each articulated unit of an articulated vehicle train, and (3) frequency response (by frequency response we mean the directional response of the vehicle to sinusoidal steer inputs).

At the present time, the computer programs permit the analysis of articulated vehicles which have up to three articulation points and a maximum of 11 axles. The computer codes can be easily expanded to the study of vehicles which have an even greater number of axles and articulation points.

In developing the equations of motion for the linear yaw plane model, the roll dynamics of the vehicle is neglected. Further, the vehicle is assumed to travel at a constant forward velocity. The degrees of freedom permitted in the model are therefore limited to lateral and yawing motion of the tractor and articulation in the horizontal plane of the other sprung masses of the multiple articulated vehicle.

The following are the assumptions made in the process of deriving the equations of motion:

- A. The cornering forces and aligning moments generated at the tire-road interface are assumed to be linear functions of the sideslip angle of the tire.
- B. Articulation angles made by the various elements of the vehicle train are small such that the following approximations hold:
 $\sin \Gamma_i \approx \Gamma_i$, $\cos \Gamma_i \approx 1$ (where Γ_i 's are the articulation angles).
- C. The motion of the vehicle takes place on a horizontal surface with uniform friction characteristics.
- D. There are no significant tire forces present in the longitudinal direction (either tractive or braking).
- E. Pitch and roll motions of the sprung masses are small and hence neglected.

- F. All joints are frictionless and articulation takes place about vertical axes.
- G. Steering system dynamics is not included in the model and the steering input is assumed to be given directly to the front wheels.
- H. In the case of tanker trains, the tanker compartments are assumed to be either completely full or completely empty, thereby avoiding sloshing of the liquid.
- I. Each element or unit of the articulated vehicle is assumed to be a rigid body (in the case of liquid filled tanks, all of the liquid is assumed to take part in the yawing motion, i.e., relative motion of the liquid with respect to the walls of the tank is neglected) and the unsprung masses are assumed to be rigidly attached to their respective sprung masses.

Due to the simple manner in which the vehicle is represented in the model, the input data required are moderate and computational costs are very low.

1.2 The TBS Model

This model is for predicting the directional response of commercial vehicles to steering inputs and/or braking (4). The simulation consists of two interactive computer programs, one for a straight truck and the other for a tractor-semitrailer. The model for the tractor-semitrailer has four degrees of freedom, namely, the longitudinal velocity, the lateral velocity, and the yaw velocity of the tractor, and the articulation angle of the semi-trailer relative to the tractor. There are no roll or pitch degrees of freedom. Load transfers, both longitudinal and lateral, are taken into consideration and are computed quasi-statically.

In this model, the hitch is assumed to transmit a yaw moment (but not a roll or pitch moment) through the friction in it. The hitch is modelled as a circular plate with a uniform pressure distribution, equal to the static load divided by the area of the plate. The coefficient of friction is assumed to be a constant. For "steel on steel", the value of the friction coefficient at the hitch is taken to be approximately 0.05.

The normal load on each wheel of the vehicle is equal to the sum of the static load and the load transfer (both longitudinal and lateral) taking place at any instant of time.

A simplified model for tandem axles is included. A quasi-static inter-axle load transfer is specified by entering an appropriate load transfer coefficient. The product of this coefficient and the braking force on one side of the tandem axles gives the inter-axle load transfer for that side.

For a free rolling tire, the model developed by Fiala is used to describe the relationship between lateral force and sideslip angle (4). For braking, two linear equations are used to describe the relationship between the braking effort coefficient and longitudinal slip, one for the range from zero to the peak value of the braking effort coefficient, and the other for the range from the peak value to the sliding value (100% skid) of the braking effort coefficient. For combined braking and cornering, an empirical equation is used to describe the functional relationships between the lateral and longitudinal forces and sideslip angle and longitudinal skid.

In the TBS model, antilock braking system can be accommodated. Dual tires are treated as two single tires, each sharing the vertical load on them equally and each yielding the same longitudinal and lateral forces.

Braking is handled in the model by specifying the time history of the attempted brake force for the brakes on either side of each axle. Since each side is considered separately, brake imbalance may be simulated. Steering inputs are entered in a tabular form. Each line of the table consists of the time followed by the average steer angle of the front wheels.

It should be mentioned that the model cannot handle the case when a wheel lifts off the ground. In other words, computations are stopped if this happens. Furthermore, if the articulation angle becomes larger than a user specified value, which may indicate "jackknifing" or "trailer swing", computations are also stopped.

1.3 The Yaw/Roll Model

The yaw/roll model was developed for the purpose of predicting the directional and roll response of single and multiple articulated vehicles engaged in steering manoeuvres which approach the rollover condition. It should be noted that the model does not permit the simulation of braking manoeuvres. The model is unique in the sense that it permits the analysis of unconventional vehicle layouts. The equations of motion are developed in such a fashion that it is possible to use the model for simulating vehicles with (1) any number of units and articulation points, (2) any number of placement of wheels and tires, and (3) any of the particular hitch mechanisms and constraints that are used in heavy-duty commercial vehicles.

In its present form, the computer code permits the simulation of vehicles with up to three articulation points (i.e., four sprung masses) and 11 axles. The computer program can be easily expanded to permit the analysis of vehicles with an even larger number of articulation points and axles.

In the model, the forward velocity of the lead unit is assumed to remain constant during the manoeuvre. Hence, each sprung mass is treated as a rigid body with five degrees of freedom: lateral, vertical, yaw, roll and pitch. The axles are treated as beam axles which are free to roll and bounce with respect to the sprung mass to which they are attached.

The following assumptions were made in the process of deriving the equations of motion:

- A. Only steering manoeuvres (in which the input is an angular displacement of the front wheels on the lead unit) are modelled.
- B. The vehicle moves over a horizontal surface possessing uniform frictional characteristics.
- C. The pitch motions of the sprung masses are small such that $\sin \theta_s = \theta_s$ and $\cos \theta_s = 1$.
- D. The relative roll displacements between the sprung masses and the axles remain small, such that $\sin(\phi_s - \phi_u) = \phi_s - \phi_u$ and $\cos(\phi_s - \phi_u) = 1$.
- E. The relative roll motion between the unsprung and sprung masses takes place about roll centres, R, which are located at fixed distances beneath the sprung masses (see Fig. 1.1).
- F. The line of action of the suspension springs remains parallel to the k_u axis (Fig. 1.1), with only compression and tensile forces being transmitted to the sprung mass. Figure 1.1 shows that the roll centre, R, is free to move in the k_u direction, such that any force on the axle in the j_u direction acts on the sprung mass at the roll centre, R. In the case of a suspension consisting of leaf springs, the springs are twisted (about a longitudinal axis) when the axle rolls relative to the sprung mass, with the resulting roll-resisting moment being treated as an auxiliary roll stiffness, KRS (see Fig. 1.1).

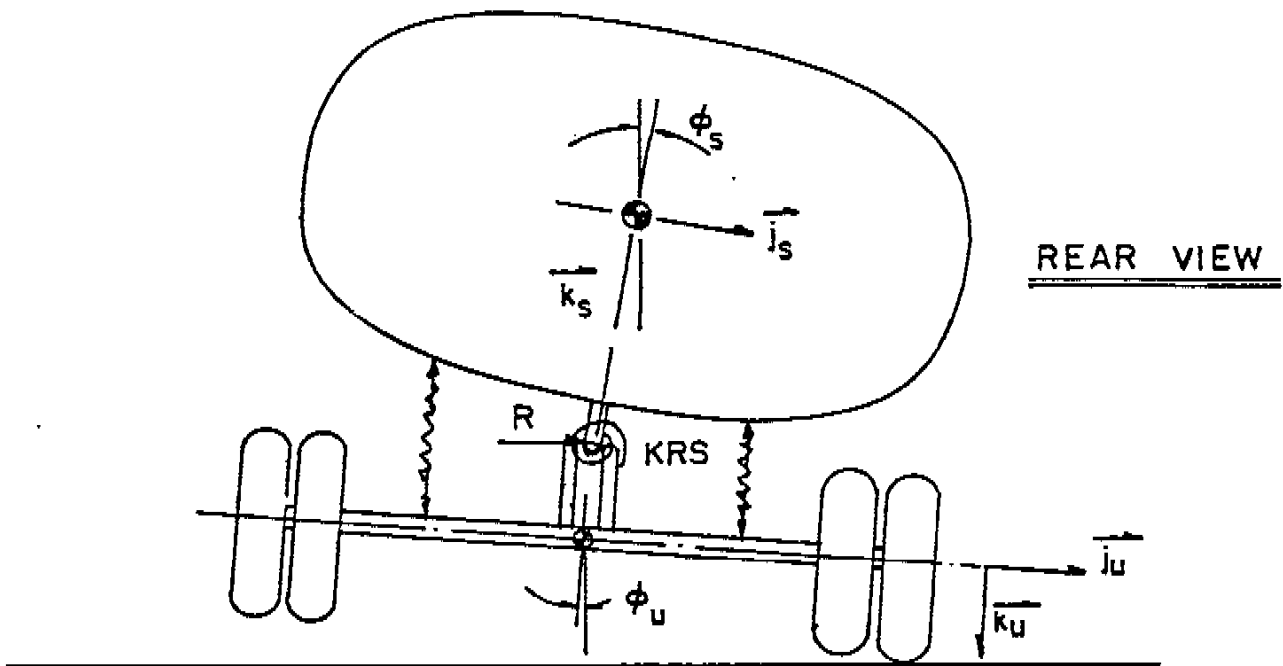


Figure 1.1 Idealized representation of axles and suspension springs

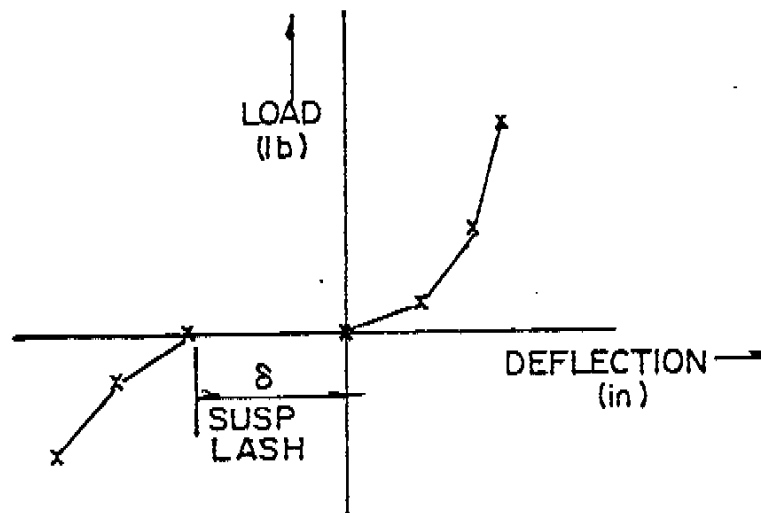


Figure 1.2 Idealized representation of suspension nonlinearities

- G. Nonlinearities in the force-displacement behaviour of a suspension, such as suspension lash, are approximated as shown in Figure 1.2.
- H. The forces acting on each axle are independent of the forces acting on adjacent axles, i.e., interaxle load transfers are neglected.
- I. The cornering force and aligning moment produced by a given tire is a nonlinear function depending only on sideslip angle and vertical load. The influence of wheel inclination (or camber) on lateral force generation has been neglected on the grounds that inclination angles remain small prior to wheels being lifted off the ground in a severe manoeuvre.
- J. The principal axes of inertia of the sprung and unsprung masses coincide with the respective body-fixed co-ordinate systems.

In its present form, the computer program permits the analysis of vehicles which are equipped with any of the four coupling mechanisms used in heavy-duty commercial vehicles, namely, the fifth wheel, inverted fifth wheel, kingpin, and pintle hook. Note that the "fifth wheel" and the "inverted fifth wheel" permit the lead and the trailing units to yaw and pitch with respect to one another, but are "stiff" in roll. On the other hand, the so-called "kingpin" connection permits only yaw motions between the lead and the trailing units. In the case of the "pintle hook", the trailing unit can roll, bounce, yaw, and pitch with respect to the lead unit.

1.4 The Phase 4 Model

This model was developed in 1980 for simulating the braking and steering dynamics of trucks, tractor-semitrailers, doubles, and triples combinations. The goal in developing this program was to consolidate principal features of all existing computer models into a single program. In short, the Phase 4 model represents UMTRI's latest thinking in computer modelling of the braking and steering response of commonly used commercial vehicles.

The Phase 4 program is a time-domain mathematical simulation of a truck/tractor, a semitrailer, and up to two full trailers. The motions of the vehicles are represented by differential equations derived from Newtonian mechanics, that are solved for successive time increments by digital integration.

The program is written in a generalized fashion to allow simulation of a large number of vehicle configurations. The first vehicle is the power unit and may be a truck or tractor, both of which may carry payload. As a single unit with no payload, it is equivalent to an empty truck or bobtail tractor. With payload, it is a truck, which, with a semitrailer simulates a car hauler, dromedary tractor, etc. The second unit is always a semitrailer (i.e., the current model does not include a truck with full trailer). The third and fourth units are full trailers consisting of semi-trailers on either a fixed or converter dolly. Separate payload may be specified for each trailer.

The mathematical model incorporates up to 71 degrees of freedom. The number of degrees of freedom are dependent on the vehicle configuration and derive from the following:

- Six degrees of freedom (three translational and three rotational) for the truck/tractor sprung mass
- Three degrees of freedom for the semitrailer (the three other degrees of freedom of the semitrailer are effectively eliminated by dynamic constraints at the hitch)
- Five degrees of freedom for each of the two full trailers allowed
- Two degrees of freedom (vertical and roll) for each of the 13 axles allowed
- A wheel rotational degree of freedom for each of the 26 wheels allowed

The motion of each of the sprung masses is determined from the summation of forces and moments arising from the tires (acting through the unsprung mass and suspension), gravity, and the hitch point constraints. Small roll and pitch angle assumptions are made in deriving equations so that the simulation can be validly applied only up to a manoeuvre limit at which vehicle roll-over occurs.

The Phase 4 model can be used to simulate the following vehicle configurations:

Straight truck, empty and loaded

Bobtail tractor

Tractor-semitrailer (3 to 5 axles), empty and loaded

Tractor-Semitrailer-full trailer (5 to 9 axles), empty and loaded

Tractor-semitrailer-full trailer-full trailer (7 to 13 axles),
empty and loaded.

For simulation of braking performance, the program incorporates state-of-the-art representation of truck air brake systems, antilock braking systems, and tire-road friction models. Typical examples of braking studies for which it can be, or has been used, are:

- A. Stopping distance performance
- B. Effects of brake timing
- C. Dynamic behaviour in braking
- D. Comparisons of antilock wheel control logic
- E. Influence of tire-road friction coupling
- F. Split friction surfaces
- G. Brake proportioning
- H. Tandem-axle effects on braking limits.

For simulation of cornering performance behaviour, the program incorporated state-of-the-art representations of truck tire lateral force

characteristics (with roll-off effects during combined braking), and vehicle suspension properties of significance to cornering behaviour. Typical examples of studies involving cornering are as follows:

- A. Understeer/oversteer properties of commercial vehicles
- B. Determining cornering limits
- C. Assessing tandem-axle effects on cornering
- D. Jackknife prediction
- E. Effects of suspension properties on cornering and cornering limits
- F. Accident simulation.

In addition to the above, the program can be operated open-loop (defined steer angle inputs) or closed-loop (defined path input), and on roads of specified grade or cross-slope.

The Phase 4 program is uniquely applicable in studies in which the influence of the following items are to be considered in detail:

- A. Spring force/deflection characteristics (hysteresis and free-play)
- B. Brake "fade" - brake temperature
- C. Brake hysteresis
- D. Load-leveler action in tandem suspensions
- E. Brake proportioning algorithms
- F. Steering system compliance (inputs at the steering wheel)
- G. Frame torsional stiffness.

1.5 The Static Roll Model

The static roll model was developed for the purpose of calculating the rollover threshold of articulated vehicles during steady turning manoeuvres. The dynamics of roll motion are not included in the model. Instead, the roll response in a steady turn is computed by repeatedly solving, for small increments of roll angle, a set of equations which describe the static equilibrium of the vehicle in the roll plane.

Figure 1.3 shows the side view of an example tractor-semitrailer as presented in the roll plane model. As shown in the Figure, axles with similar suspension properties are grouped together in such a fashion that all the axles on the vehicle are represented by a set of three composite axles. The composite axles are:

- 1) tractor front axle
- 2) tractor rear axle (either a single or tandem axles are combined and represented by one axle)
- 3) trailer axle (all the axles on the trailer are combined and represented by one axle).

The torsional compliance that exists in the tractor frame is represented by a torsional spring element, K_{FR} (Fig. 1.3). Similarly, the structural compliance in the body of the trailer and the fifth wheel arrangement are lumped together and represented by another torsional element, K_5 . The idealized representation of the friction (CFR) present

in the tractor frame and the separation of the fifth wheel plates (LASH5) are shown in Figures 1.4 and 1.5 respectively.

In the model, the relative motion between the sprung mass and the axles is assumed to take place about roll centres which are at fixed distances beneath the sprung masses. As shown in Figure 1.6, the suspension springs are assumed to remain parallel to the \vec{k}_{u_i} axes of the axles and transmit only compressive or tensile forces.

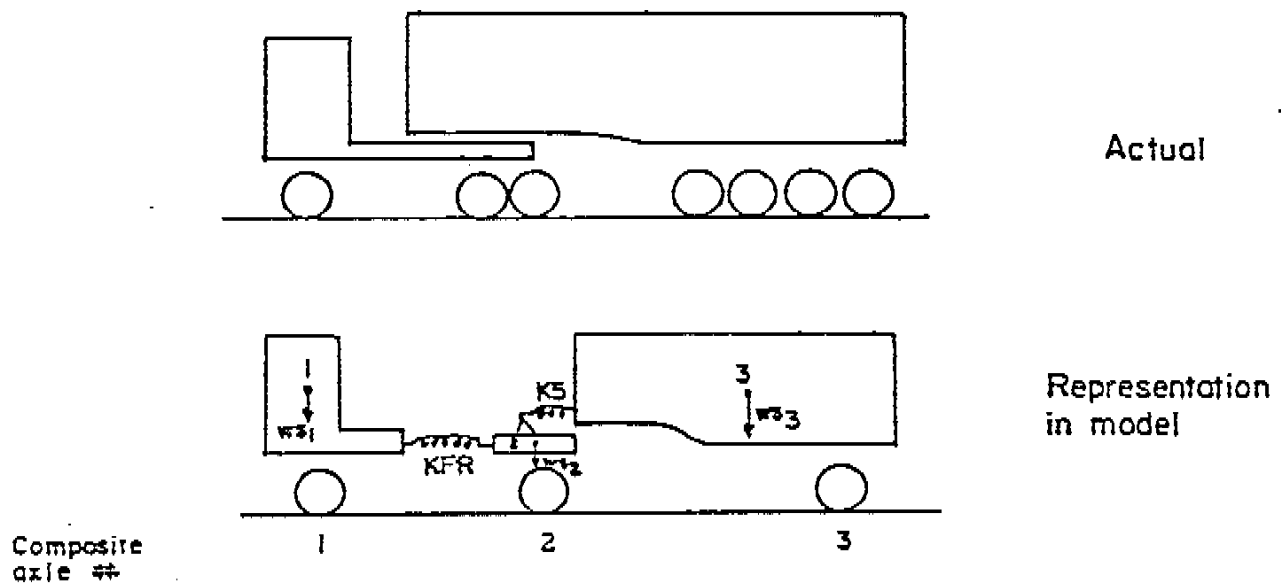


Figure 1.3 Side view of the representation of axles in the static roll model

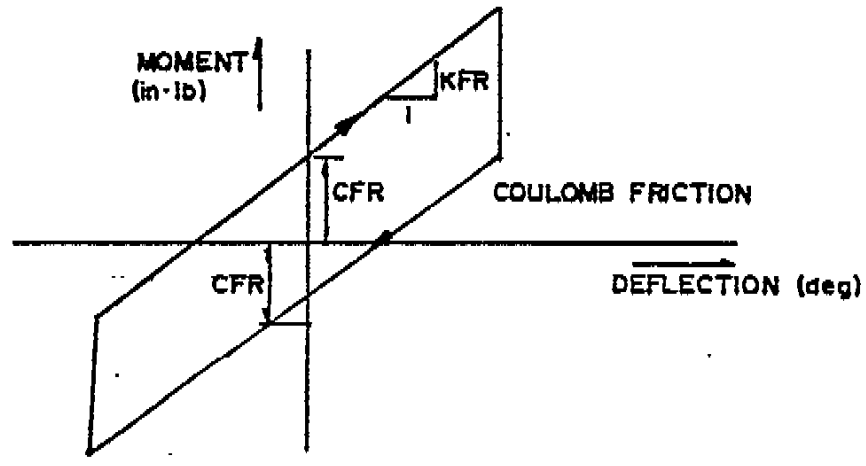


Figure 1.4 Idealized representation of tractor frame compliance

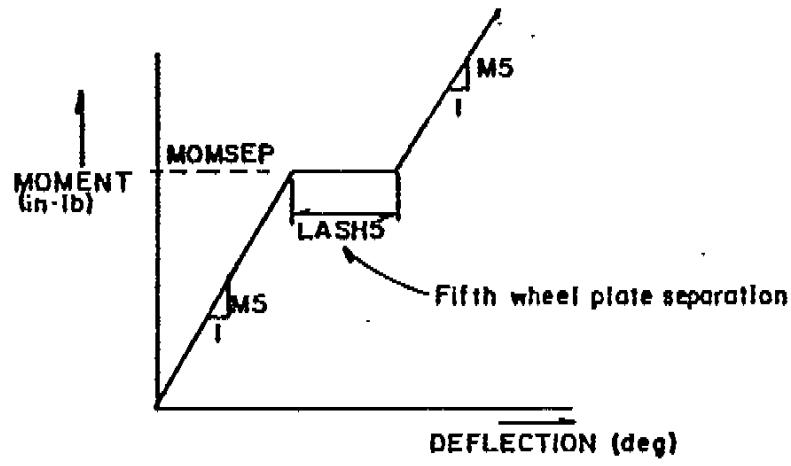
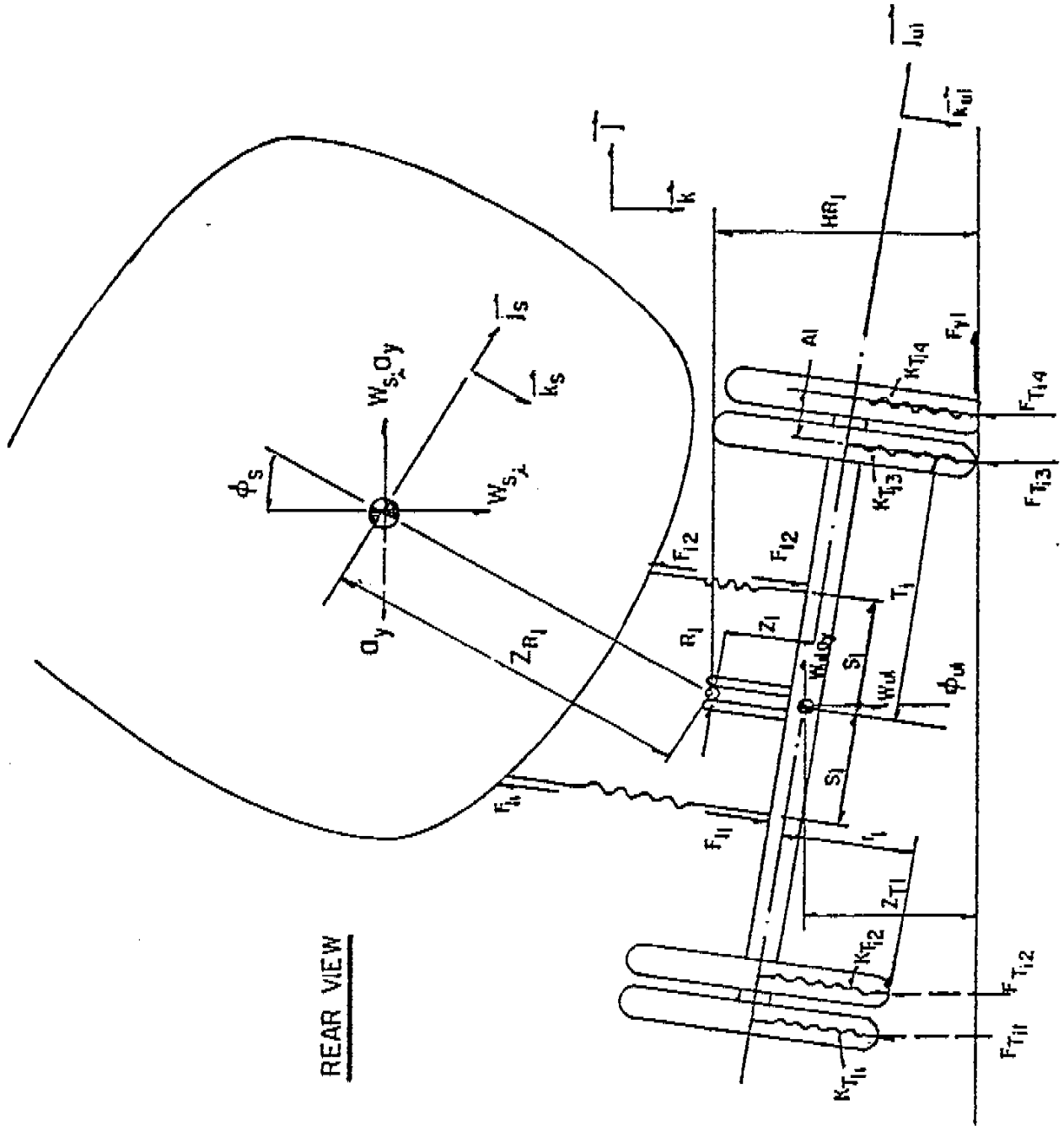


Figure 1.5 Idealized representation of fifth wheel compliance



REAR VIEW

Figure 1.6

The roll centres are permitted to slide freely (with respect to the axles) along the \vec{k}_{u_i} axes. All axle forces which act in a direction parallel to the \vec{k}_{u_i} axes are taken up by the suspension springs, while all axle forces acting along the \vec{j}_{u_i} axes are assumed to act through the roll centre, R_i .

Suspension nonlinearities such as backlash and progressively hardening suspension springs are presented by a tabular load-deflection input format. The suspension forces and local spring rates at any given deflection are then computed by linear interpolation. Figure 1.7 shows the representation of a suspension spring in the model.

The other simplifying assumptions implicit in the derivation of the equations are listed below.

- A. The roll angles of the sprung mass and the axles are small, such that the small angle assumptions $\sin(\phi) = \phi$ and $\cos(\phi) = 1.0$ hold.
- B. The articulation angles are small so that the influence of articulation angle on roll response can be neglected.
- C. The total vertical load carried by each composite axle is assumed to remain constant during the rollover process. In order to accommodate any pitching motion that might take place during rollover, the sprung masses are permitted to take up different vertical deflections at each of the three axle locations.

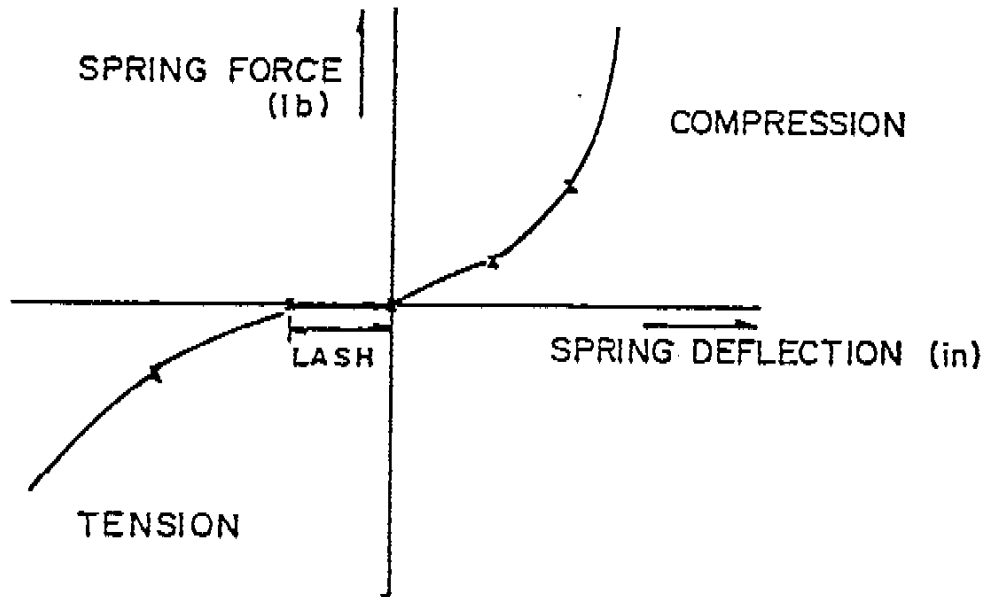


Figure 1.7 Idealized representation of suspension spring characteristics

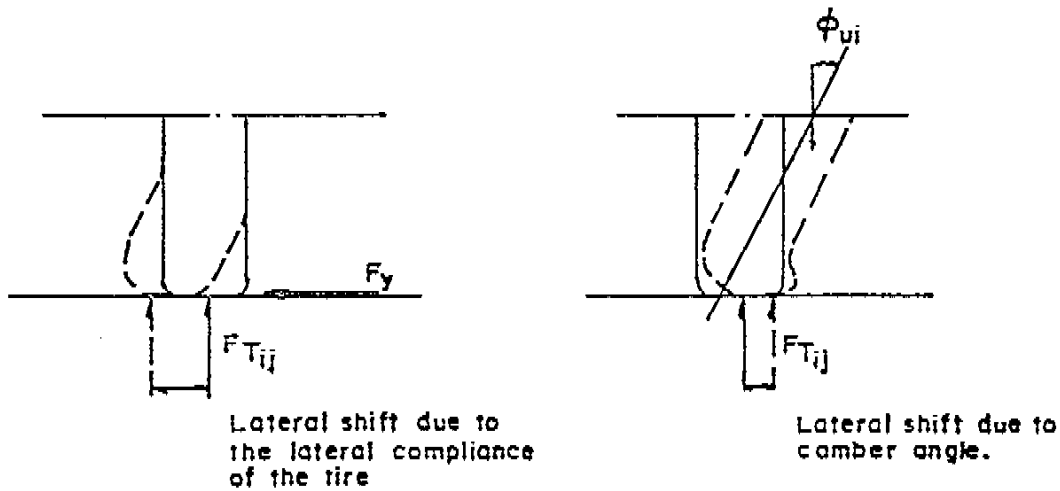


Figure 1.8 The effect of lateral compliance and camber angle on the centroid of the normal pressure distribution at the tire/road interface

D. The vertical load carried by each tire is assumed to act through the midpoint of its tread width. As shown in Figure 1.8, the effect of camber angle and the effect of the lateral compliance of the tire tend to have opposing effects on the lateral translation of the centroid of the normal pressure distribution at the tire-road interface. Both of these effects are small and tend to cancel out. In order to keep the analysis simple, the lateral translation of the normal load is neglected.

The model contains a fairly detailed description of suspension and tire properties, such that the accurate prediction of steady-turning rollover threshold is possible. Computational costs are low due to the fact that no roll dynamics is included in the model. Moreover, a single computer run is sufficient for computing the rollover threshold, as well as the roll response of the vehicle over the entire range of lateral acceleration levels up to the rollover threshold.

2. VEHICLE CONFIGURATIONS USED IN THE SIMULATION STUDY

To quantitatively compare their predictive ability, the computer simulation models described above were used to predict the responses of six different commercial articulated vehicles in two types of turning manoeuvres, namely steady-state turning and lane-change (obstacle avoidance) manoeuvres.

The six vehicle configurations selected include five tractor-semitrailers and one five-axle double with 27 ft. trailer (that is, a two-axle tractor with a single-axle semitrailer and a two-axle full trailer). The basic parameters of the vehicles are summarized in Table 2.1.

A. Vehicle Configuration 1 is a fully-loaded three-axle tractor with a two-axle semitrailer. The basic parameters are similar to those of an International Harvester three-axle tractor (COF 4000 D) with a Fruehauf 45 - foot van-type semitrailer (FG8-F2-45') described in reference (5). A complete set of input data for the four computer simulation models, namely the Phase 4 model, the yaw/roll model, the TBS model, and the linear yaw plane model, is given in Appendix A.

B. Vehicle Configuration 2 is similar to Vehicle Configuration 1, but with the following modifications:

- a) The tractor frame has been stiffened, and its torsional stiffness has been increased from 20,000 to 120,000 in-lb/deg.
- b) An auxiliary roll-stiffening device ("sway bar") has been installed on the tractor front suspension. The device provides an additional roll stiffness of 109,385 in-lb/deg.

Table 2.1

Basic Parameters of Various Vehicle Configurations

Vehicle Configuration	1	2	3	4	5	6
A. Tractor	3-axle	3-axle	3-axle	3-axle	3-axle	2-axle
Wheelbase	142.0	142.0	144.0	144.0	144.0	120.0
Curb weight on front suspension	8,898	8,898	8,960	8,960	8,960	8,960
Curb weight on rear suspension	7,118	7,118	6,540	6,540	6,540	4,240
Sprung mass C.G. height	39.7	39.7	44.0	44.0	44.0	44.0
Sprung mass roll moment of inertia (in-lb-sec ²)	18,166.6	18,166.6	15,000	15,000	15,000	15,000
Sprung mass pitch moment of inertia (in-lb-sec ²)	69,955.0	69,955.0	75,000	75,000	75,000	75,000
Sprung mass yaw moment of inertia (in-lb-sec ²)	69,955.0	69,955.0	75,000	75,000	75,000	75,000
Fifth wheel location, ahead of rear suspension centre (in)	0.0	0.0	14.35	14.35	0	8.73
Fifth wheel height (in)	48.5	48.5	48.0	48.0	48.0	48.0
Frame torsional stiffness (in-lb/deg)	20,000	120,000	50,000	50,000	50,000	50,000
Roll centre height of front suspension (in)	24.55	24.55	23.0	23.0	23.0	23.0
Auxiliary roll stiffness of front suspension (in-lb/deg)	0	109,385	1,500	0	0	1,500
Roll centre height of rear suspension (in)	22.0	22.0	29.0	29.0	29.0	29.0
Auxiliary roll stiffness of leading tandem axle (in-lb/deg)	0	0	6,000	0	0	0
Auxiliary roll stiffness of trailing tandem axle (in-lb/deg)	78,000	78,000	6,000	78,000	78,000	8,000
Front tires	Type A	Type A	Type C	Type C	Type C	Type C
Rear tires	Type A	Type A	Type C	Type C	Type C	Type C

Table 2.1

Basic Parameters of Various Vehicle Configurations

Vehicle Configuration	1 2 3 4 5 6					
	Tandem Axle	Tandem Axle	Tandem Axle	Tandem Axle	Tandem Axle	Single Axle
B. Semitrailer						
Wheelbase	410.0	410.0	432.0	432.0	432.0	252.0
Kingpin static load	6,252.3	6,252.3	4,500	4,500	4,500	2,250
Curb weight on rear suspension	11,068.7	11,068.7	7,500	7,500	7,500	3,750
Sprung mass C. G. height	69.0	69.0	60.0	60.0	60.0	60.0
Sprung mass roll moment of inertia (in-lb-sec ²)	73,000	73,000	60,000	60,000	60,000	30,000
Sprung mass pitch moment of inertia (in-lb-sec ²)	789,869	789,860	750,000	750,000	750,000	93,750
Sprung mass yaw moment of inertia (in-lb-sec ²)	789,869	789,869	750,000	750,000	750,000	93,750
Payload weight	40,600	40,600	52,500	52,500	52,500	25,800
Payload C.G. ahead of rear suspension centre	182.0	182.0	213.9	213.9	213.9	117.7
Payload C.G. height	64.5	64.5	85.0	85.0	85.0	85.0
Payload roll moment of inertia (in-lb-sec ²)	37,500	37,500	132,000	132,000	132,000	65,000
Payload pitch moment of inertia (in-lb-sec ²)	1,727,000	1,727,000	3,050,000	3,050,000	3,050,000	375,000
Payload yaw moment of inertia (in-lb-sec ²)	1,727,000	1,727,000	3,100,000	3,100,000	3,100,000	375,000
Roll stiffness of fifth wheel (in-lb/deg)	9,999,999	9,999,999	1,000,000	1,000,000	1,000,000	1,000,000
Roll centre height	25.6	25.6	29.0	29.0	29.0	29.0
Auxiliary roll stiffness of leading tandem axle (in-lb/deg)	0	0	10,000	0	0	10,000
Auxiliary roll stiffness of trailing tandem axle (in-lb/deg)	0	0	10,000	0	0	10,000
Tires	Type B	Type B	Type C	Type C	Type C	Type C

Table 2.1

Basic Parameters of Various Vehicle Configurations

Vehicle Configuration	1	2	3	4	5	6
C. Trailer						2-axle
Distance from dolly suspension to pintle hook (in)						80.0
Turntable location ahead of dolly suspension centre (in)						0
Turntable height (in)						48.0
Wheelbase (in)						252.0
Curb weight on front suspension (lb)						4,250
Curb weight on rear suspension (lb)						4,250
Sprung mass C.G. height (in)						60.0
Sprung mass roll moment of inertia (in-lb-sec ²)						36,000
Sprung mass pitch moment of inertia (in-lb-sec ²)						115,000
Sprung mass yaw moment of inertia (in-lb-sec ²)						115,000
Payload weight (lb)						26,500
Payload C.G. ahead of rear suspension centre (in)						126.0
Payload C.G. height (in)						85.0
Payload roll moment of inertia (in-lb-sec ²)						65,000
Payload pitch moment of inertia (in-lb-sec ²)						375,000
Payload yaw moment of inertia (in-lb-sec ²)						375,000
Centre height of front suspension (in)						29.0
Auxiliary roll stiffness of front suspension (in-lb-deg)						10,000
Roll centre height of rear suspension (in)						29.0
Auxiliary roll stiffness of rear suspension (in-lb/deg)						10,000
Tires						Type C

The stiffening of the tractor frame and the increasing of the roll stiffness of the front suspension of the tractor modify the roll moment distribution between the tractor front and rear suspensions in a turning manoeuvre. High percentage of the roll moment will be supported by the front suspension, which causes more lateral load transfer from the inside tire to the outside tire on the tractor front axle. This produces an understeer effect for the tractor. Therefore, the increasing of the frame torsional stiffness and the roll stiffness of the front suspension of the tractor will result in a significant change in the handling behaviour of the vehicle.

It should be pointed out that although the frame stiffener and the auxiliary roll-stiffening device on the front suspension employed to achieve significant changes in roll moment distribution would never be used in practice, they do provide changes in vehicle handling characteristics suitable for studying the influence of altering the roll moment distribution and for evaluating the ability of various simulation models to predict these influences.

A complete set of input data for the four computer models for simulating this vehicle configuration is given in Appendix B.

C. In comparison with Vehicle Configuration 1 and 2, Vehicle Configuration 3 has different loading conditions, and is equipped with a different type of tire. Furthermore, the fifth wheel is located 14.35 in. ahead of the rear suspension centre of the tractor. These factors combined will make the handling behaviour of this vehicle configuration different from that of Vehicle Configurations 1 and 2.

D. Vehicle Configuration 4 is similar to Vehicle Configuration 3, but with the following modifications:

- a) Auxiliary roll-stiffening devices on the tractor front suspension and on its leading tandem axle suspension have been removed. Consequently, the auxiliary roll stiffness of the two suspensions are reduced to zero.
- b) A different auxiliary roll-stiffening device is installed on the trailing tandem axle of the tractor and its roll stiffness is increased to 78,000 in-lb/deg.

These two factors combined produce an oversteer effect for the tractor.

A complete set of input data for the four computer models for simulating this vehicle configuration is given in Appendix D.

E. Vehicle Configuration 5 is similar to Vehicle Configuration 4, with the exception that the fifth wheel centre is located at the centre of the rear suspension of the tractor. The rearward shift of the fifth wheel centre, as compared with that in Vehicle Configuration 4, tends to produce an oversteer effect for the tractor.

A complete set of input data for the computer models for simulating this vehicle configuration is given in Appendix E.

F. Vehicle Configuration 6 is a five-axle double with 27 ft trailers. It consists of a two-axle tractor, a single axle semitrailer and a two-axle full trailer. This vehicle configuration is included in the study

to provide an additional case for evaluating the predictive ability of the various computer simulation models. It should be mentioned that only the linear yaw plane model, the yaw/roll model, and the Phase 4 model were used in the simulation of this vehicle configuration, as the TBS model was designed solely for simulating the tractor-semitrailer.

Three sets of input data for the three computer models for simulating this vehicle configuration are given in Appendix F.

As can be seen from Table 2.1, three types of tire, referred to as Type A (Firestone Rib 10.00 x 22F), Type B (Freuhauf Rib 10.00 x 20F), and Type C, are used in the study. The variations of the cornering (lateral) force and aligning torque with sideslip angle for the three types of tire are shown in Figs. 2.1, 2.2, and 2.3, respectively. It can be seen that Types A and B have lower cornering stiffness (or the equivalent) than Type C. The aligning torque of Type A is higher than those of Types B and C at sideslip angles less than approximately 8° with normal load of 9,000 lb, and at sideslip angles less than approximately 10° with normal load of 6,000 lb. Types B and C have similar aligning torque-sideslip angle characteristics at normal loads of 6,000 and 9,000 lb.

TIRE A

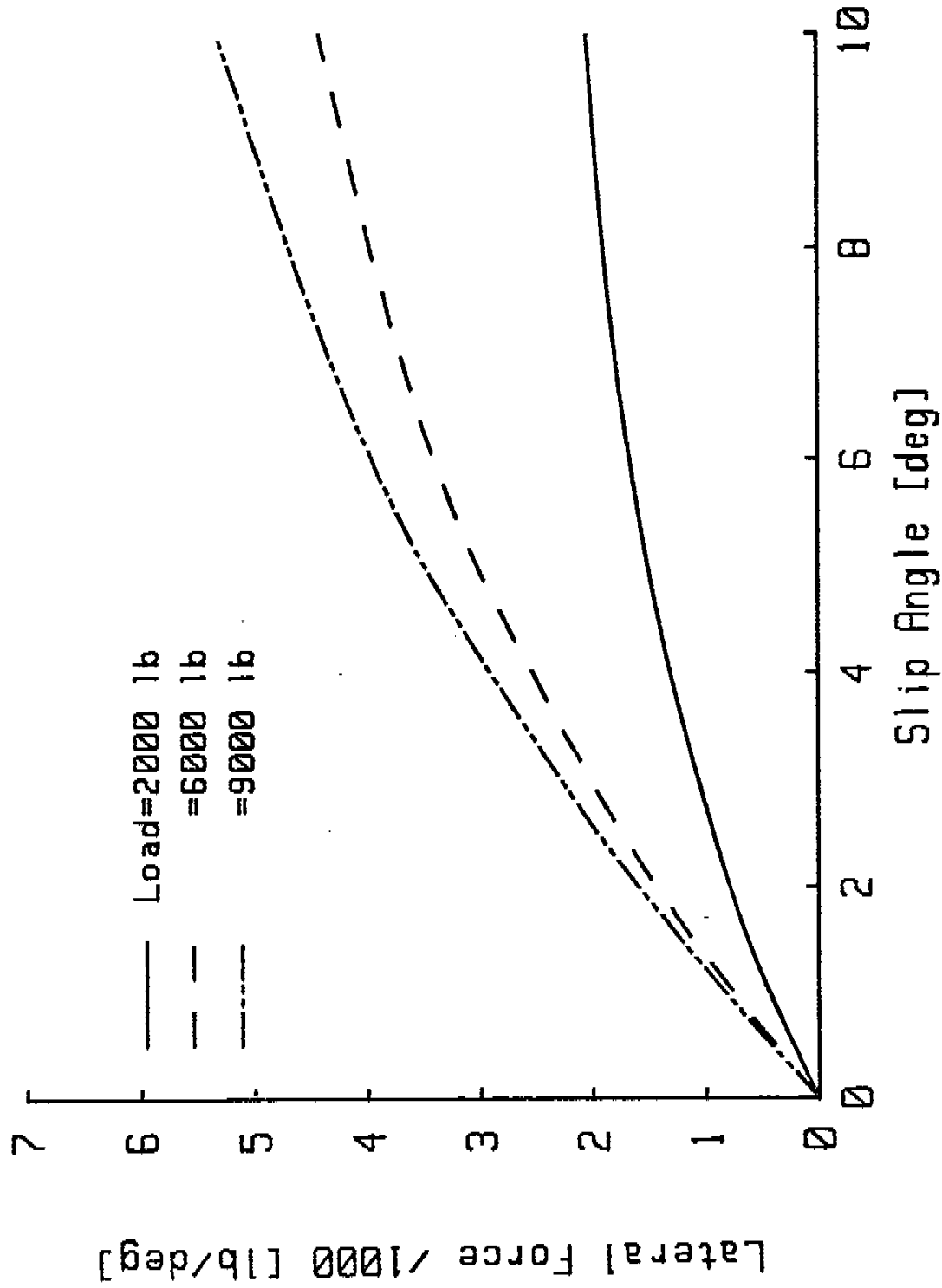


Fig. 2.1 (a) Firestone 10.00 x 22F

TIRE A

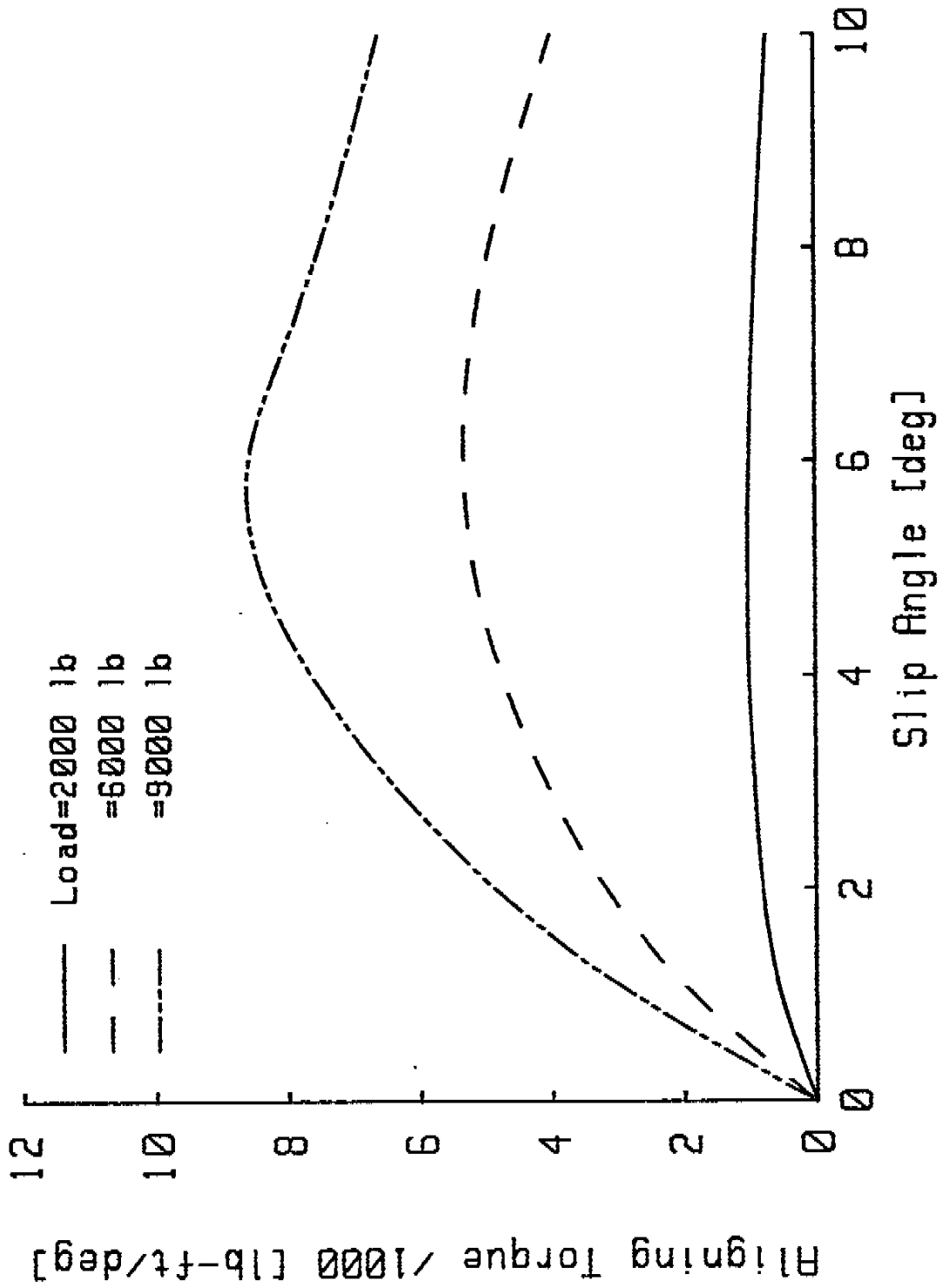


Fig. 2.1 (b)

TIRE B

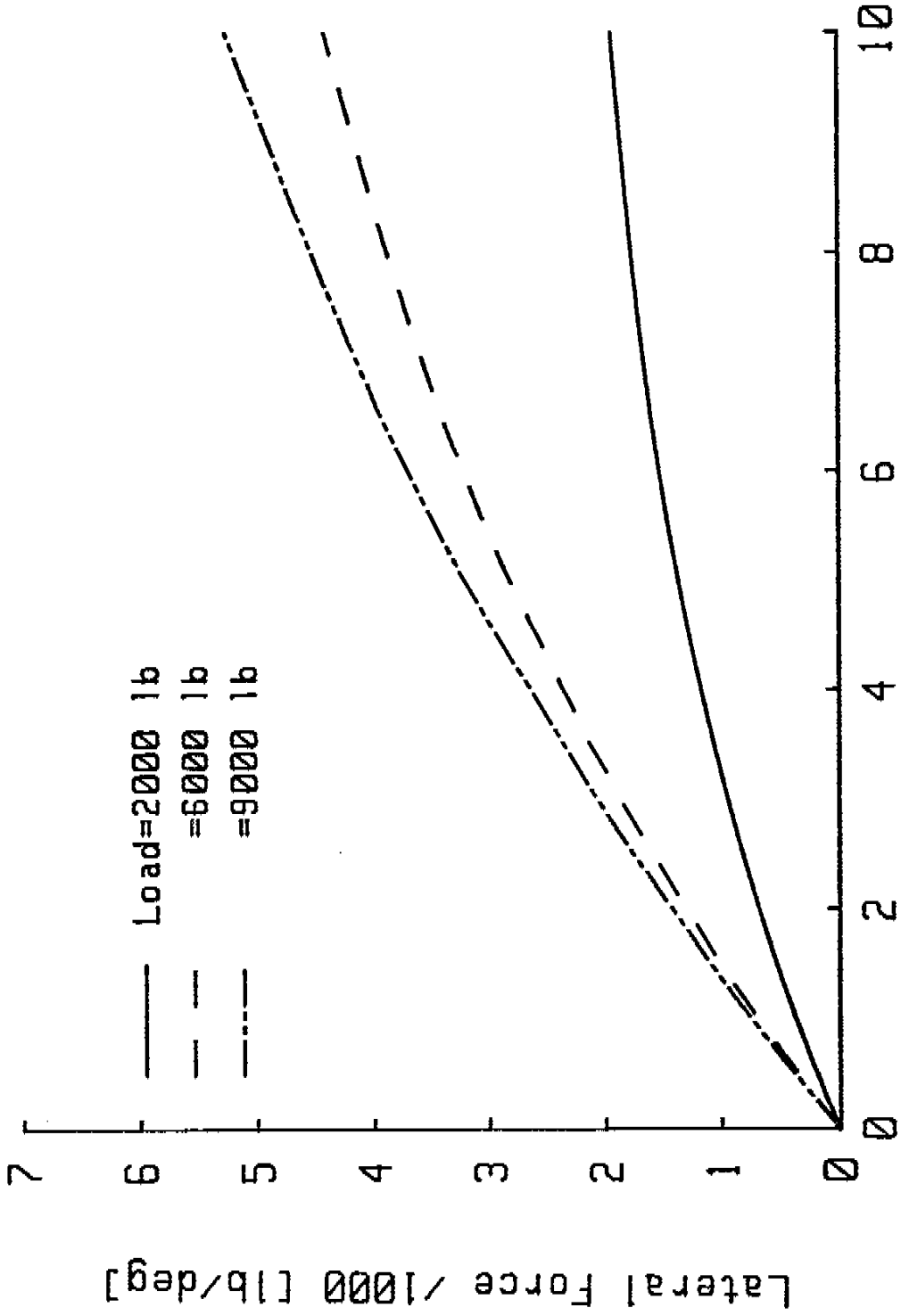


Fig. 2.2 (a) Freuhauf 10.00 x 20F

TIRE B

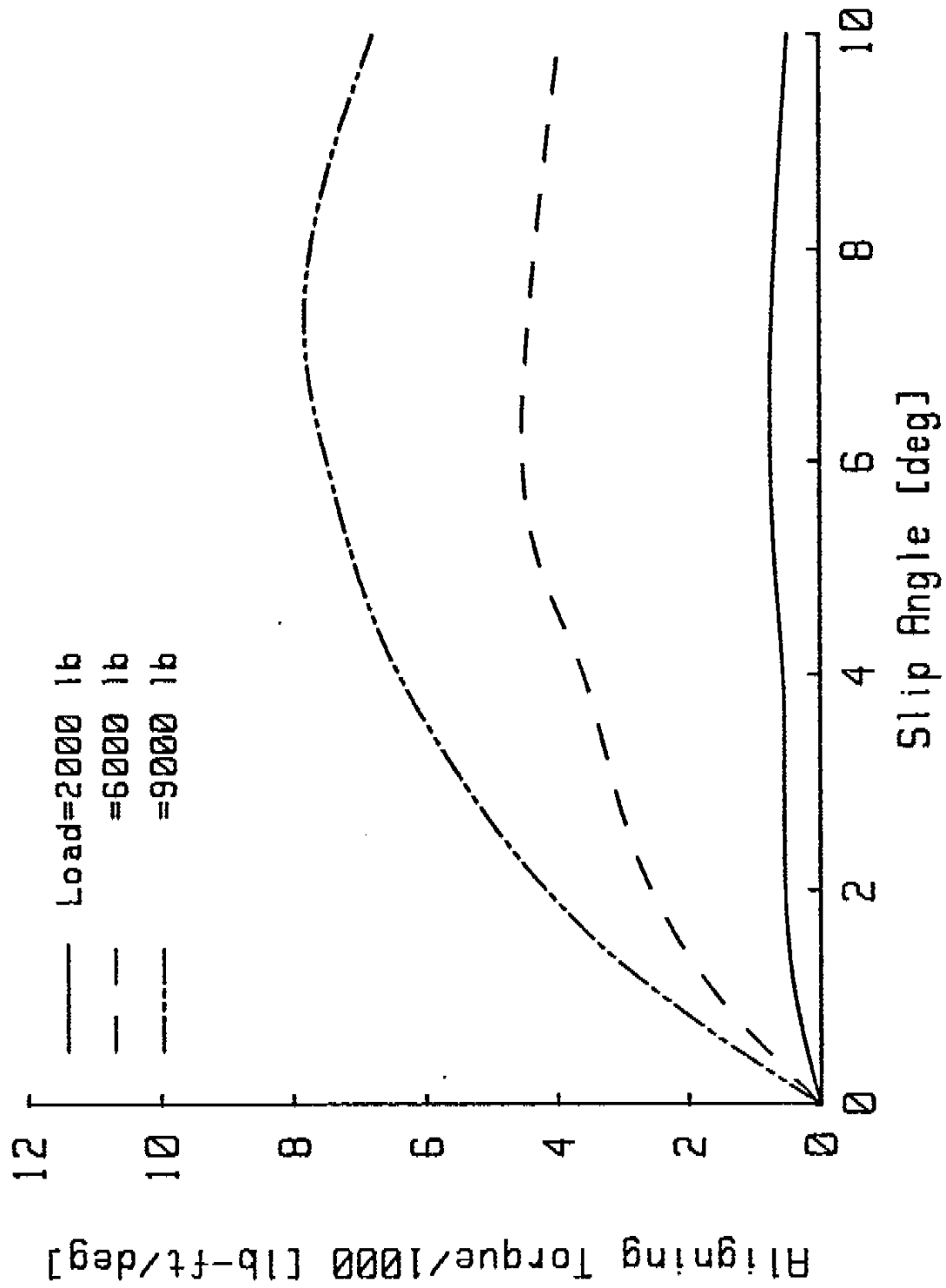


Fig. 2.2 (b)

TIRE C

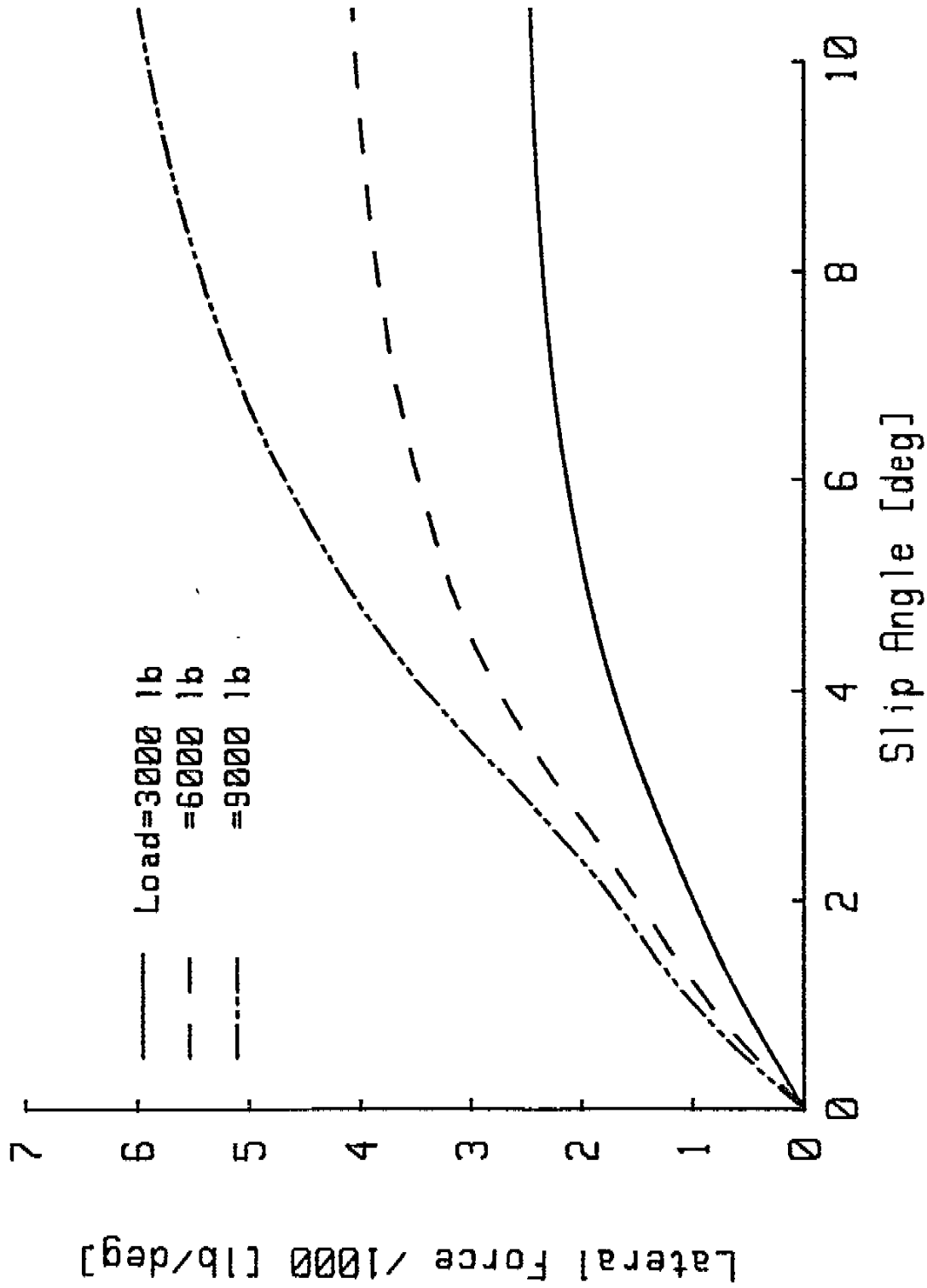


Fig. 2.3 (a)

TIRE C

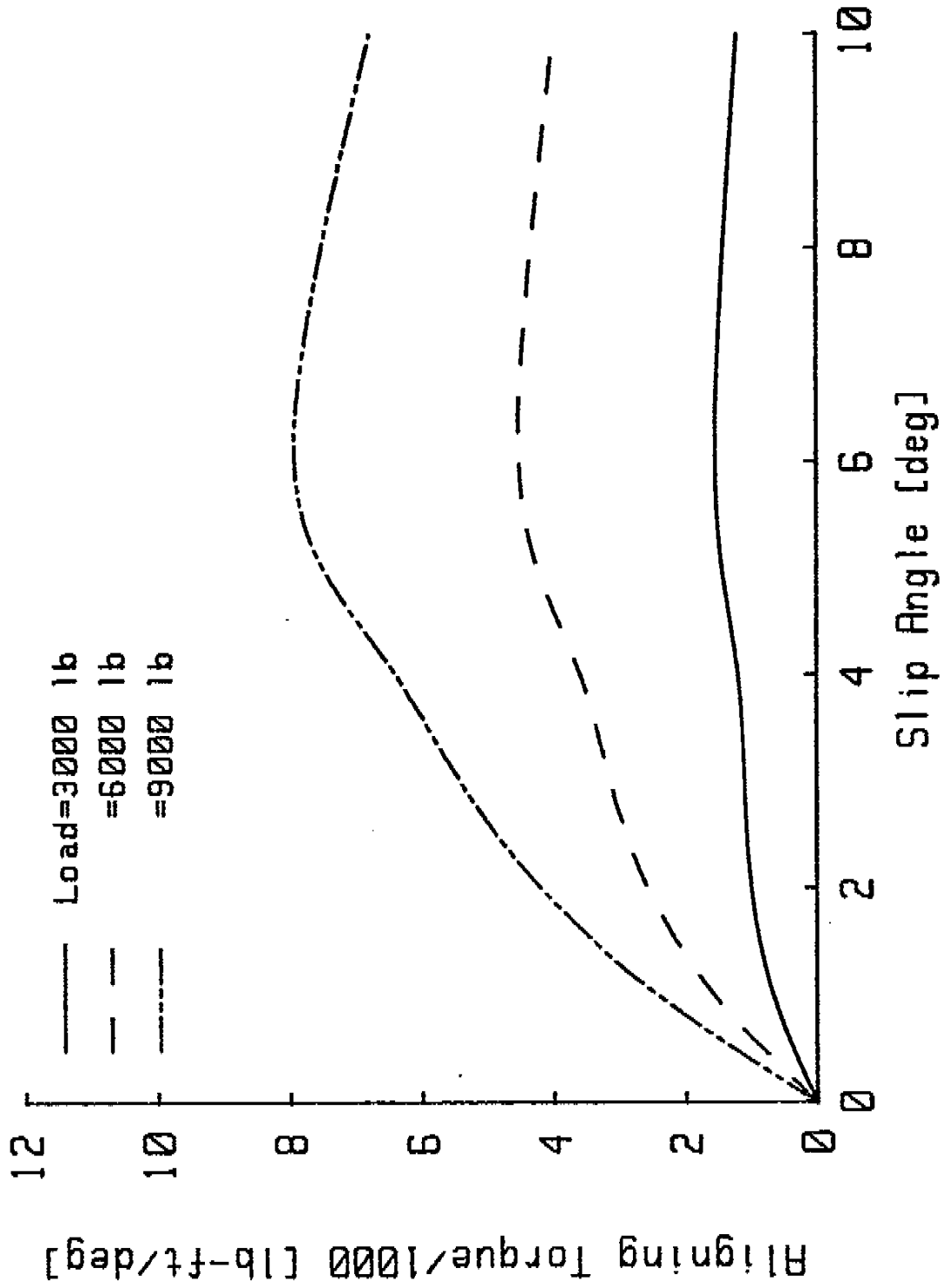


Fig. 2.3 (b)

It has been shown that among other factors the characteristics of the tires and their placement on the vehicle, the distribution of roll stiffness among the suspensions, the location of the fifth wheel, and the location of the centre of gravity of the payload have significant effects on the handling of an articulated vehicle. The six vehicles and the three types of tire selected in this study, therefore, represent a range of vehicle configurations that are expected to have substantially different lateral dynamic behaviour in both the linear and nonlinear regimes. These will provide a wide range of conditions under which the predictive ability of the various computer simulation models may be evaluated and compared quantitatively.

3. A COMPARISON OF THE CAPABILITIES OF VARIOUS COMPUTER SIMULATION MODELS IN PREDICTING STEADY-STATE STEERING RESPONSES

The steady-state steering responses of the six vehicle configurations described in the preceding section were predicted using the four computer simulation models, that is, the linear yaw plane model, the TBS model, the yaw/roll model, and the Phase 4 model. In the simulations, ramp inputs of front-wheel steering angle as shown in Fig. 3.1 were applied. After the response of the vehicle reached a steady-state, the lateral acceleration and yaw rate of the tractor as functions of the front-wheel steering angle were determined, and the handling diagram for the tractor was plotted (5)(6). The handling diagram illustrates the relationship between the lateral acceleration of the tractor a_y and the parameter $(l/R - \delta)$, where l is the wheelbase of the tractor, R is the turning radius, and δ is the front-wheel steering angle. The turning radius can be derived from the ratio of the yaw rate, r , to forward speed of the vehicle, V . The steady-state steering behaviour of the vehicle (neutral steer, understeer, or oversteer) can then be determined from the handling diagram. If the slope of the a_y versus $(r l / V - \delta)$ curve is negative, then understeer behaviour is indicated. If the slope of the curve is positive, then the vehicle exhibits oversteer characteristics. On the other hand, if the slope of the curve is infinite, neutral steer is indicated.

The steering responses of the six vehicle configurations in steady-state turns predicted using the four computer simulation models are given below.

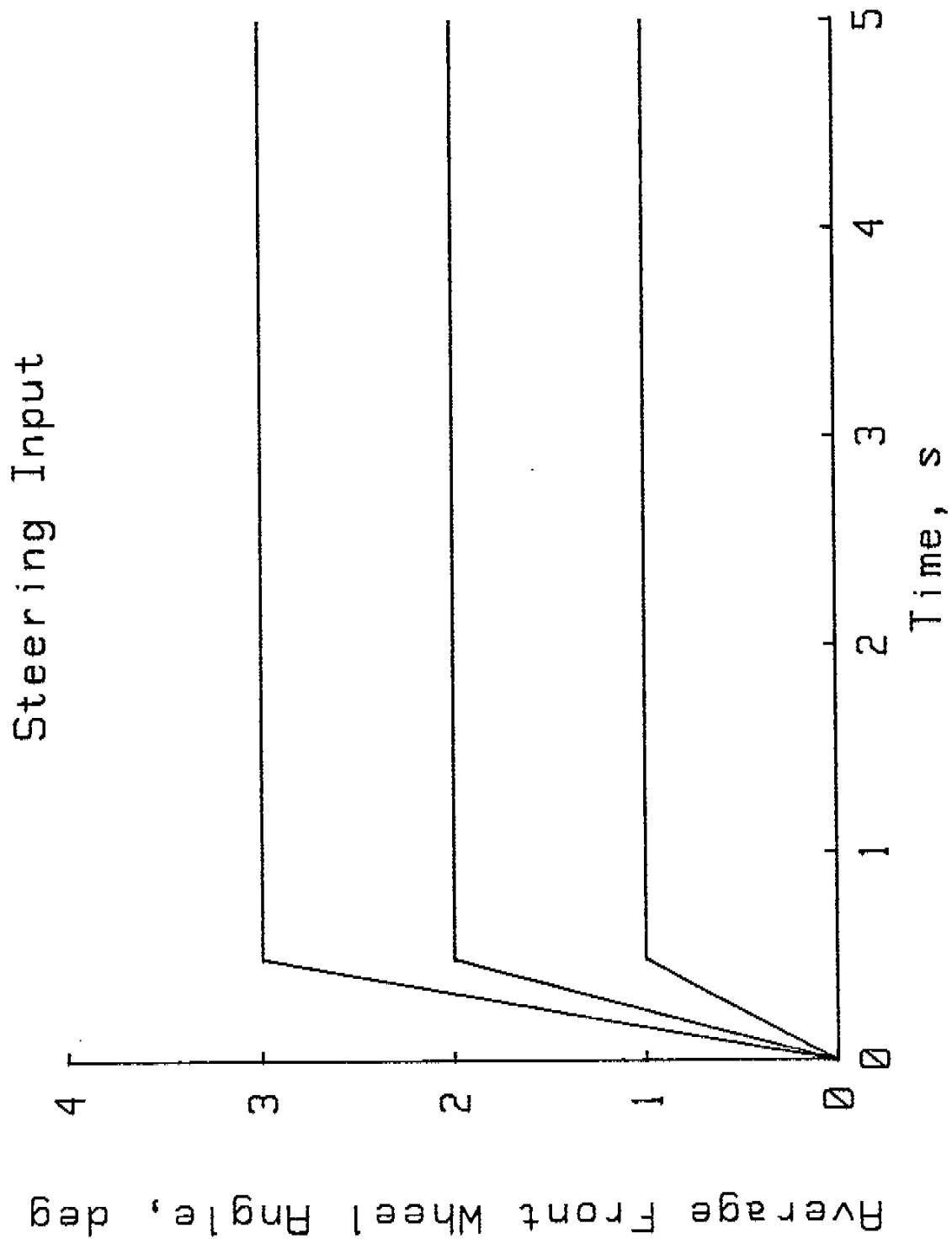


Figure 3.1 Ramp Input of Front-wheel Steering Angle Used in the Simulations

3.1 Vehicle Configuration 1

The steering responses of this vehicle configuration in steady-state turns at a forward speed of 43 mph (63.07 ft/s) on a dry, smooth asphalt surface were predicted using the four computer simulation models. The predicted relationships between the lateral accelerations of the tractor and the front-wheel steering angle, together with the measured data reported in reference (5), are shown in Fig. 3.2. The predicted yaw rates of the tractor as a function of the front-wheel steering angle, together with the measured ones, are shown in Fig. 3.3. Based on the predicted lateral accelerations and yaw rates of the tractor, a handling diagram is drawn as shown in Fig. 3.4. For comparison, the measured data are also shown. It should be noted that the square symbol in the figure represents the values calculated from the measured yaw rates of the tractor shown in Figs. 3.2 at a forward speed of 63.07 ft/sec, whereas the triangular symbol represents the values taken from reference (5). All the measured data shown in Figs. 3.2, 3.3 and 3.4 are for left-turn manoeuvres. The predicted values of yaw rate, \bar{r} , lateral acceleration, a_y , roll angle of the tractor, ϕ_1 , roll angle of the semitrailer, ϕ_2 , and articulation angle of the semitrailer with respect to the tractor Γ_1 and the corresponding measured values for various average front-wheel steering angles, δ_{av} , are given in Table 3.1

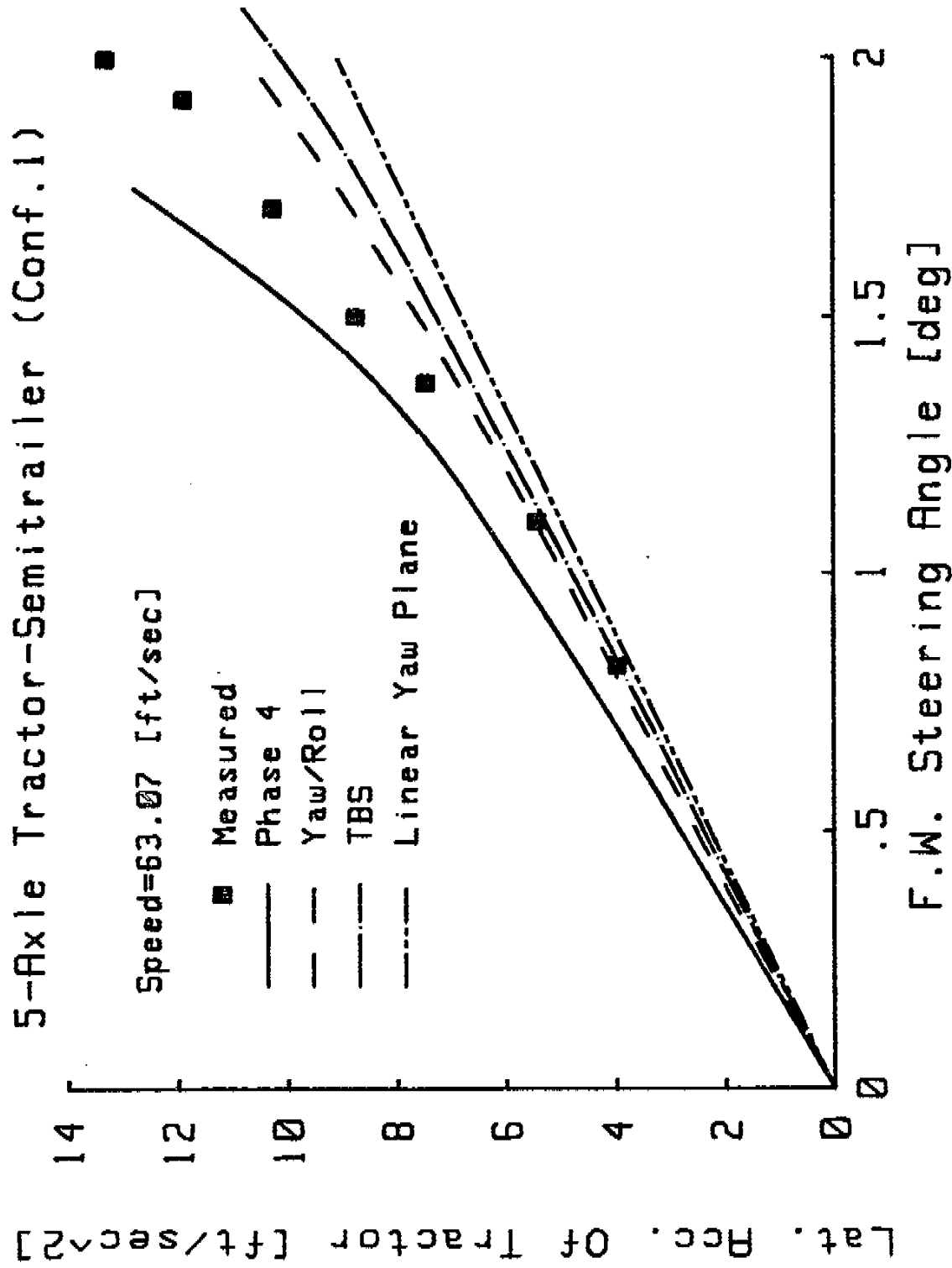


Fig. 3.2 Steady-state Lateral Acceleration Response to Steering Input of Vehicle Configuration 1 Predicted by Various Models

5-Axle Tractor-Semitrailer (Conf.1)

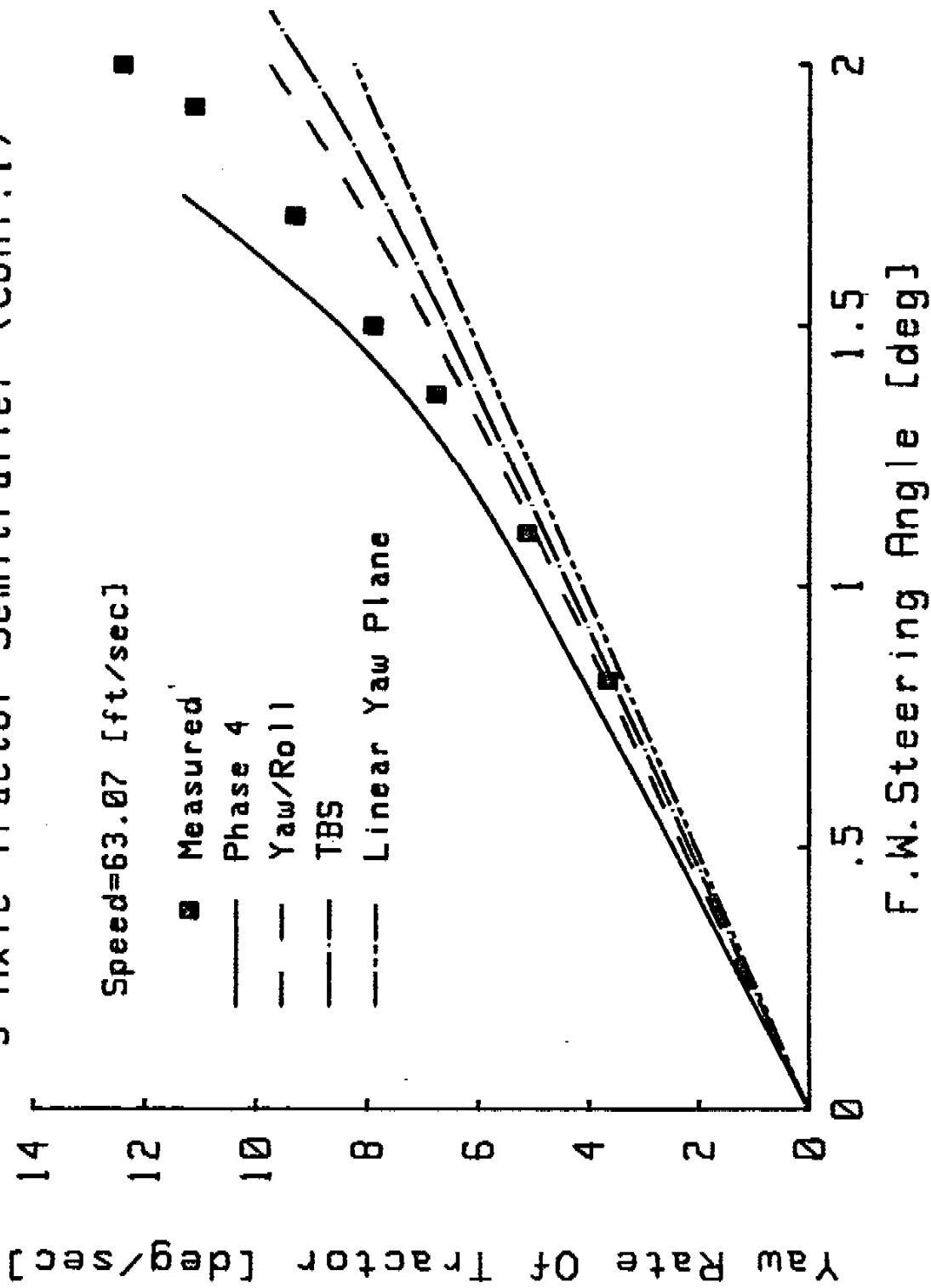


Fig. 3.3 Steady-state Yaw Rate Response to Steering Input of Vehicle Configuration 1 Predicted by Various Models

5-Axle Tractor-Semitrailer (Conf. 1)

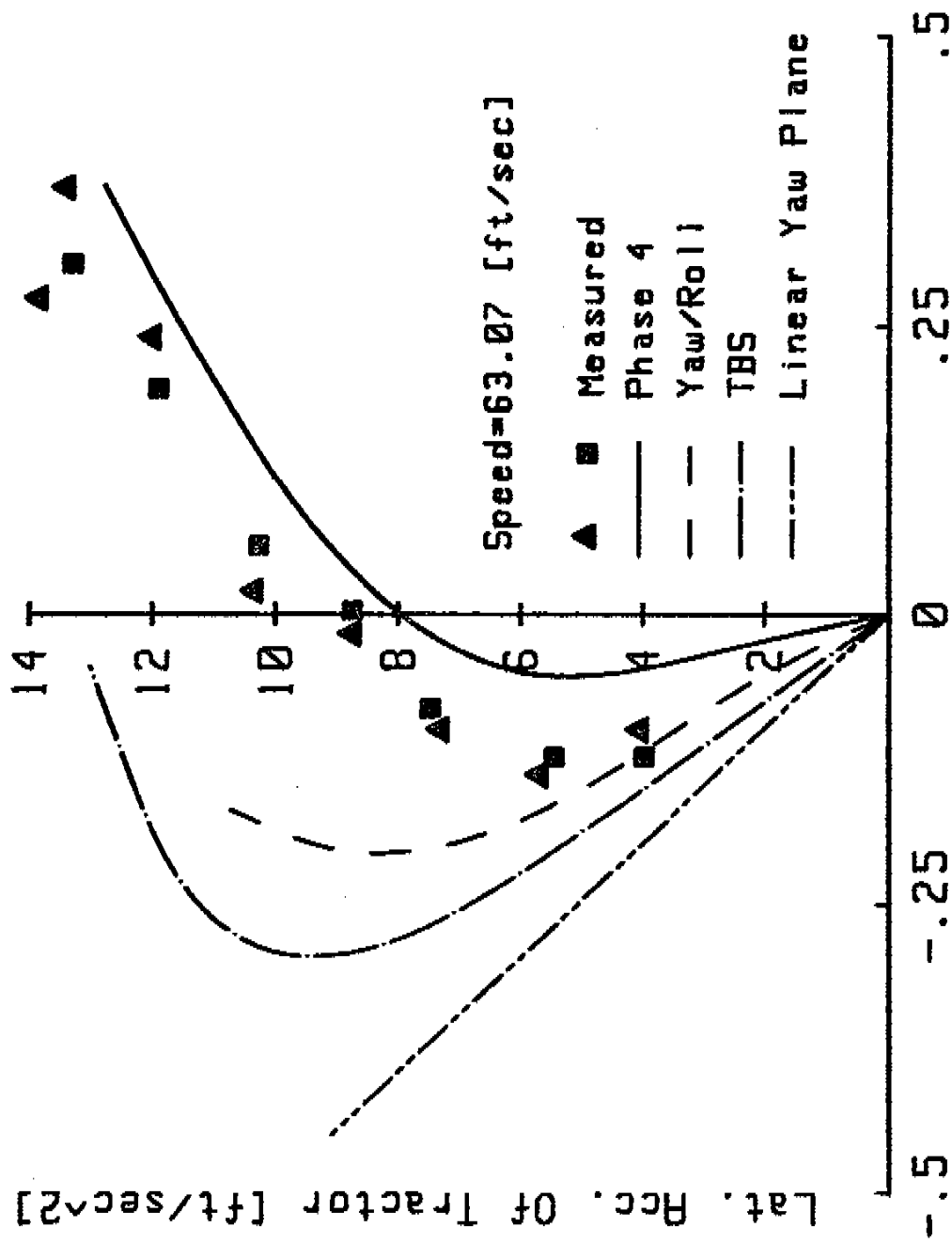


Fig. 3.4 Handling Characteristics of Vehicle Configuration 1

Predicted by Various Models

TABLE 3.1
VEHICLE CONFIGURATION 1

A. Phase 4 Model

δ_{av} [deg]	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*z/U-\delta_{av}$ [deg]	ϕ_1 [deg]	ϕ_2 [deg]	Γ_1 [deg]
0.5	62.99	2.48	2.82	-0.034	-1.18	-0.94	1.26
1.0	63.07	5.05	5.77	-0.052	-2.39	-1.94	2.49
1.5	63.06	8.49	9.65	+0.093	-3.94	-3.23	4.05
1.75	63.07	11.31	12.80	+0.372	-5.15	-4.26	4.83

B. Yaw/Roll Model

δ_{av} [deg]	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*z/U-\delta_{av}$ [deg]	ϕ_1 [deg]	ϕ_2 [deg]	Γ_1 [deg]
0.5	63.07	2.29	2.52	-0.07	-0.76	-0.76	1.15
1	63.07	4.52	4.97	-0.15	-1.50	-1.50	2.24
1.5	63.07	6.91	7.608	-0.203	-2.29	-2.29	3.40
1.75	63.07	8.25	9.08	-0.202	-2.74	-2.75	4.01
2.0	63.07	9.76	10.73	-0.168	-3.24	-3.25	4.62

C. TBS Model

δ_{av} [deg]	U [ft/sec]	r [deg/sec]	A_y [ft/sec ²]	$r^* \ell/U - \delta_{av}$ [deg]	r_1 [deg]
0.6	62.97	2.61	2.87	- 0.109	1.3
1.0	63.07	4.36	4.80	- 0.182	2.16
1.2	63.2	5.25	5.80	- 0.217	2.6
1.5	63.07	6.59	7.27	- 0.263	3.26
1.9	63.07	8.55	9.45	- 0.295	4.13
2.1	63.08	9.75	10.81	- 0.271	4.51
2.2	63.08	10.63	11.81	- 0.205	4.53
2.25	63.05	11.75	13.02	- 0.044	4.56

D. Linear Yaw Plane Model

δ_{av} [deg]	U [ft/sec]	r [deg/sec]	A_y [ft/sec ²]	$r^* \ell/U - \delta_{av}$ [deg]	r_1 [deg]
0.5	63.07	2.06	2.27	- 0.113	1.03
1.5	63.07	6.18	6.80	- 0.340	3.08
2.0	63.07	8.24	9.08	- 0.454	4.12

E. Measurements

δ_{av} (deg)	r (deg/sec)	A_y (ft/sec ²)	Calculated *	Measured **	
			$r^* \ell/U - \delta_{av}$ (deg)	A_y (ft/sec ²)	$r^* \ell/U - \delta$ (deg)
0.82	3.66	3.97	-0.1333	4.04	- 0.1
1.1	5.13	5.44	-0.1375	5.68	- 0.139
1.37	6.77	7.47	-0.0998	7.3	- 0.1
1.5	7.9	8.75	+0.0178	8.75	- 0.017
1.71	9.3	10.27	+0.0349	10.34	+ 0.02
1.92	11.12	11.9	+0.1664	12.0	+ 0.24
2.055	12.4	13.3	+0.2715	13.4	+ 0.37
2.2	12.83	13.7	+0.202	13.84	+ 0.274

* Calculations based on the measured yaw rates, a forward speed of 63.07 ft/sec, and a wheelbase of 142 in.

** Measured values taken from reference (5)

All measured values are for left-turn manoeuvres

It can be seen from Fig. 3.2 that the lateral accelerations of the tractor predicted using the linear yaw plane model, the TBS model and the yaw/roll model are reasonably close within the range up to 2 degrees of front-wheel steering angle (equivalent to lateral acceleration of approximately 0.3 g). However, there is a significant difference between the lateral accelerations predicted using the Phase 4 model and those predicted using the other three models for front-wheel steering angles greater than 1.5 degrees (equivalent to lateral acceleration of approximately 0.2 g.)

From Fig. 3.2 or Table 3.1, it can be noted that at front-wheel steering angle $\delta_{av} = 1.0^\circ$, the differences between the measured lateral acceleration and the predicted ones using the Phase 4 model, the yaw/roll model, the TBS model, and the linear yaw plane model are 17.5%, 1.2%, 2.3%, and 7.7%, respectively. At front-wheel steering angle $\delta_{av} = 1.5^\circ$, the corresponding differences are 10.3%, 13.1%, 13.8%, and 22.3%, respectively.

As can be seen from Fig. 3.3 or Table 3.1, the differences between the measured yaw rates and the predicted ones using the Phase 4 model, the yaw/roll model, the TBS model and the linear yaw plane model show similar trend as that between the measured lateral accelerations and the predicted ones using the four computer simulation models described above.

Based on the data shown in Figs. 3.2 and 3.3, and Table 3.1, it appears that for lateral accelerations below 0.2 g, the four computer

simulation models give similar predictions and the predicted values agree reasonably well with the measured ones. For the lateral acceleration range between 0.2 g and 0.3 g, the Phase 4 model, the yaw/roll model and the TBS model seem to have similar error of prediction, in comparison with the measured values. However, the Phase 4 model overestimates the responses, while the yaw/roll model and the TBS model underestimate them. For lateral accelerations higher than 0.2 g, the linear yaw plane model gives higher error of prediction than the other three models. This is primarily due to the fact that in the linear yaw plane model a linear tire model is used and the load transfer and its effects on tire characteristics have been entirely neglected.

It should also be mentioned that the lateral acceleration which causes an inside tire to lift off the ground predicted by the Phase 4 model, the yaw/roll model and the TBS model is considerably lower than the measured one reported in reference (5).

Fig. 3.4 illustrates the steady-state handling characteristics of Vehicle Configuration 1 as predicted by the four computer simulation models. It can be seen that the lateral acceleration at which the vehicle changes from understeer to oversteer, referred to as the "transition acceleration", predicted using the Phase 4 model is just under 0.2 g. The transition accelerations predicted using the yaw/roll model and the TBS model are approximately 0.25 g and 0.3 g, respectively, while the measured one is approximately 0.2 g. Below the transition acceleration, the Phase 4 model underestimates the understeer level (or "understeer gradient") as compared with the measured data, whereas the TBS model and the linear

yaw plane model overestimate the understeer level to varying degrees. The yaw/roll model appears to give the best prediction of the understeer level. It should be mentioned that since a linear tire model is used, the linear yaw plane model is unable to predict any variation of the handling behaviour of the vehicle with lateral acceleration and the predicted understeer level remains a constant.

From Table 3.1, it can be seen that the yaw/roll model, the TBS model, and the linear yaw plane model give similar predictions of the articulation angle of the semitrailer with respect to the tractor, while the Phase 4 model gives a higher prediction than the other three models. It should also be mentioned that the roll angles of the spring masses of the tractor and the semitrailer predicted by the yaw/roll model are essentially the same, whereas those predicted using the Phase 4 model are considerably different.

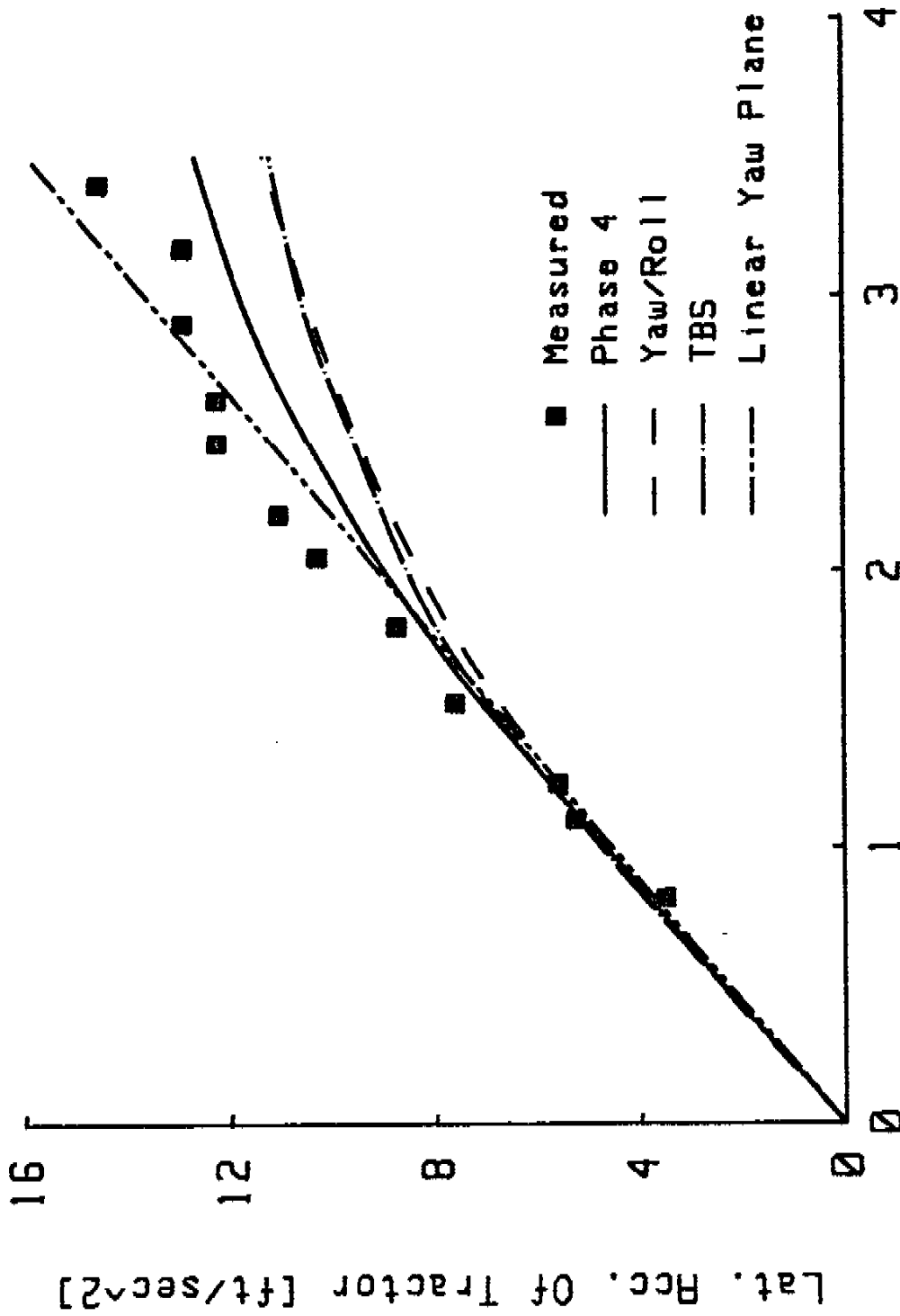
3.2 Vehicle Configuration 2

As mentioned in Section 2, this vehicle is a modified version of Vehicle Configuration 1, with much higher torsional stiffness of the tractor frame and roll stiffness of the tractor front suspension. These two major modifications tend to make the tractor highly understeer.

It should be pointed out that among the four computer simulation models, only the Phase 4 model takes into account the effects of both the tractor frame torsional stiffness and the roll stiffnesses of the suspensions. The yaw/roll model and the TBS model only take into account the effects of the roll stiffnesses of the suspensions. The tractor frame is assumed to be rigid in these two simulation models. The linear yaw plane model does not include either the tractor frame torsional stiffness or the roll stiffnesses of the suspensions. Consequently, these changes do not affect the predictions made by the linear yaw plane model. The steady-state steering response of Vehicle Configuration 2 predicted using the linear yaw plane model is, therefore, the same as that of Vehicle Configuration 1 described previously.

The predicted steady-state lateral accelerations and yaw rates of the tractor using the four computer simulation models, are shown in Figs. 3.5 and 3.6, respectively. Based on the predictions, a handling diagram is drawn as shown in Fig. 3.7. For comparison, the measured data taken from reference (5) are also included in the figures. The predicted and the measured values for various front-wheel steering angles are also given in Table 3.2.

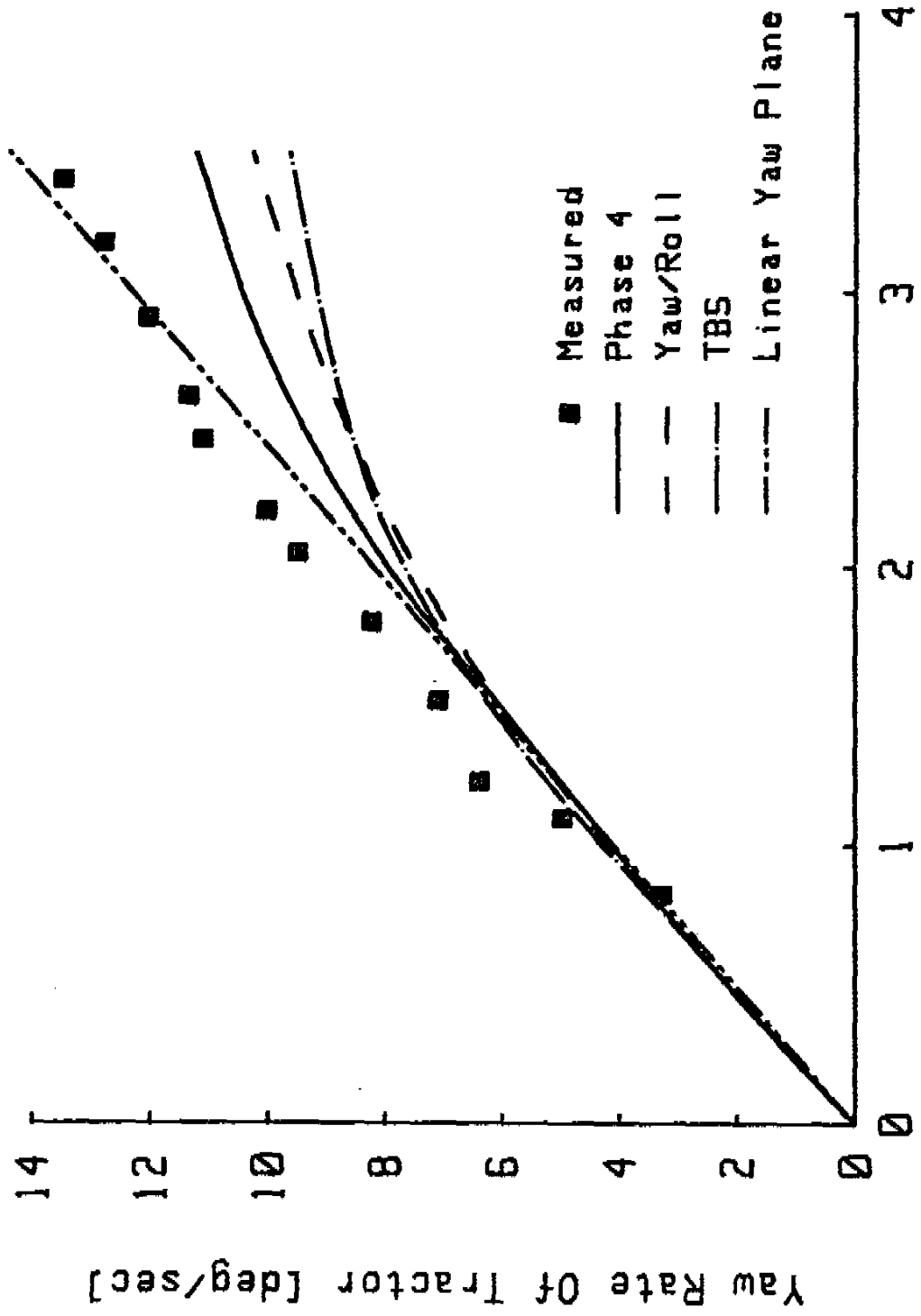
5-Axle Tractor-Semitrailer (Conf.2)



F.W. Steering Angle [deg]

Fig. 3.5 Steady-state Lateral Acceleration Response to Steering input of Vehicle Configuration 2 Predicted by Various Models

5-Axle Tractor-Semitrailer (Conf.2)



F.W. Steering Angle [deg]

Fig. 3.6 Steady-state Yaw Rate Response to Steering Input of Vehicle Configuration 2 Predicted by Various Models

5-Axle Tractor-Semitrailer (Conf.2)

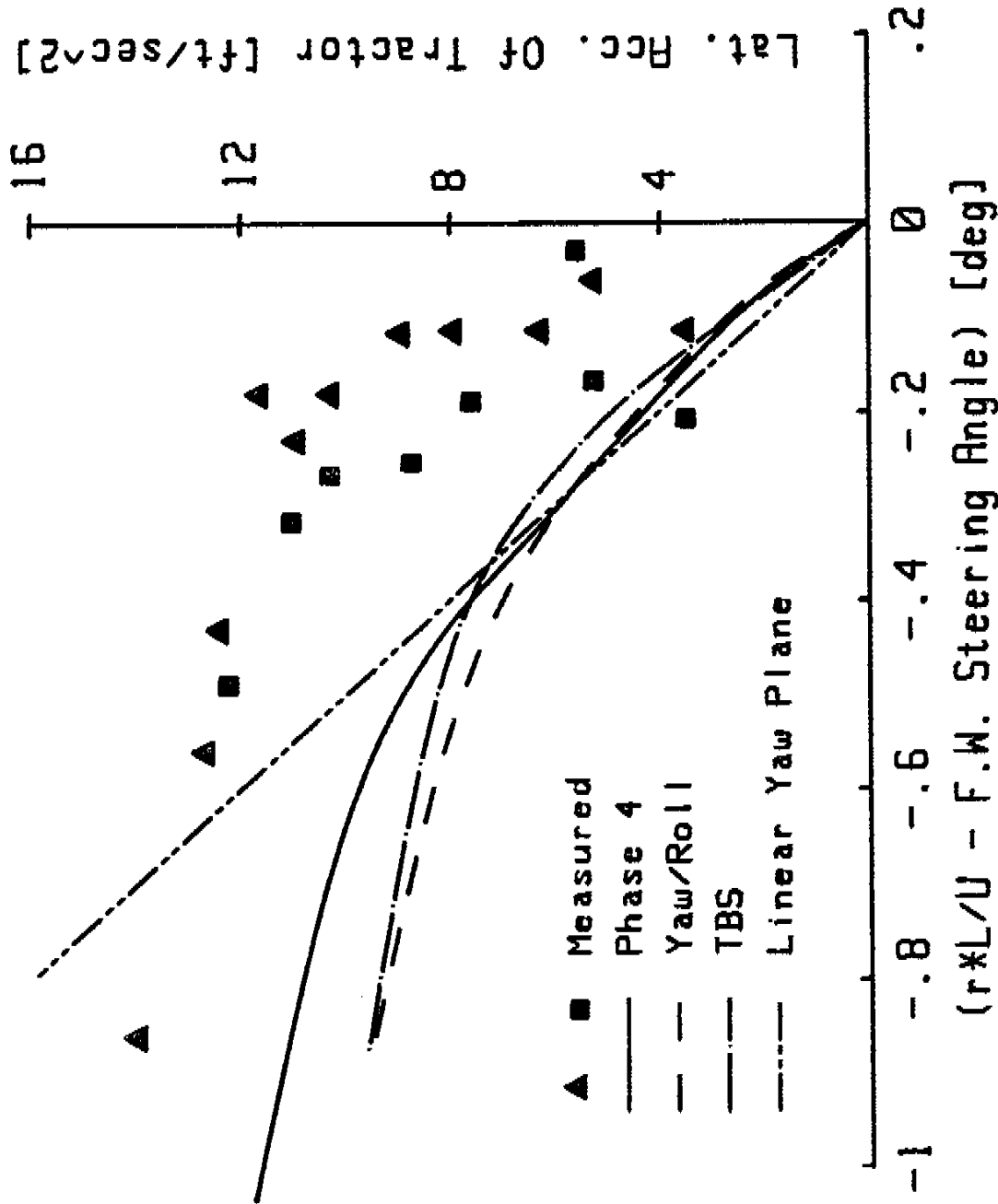


Fig. 3.7 Handling Characteristics of Vehicle Configuration 2 Predicted by Various Models

TABLE 3.2
VEHICLE CONFIGURATION 2

A. Phase 4 Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*l/U-\delta_{av}$ (deg)	ϕ_1 (deg)	ϕ_2 (deg)	Γ_1 (deg)
0.5	63.07	2.18	2.368	-0.091	-0.50	-0.71	1.06
1.0	63.11	4.15	4.65	-0.221	-0.95	-1.37	2.00
1.5	63.10	6.06	6.79	-0.363	-1.39	-2.00	2.85
2.0	63.07	7.98	8.96	-0.502	-1.83	-2.64	3.72
2.5	63.05	9.40	10.55	-0.735	-2.15	-3.10	4.23
3.0	63.07	10.47	11.78	-1.035	-2.39	-3.46	4.55
3.5	63.10	11.25	12.66	-1.390	-2.55	-3.69	4.68

B. Yaw/Roll Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*l/U-\delta_{av}$ (deg)	ϕ_1 (deg)	ϕ_2 (deg)	Γ_1 (deg)
0.5	63.07	2.20	2.42	-0.087	-0.58	-0.58	1.11
1.0	63.07	4.20	4.61	-0.212	-1.11	-1.11	2.08
1.5	63.07	6.05	6.65	-0.364	-1.59	-1.60	2.99
2.0	63.07	7.53	8.29	-0.587	-1.98	-2.0	3.72
2.5	63.07	8.66	9.53	-0.875	-2.28	-2.3	4.25
3.0	63.07	9.55	10.51	-1.208	-2.52	-2.54	4.63
3.5	63.07	10.29	11.32	-1.569	-2.71	-2.74	4.93

C. TBS Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*l/U-\delta_{av}$ (deg)	Γ_1 (deg)
0.5	63.05	2.17	2.39	-0.092	1.08
1.0	63.11	4.31	4.75	-0.191	2.14
1.5	63.07	6.24	6.88	-0.329	3.07
2.0	63.08	7.7	8.53	-0.555	3.74
2.5	63.06	8.63	9.63	-0.880	4.12
2.0	63.05	9.19	10.41	-1.275	4.31
3.5	63.12	9.66	11.2	-1.689	4.4

D. Linear Yaw Plan Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*l/U-\delta_{av}$ (deg)	Γ_1 (deg)
0.5	63.07	2.06	2.27	-0.113	1.03
1.5	63.07	6.18	6.80	-0.340	3.08
2.0	63.07	8.24	9.08	-0.454	6.12
3.5	63.07	14.43	15.89	-0.794	7.21

E. Measurements

δ_{av} (deg)	r (deg/sec)	A_y (ft/sec ²)	Calculated * $r^* \ell / U - \delta_{av}$ (deg)	Measured **	
				A_y (ft/sec ²)	$r^* \ell / U - \delta$ (deg)
0.82	3.27	3.5	-0.206	3.5	-0.113
1.1	4.98	5.25	-0.165	5.25	-0.06
1.23	6.40	5.6	-0.029	6.3	-0.113
1.52	7.10	7.6	-0.187	7.93	-0.113
1.8	8.24	8.75	-0.254	8.94	-0.116
2.05	9.5	10.3	-0.267	10.27	-0.18
2.2	10.03	11.04	-0.318	10.93	-0.23
2.46	11.12	11.66	-0.373	11.63	-0.18
2.62	11.36	12.25	-0.488	12.4	-0.43
2.9	12.05	12.90	-0.639		
3.17	12.8	12.90	-0.768	12.68	-0.56
3.4	13.5	14.54	-0.867	14.0	-0.86

* Calculations based on the measured yaw rates, a forward speed of 63.07 ft/sec, and a wheelbase of 142 in.

** Measured values taken from reference (5).

It can be seen from Figs. 3.5 and 3.6 that within the range up to 2 degrees of front-wheel steering angle (equivalent to lateral acceleration of approximately 0.25 g), all four simulation models give practically the same predictions, and the predicted values agree very well with the measured data. Within the range between 2 and 4 degrees of front-wheel steering angle, the linear yaw plane model gives the best overall predictions of lateral acceleration and yaw rate of the tractor, among the four simulation models. For instance, at front-wheel steering angle $\delta_{av} = 3^\circ$, the differences between the measured lateral acceleration and the predicted ones using the linear yaw plane model, the Phase 4 model, the yaw/roll model and the TBS model are 3.7%, 10.3%, 19.9% and 20.7%, respectively.

Fig. 3.7 shows a comparison of the steady-state handling characteristics of the vehicle predicted using the four simulation models and those measured (5). It can be seen that up to a lateral acceleration of approximately 0.25 g, all four models give essentially the same predictions. Beyond lateral acceleration of 0.25 g, the yaw/roll model and the TBS model give the highest prediction of understeer level (or "understeer gradient"), while the linear yaw plane model gives the lowest prediction. It can also be noted that while the handling characteristics predicted by the Phase 4 model, the yaw/roll model, and the TBS model and the measured ones show similar trend, in quantitative terms there is a significant difference between them. It can, therefore, be said that the agreement between the measured and the predicted handling characteristics using the four models is, in general, poor for lateral acceleration above 0.15 g.

From Table 3.2, it can be seen that all the four models give similar predictions of the articulation angle between the tractor and semitrailer for front-wheel steering angle less than 3.0° . It should also be mentioned that the roll angles of the sprung masses of the tractor and semitrailer predicted by the yaw/roll model are practically the same, while those predicted using the Phase 4 model are noticeably different.

3.3 Vehicle Configuration 3

As can be seen from Table 2.1, the major differences between this vehicle and Vehicle Configurations 1 and 2 are the location of the fifth wheel, which is 14.35 in. ahead of the tractor rear suspension centre for Vehicle Configuration 3, the characteristics of the tires, roll stiffness of the fifth wheel, and the auxiliary roll stiffnesses of the tractor suspensions and the tandem suspensions of the semitrailer.

The steady-state steering responses of this vehicle were predicted using the four computer simulation models at a forward speed of 35.8 mph (52.5 ft/sec) on a dry, smooth asphalt surface. The predicted steady-state lateral accelerations and yaw rates as functions of front-wheel steering angle of the tractor are shown in Figs. 3.8 and 3.9, respectively. Based on the predictions, a handling diagram, illustrating the handling characteristics of the vehicle predicted using the four simulation models, is shown in Fig. 3.10. For this vehicle configuration, no measured data are available. Therefore, the results presented are primarily for illustrating the differences in the predictive ability of various computer simulation models. The predicted values at various front-wheel steering angles are also given in Table 3.3.

As can be seen from the results shown in Figs. 3.8 and 3.9 and in Table 3.3, all four simulation models give similar predictions of lateral acceleration and yaw rate up to front-wheel steering angle of approximately 2.6° (or equivalent to lateral acceleration of approximately 0.28 g). The difference between the highest value of lateral acceleration predicted using the TBS model and the lowest one predicted using the linear yaw plane model at front-wheel steering angle of 2.6° is approximately 10.6%.

5-Axle Tractor-Semitrailer (Conf.3)

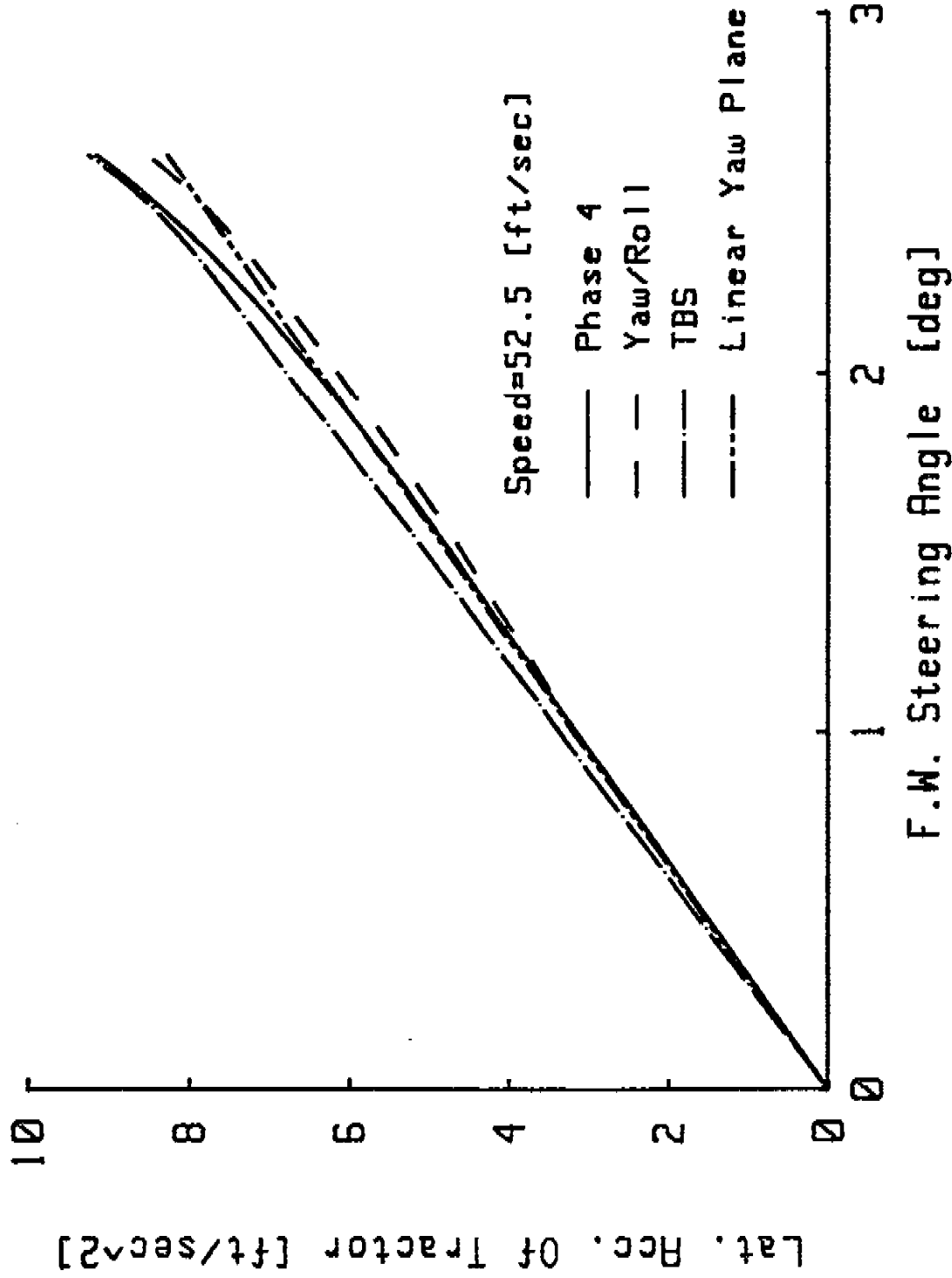
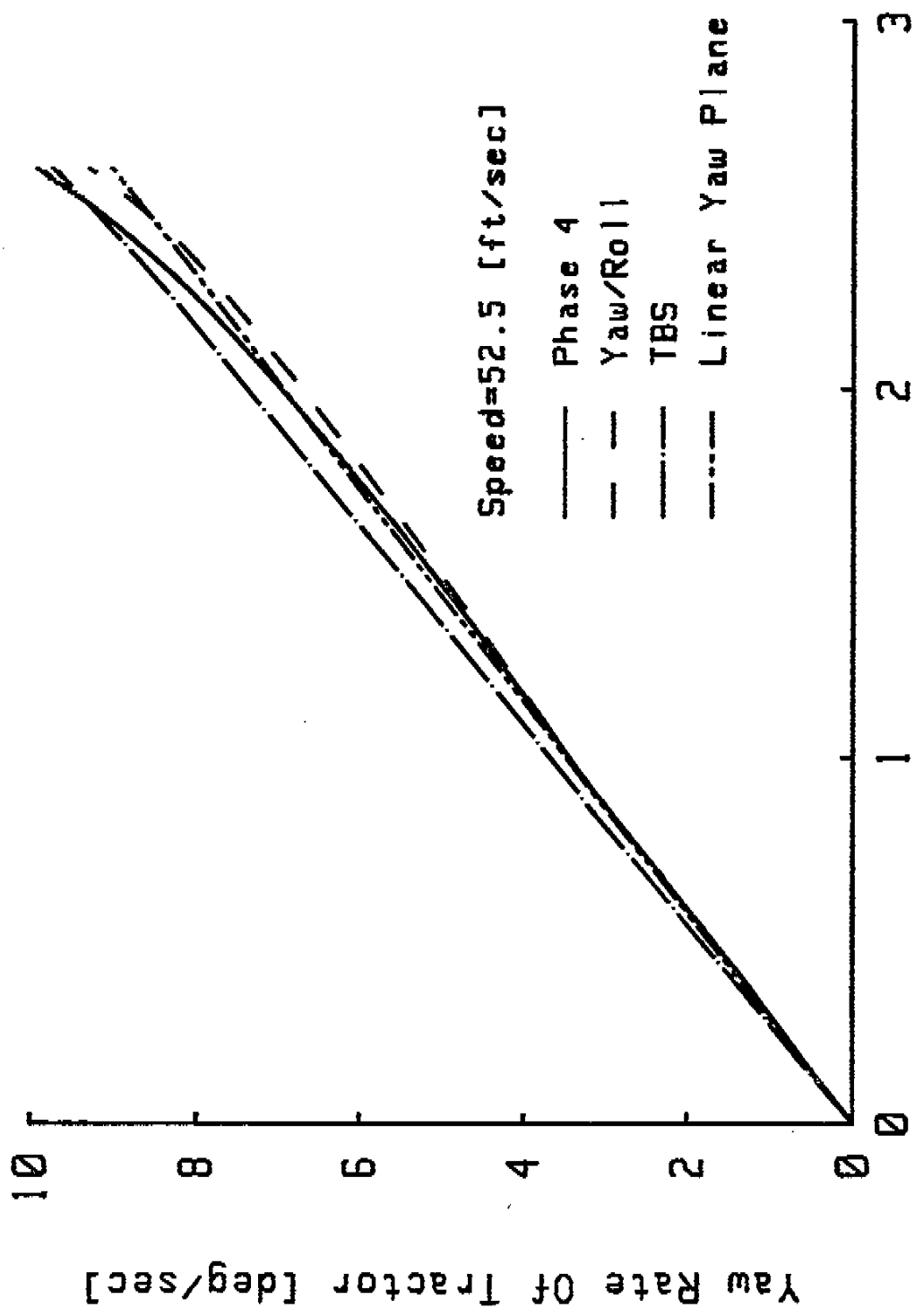


Fig. 3.8 Steady-state Lateral Acceleration Response to Steering Input of Vehicle Configuration 3 Predicted by Various Models

5-Axle Tractor-Semitrailer (Conf.3)



F.W. Steering Angle [deg]

Fig. 3.9 Steady-state Yaw Rate Response to Steering
Input of Vehicle Configuration 3
Predicted by Various Models

5-Axle Tractor-Semitrailer (Conf. 3)

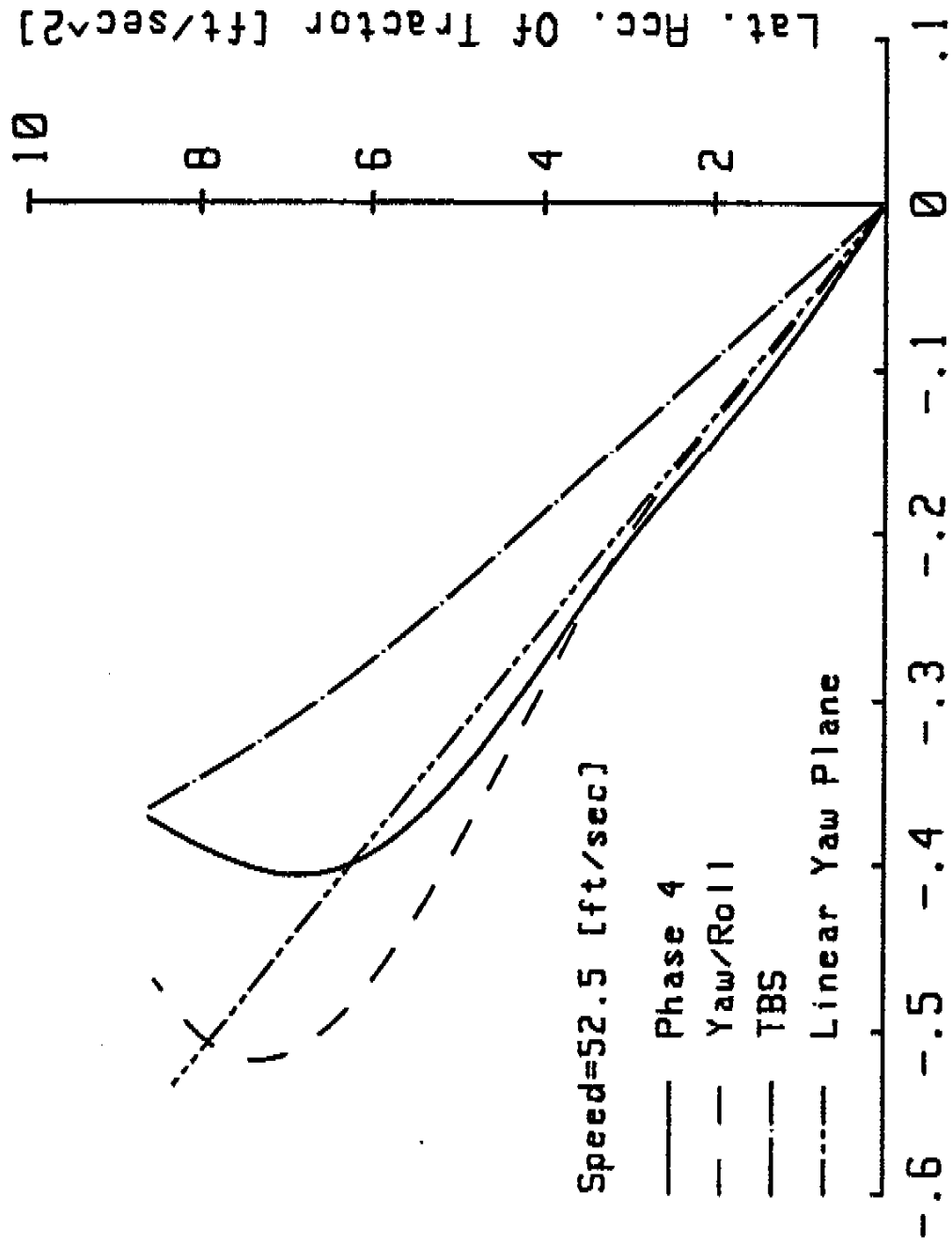


Fig. 3.10 Handling Characteristics of Vehicle Configuration 3

Predicted by Various Models

TABLE 3.3
VEHICLE CONFIGURATION 3

A. Phase 4 Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*l/U-\delta_{av}$ (deg)	ϕ_1 (deg)	ϕ_2 (deg)	Γ_1 (deg)
0.5	52.68	1.69	1.55	-0.115	-0.64	-0.57	1.11
1.0	52.7	3.44	3.15	-0.216	-1.56	-1.39	2.25
1.5	52.6	5.11	4.74	-0.332	-2.56	-2.22	3.33
2.0	52.5	6.98	6.43	-0.404	-3.41	-3.01	4.52
2.5	52.51	9.31	8.60	-0.372	-4.97	-4.5	6.06
2.6	52.49	9.95	9.16	-0.325	-6.63	-6.4	6.56

B. Yaw/Roll Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*l/U-\delta_{av}$ (deg)	ϕ_1 (deg)	ϕ_2 (deg)	Γ_1 (deg)
0.5	52.5	1.73	1.59	-0.105	-0.66	-0.7	1.15
1.0	52.5	3.44	3.148	-0.213	-1.33	-1.41	2.27
1.5	52.5	5.02	4.6	-0.352	-1.96	-2.07	3.31
2.0	52.5	6.73	6.17	-0.461	-2.67	-2.83	4.4
2.5	52.5	8.74	8.01	-0.502	-3.62	-3.85	5.64
2.6	52.5	9.32	8.53	-0.469	-4.09	-4.33	6.02

C. TBS Model

δ_{av} (Deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*l/U-\delta_{av}$ (deg)	Γ_1 (deg)
0.5	52.5	1.84	1.68	-0.079	1.21
1.0	52.5	3.68	3.37	-0.158	2.43
1.5	52.5	5.52	5.06	-0.238	3.64
2.0	52.58	7.4	6.8	-0.308	4.81
2.5	52.53	9.33	8.59	-0.367	5.65
2.6	52.5	9.76	9.27	-0.369	5.57

D. Linear Yaw Plane Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*l/U-\delta_{av}$ (deg)	Γ_1 (deg)
1.0	52.5	3.48	3.19	-0.204	2.29
2.0	52.5	6.96	6.37	-0.409	4.58
2.6	52.5	9.04	8.29	-0.533	5.9

From Fig. 3.10, it can be seen that up to lateral acceleration of approximately 0.15 g, the Phase 4 model, the yaw/roll model and the linear yaw plane model give similar predictions of the understeer level of the vehicle, whereas the TBS model predicts lower understeer level. Both the Phase 4 model and the yaw/roll model predict a transition from understeer to oversteer at a lateral acceleration of approximately 0.2 g, while the TBS model does not predict a transition below 0.25 g of lateral acceleration. As mentioned previously, since a linear tire model is used, the linear yaw plane model is unable to predict any variation of the handling behaviour of the vehicle with lateral acceleration, and the predicted understeer level remains constant.

From Table 3.3, it can be seen that the Phase 4 model gives higher prediction of the articulated angle between the tractor and semitrailer than the models at high front-wheel steering angles. It should also be mentioned that the roll angles of the sprung masses of the tractor and semitrailer predicted by the Phase 4 model are higher than those predicted by the yaw/roll model.

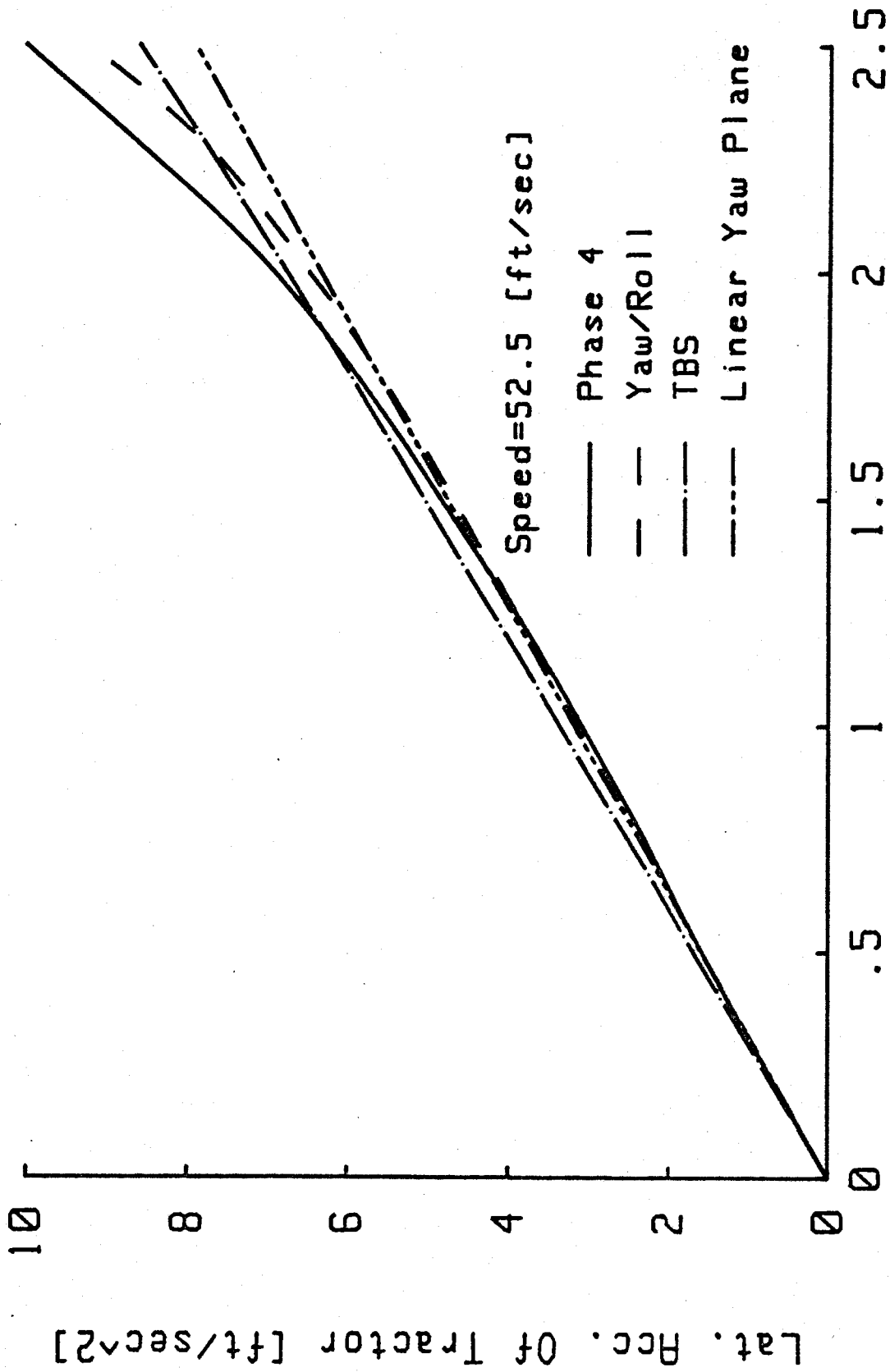
3.4 Vehicle Configuration 4

As shown in Table 2.1, the major differences between this vehicle and Vehicle Configuration 3 are the removal of the auxiliary roll-stiffening device from the tractor front suspension and the installation of a much stiffer roll-stiffening device on the tractor trailing tandem axle. The combined effect is the lowering of the understeer level of this vehicle, in comparison with Vehicle Configuration 3.

The steady-state lateral accelerations and yaw rates as functions of front-wheel steering angle of the tractor predicted using the four computer simulation models are shown in Fig. 3.11 and Fig. 3.12, respectively. The handling characteristics of the vehicle predicted by the computer simulation models are illustrated in Fig. 3.13. The predicted values are also listed in Table 3.4.

As can be seen from the predicted results shown in Figs. 3.11 and 3.12, and in Table 3.4, all four simulation models give essentially the same predictions of lateral acceleration and yaw rate up to front-wheel steering angle of 2 degrees, or lateral acceleration of approximately 0.2 g. Beyond that the differences between the predicted values obtained using the four models increase noticeably. For instance, at a front-wheel steering angle of 2.5 degrees, the differences between the predicted lateral accelerations using the Phase 4 model and those using the yaw/roll model, the TBS model and the linear yaw plane model are 7.5%, 14%, and 20.9%, respectively.

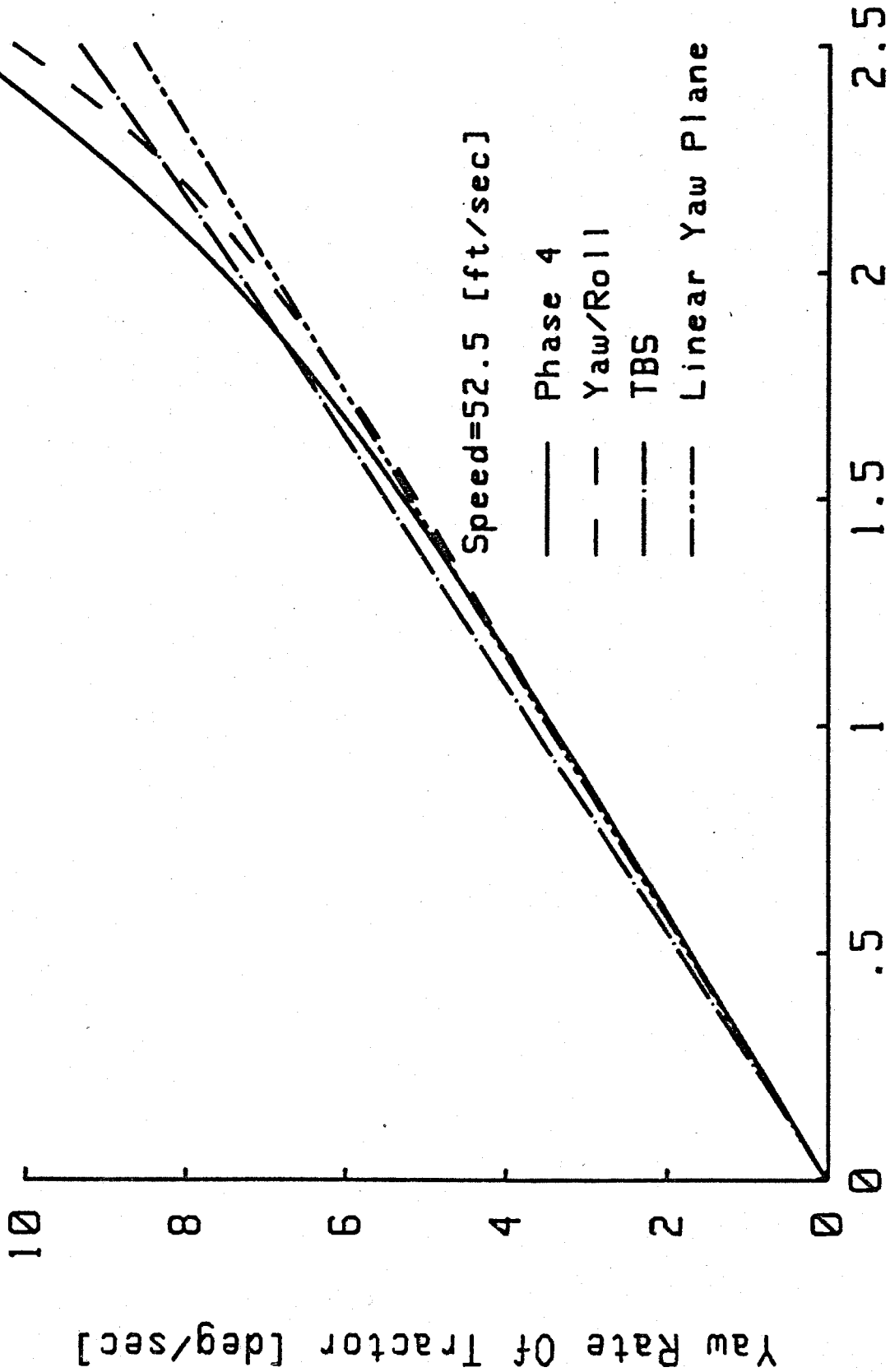
5-Axle Tractor-Semitrailer (Conf. 4)



F.W. Steering Angle [deg]

Fig. 3.11 Steady-state Lateral Acceleration Response to Steering Input of Vehicle Configuration 4 Predicted by Various Models

5-Axle Tractor-Semitrailer (Conf. 4)



F.W. Steering Angle [deg]

Fig. 3.12 Steady-state Yaw Rate Response to Steering Input of Vehicle Configuration 4
Predicted by Various Models

5-Axle Tractor-Semitrailer (Conf.4)

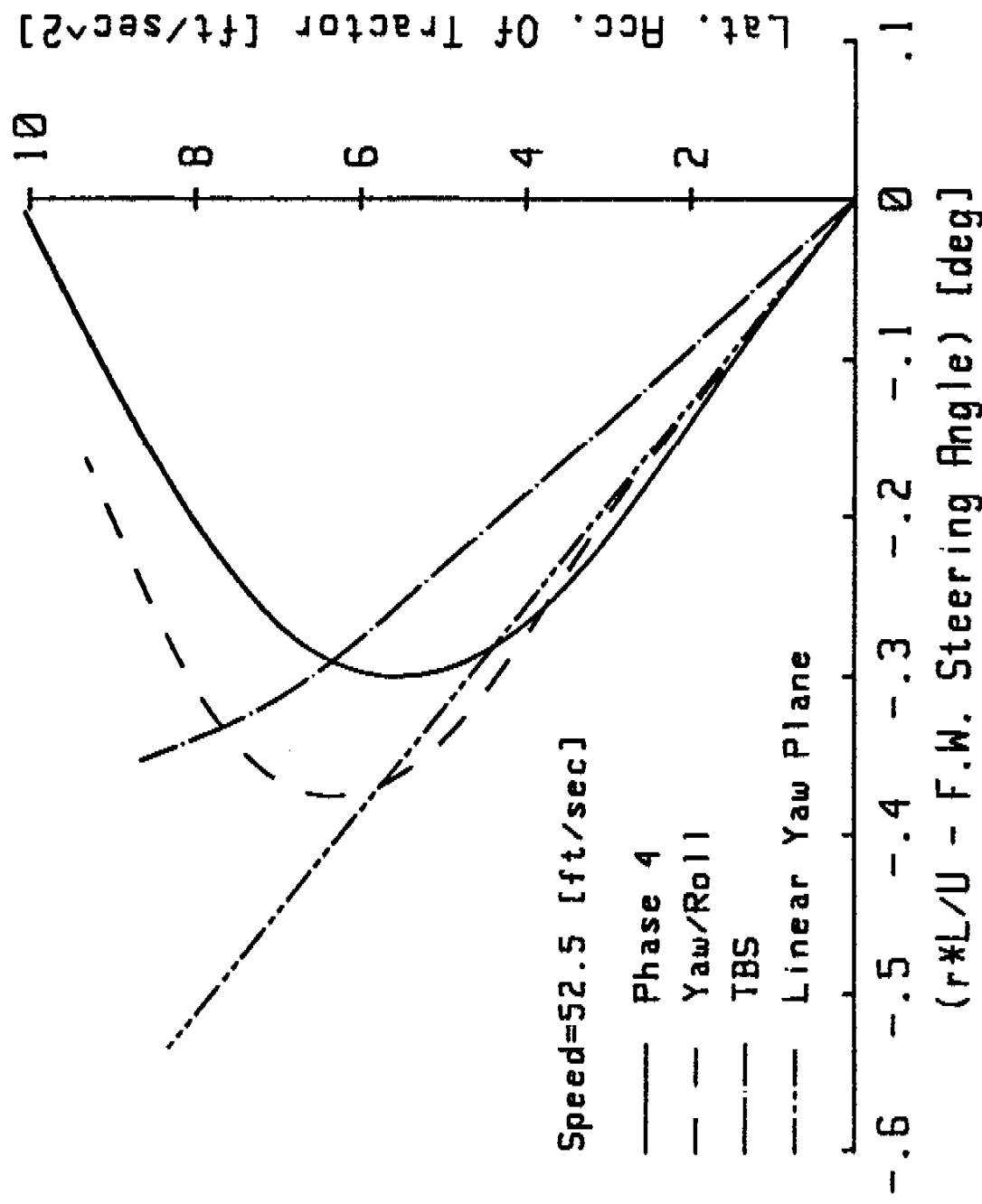


Fig. 3.13 Handling Characteristics of Vehicle Configuration 4
 Predicted by Various Models

TABLE 3.4
VEHICLE CONFIGURATION 4

A. Phase 4 Model

δ_{av} (deg)	U (ft/sec)	r (deg)	A_y (ft/sec ²)	$r^*l/U-\delta_{av}$ (deg)	ϕ_1 (deg)	ϕ_2 (deg)	Γ_1 (deg)
0.5	52.54	1.71	1.58	-0.109	-0.75	-0.59	1.12
1.0	52.76	3.43	3.08	-0.219	-1.69	-1.37	2.28
1.5	52.59	5.30	4.85	-0.291	-2.49	-2.08	3.52
1.75	52.6	6.36	5.82	-0.299	-2.07	-2.51	4.20
2.0	52.61	7.59	6.96	-0.268	-3.58	-3.04	5.04
2.25	52.51	9.10	8.44	-0.199	-4.35	-3.72	6.11
2.5	52.5	10.90	10.06	-0.008	-8.16	-7.90	7.41

B. Yaw/Roll Model

δ_{av} (deg)	U (ft/sec)	r (deg)	A_y (ft/sec ²)	$r^*l/U-\delta_{av}$ (deg)	ϕ_1 (deg)	ϕ_2 (deg)	Γ_1 (deg)
0.5	52.5	1.73	1.58	-0.105	-0.6	-0.65	1.15
1.0	52.5	3.45	3.16	-0.211	-1.22	-1.33	2.30
1.5	52.5	5.14	4.70	-0.325	-1.83	-1.99	3.43
1.75	52.5	6.06	5.54	-0.365	-2.16	-2.35	4.04
2.0	52.5	7.11	6.52	-0.375	-2.57	-2.80	4.75
2.25	52.5	8.39	7.66	-0.332	-3.09	-3.39	5.62
2.5	52.5	10.22	9.31	-0.164	-4.18	-4.59	6.89

C. TBS Model

δ_{av} (deg)	U (ft/sec)	r (deg)	A_y (ft/sec ²)	$r^*l/U - \delta_{av}$ (deg)	Γ_1 (deg)
0.5	52.5	1.84	1.69	- 0.079	1.21
1.0	52.5	3.68	3.37	- 0.158	2.43
1.5	52.5	5.53	5.07	- 0.236	3.64
2.0	52.5	7.4	6.8	- 0.308	4.83
2.5	52.52	9.39	8.65	- 0.353	5.66

D. Linear Yaw Plane Model

δ_{av} (deg)	U (ft/sec)	r (deg)	A_y (ft/sec ²)	$r^*l/U - \delta_{av}$ (deg)	Γ_1 (deg)
1.0	52.5	3.48	3.19	- 0.204	2.29
2.0	52.5	6.96	6.37	- 0.409	4.58
2.5	52.5	8.7	7.96	- 0.511	5.72
2.6	52.5	9.04	8.29	- 0.537	5.9

From Fig. 3.13, it can be seen that up to a lateral acceleration of approximately 0.125 g, the Phase 4 model, the yaw/roll model and the linear yaw plane model give essentially the same predictions of the understeer level of the vehicle, whereas the TBS model predicts a lower level of understeer. The Phase 4 model predicts a transition from understeer to oversteer at a lateral acceleration of approximately 0.175 g, while the yaw/roll model predicts the transition occurring at a slightly higher lateral acceleration of approximately 0.2 g. The TBS model does not predict a transition below 0.28 g of lateral acceleration, and as mentioned previously, the linear yaw plane model is unable to predict any variation of the handling behaviour of the vehicle with lateral acceleration.

From Table 3.4, it can be seen that the TBS model and the linear yaw plane model give similar predictions of the articulation angle. The Phase 4 model and the yaw/roll model however, generally give higher predictions of articulation angle than the other two models. It can be also noted that the roll angles of the sprung masses of the tractor and semitrailer predicted by the Phase 4 model are generally higher than those predicted by the yaw/roll model, when the front-wheel steering angle is greater than 2 degrees.

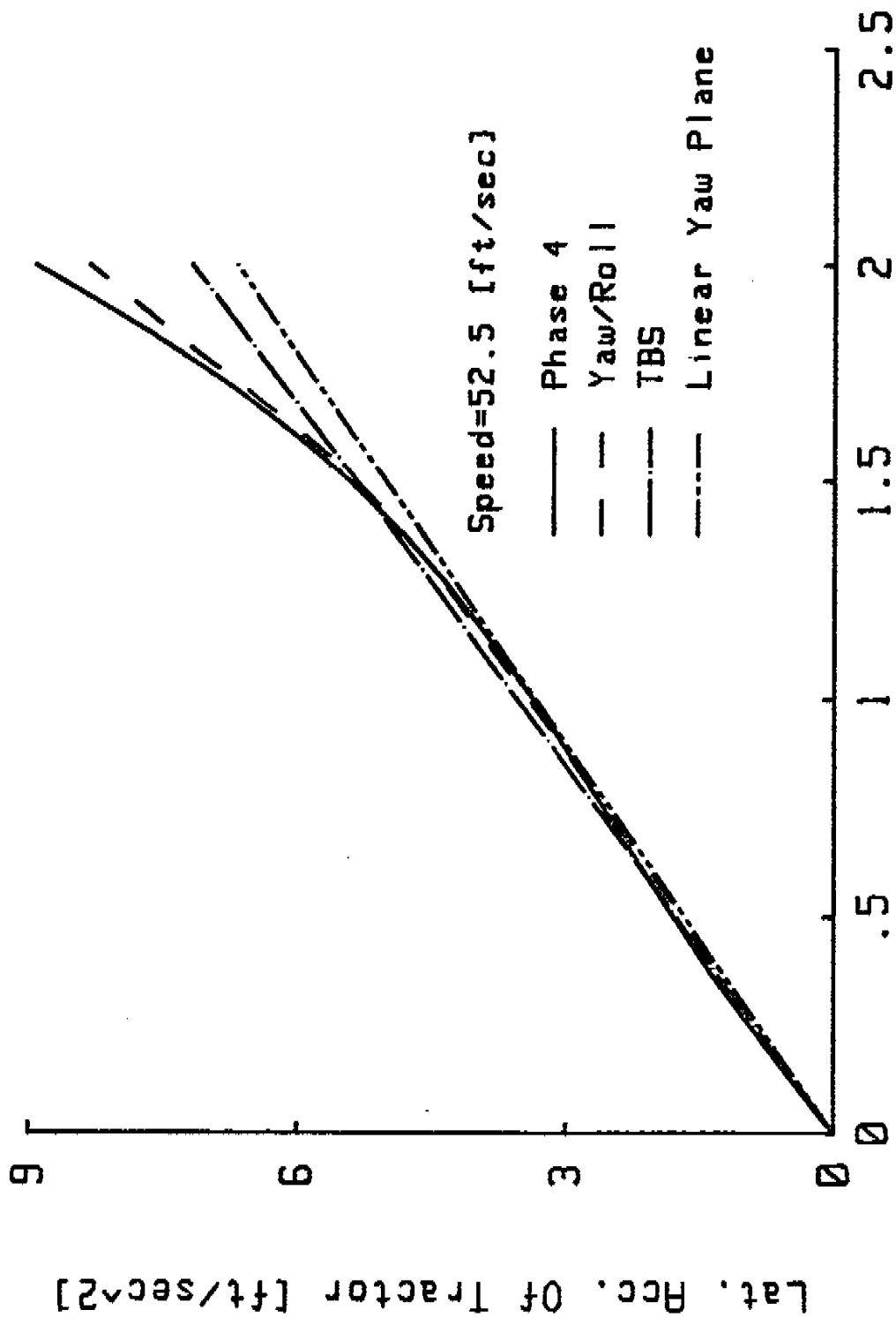
3.5 Vehicle Configuration 5

It can be seen from Table 2.1, the basic difference between this vehicle and Vehicle Configuration 4 is the location of the fifth wheel. In this vehicle, the fifth wheel is situated at the centre of the rear suspension of the tractor, whereas in Vehicle Configuration 4, the fifth wheel is located ahead of the tractor rear suspension centre. The rearward shift of the fifth wheel location generally reduces the under-steer level of the tractor.

The steady-state lateral accelerations and yaw rates as functions of front-wheel steering angle of the tractor predicted using the four computer simulation models are shown in Figs. 3.14 and 3.15 respectively. The handling characteristics of the vehicle predicted by the computer simulation models are shown in Fig. 3.16. The predicted values are also listed in Table 3.5.

As can be seen from the predicted results shown in Figs. 3.14 and 3.15 and in Table 3.5, all four simulation models give essentially the same predictions of lateral acceleration and yaw rate up to front-wheel steering angle of 1.5 degrees (or lateral acceleration of 0.15 g approximately). Beyond that the differences between the predicted values obtained using the four models increase noticeably. For instance, at front-wheel steering angle of 2.0 degrees, the differences between the predicted lateral acceleration using the Phase 4 model and those using the yaw/roll model, the TBS model and the linear yaw plane model are 6.8%, 19.6%, and 25.2% respectively.

5-Axle Tractor-Semitrailer (Conf.5)



F.W. Steering Angle [deg]

Fig. 3.14 Steady-state lateral acceleration response to steering input of Vehicle Configuration 5 predicted by various models

5-Axle Tractor-Semitrailer (Conf.5)

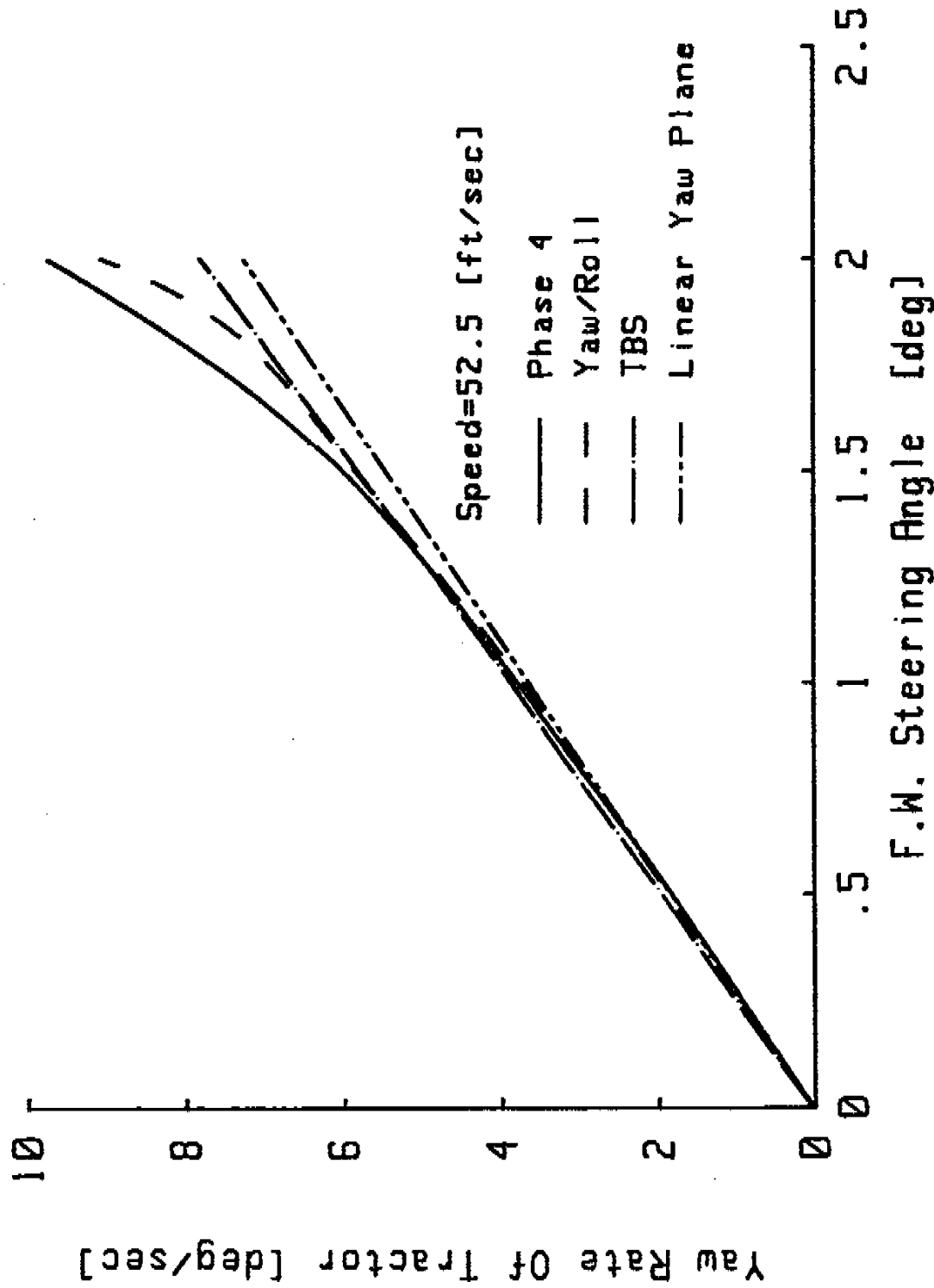


Fig. 3.15 Steady-state yaw rate response to steering input of Vehicle Configuration 5
 Predicted by various models

5-Axle Tractor-Semitrailer (Conf.5)

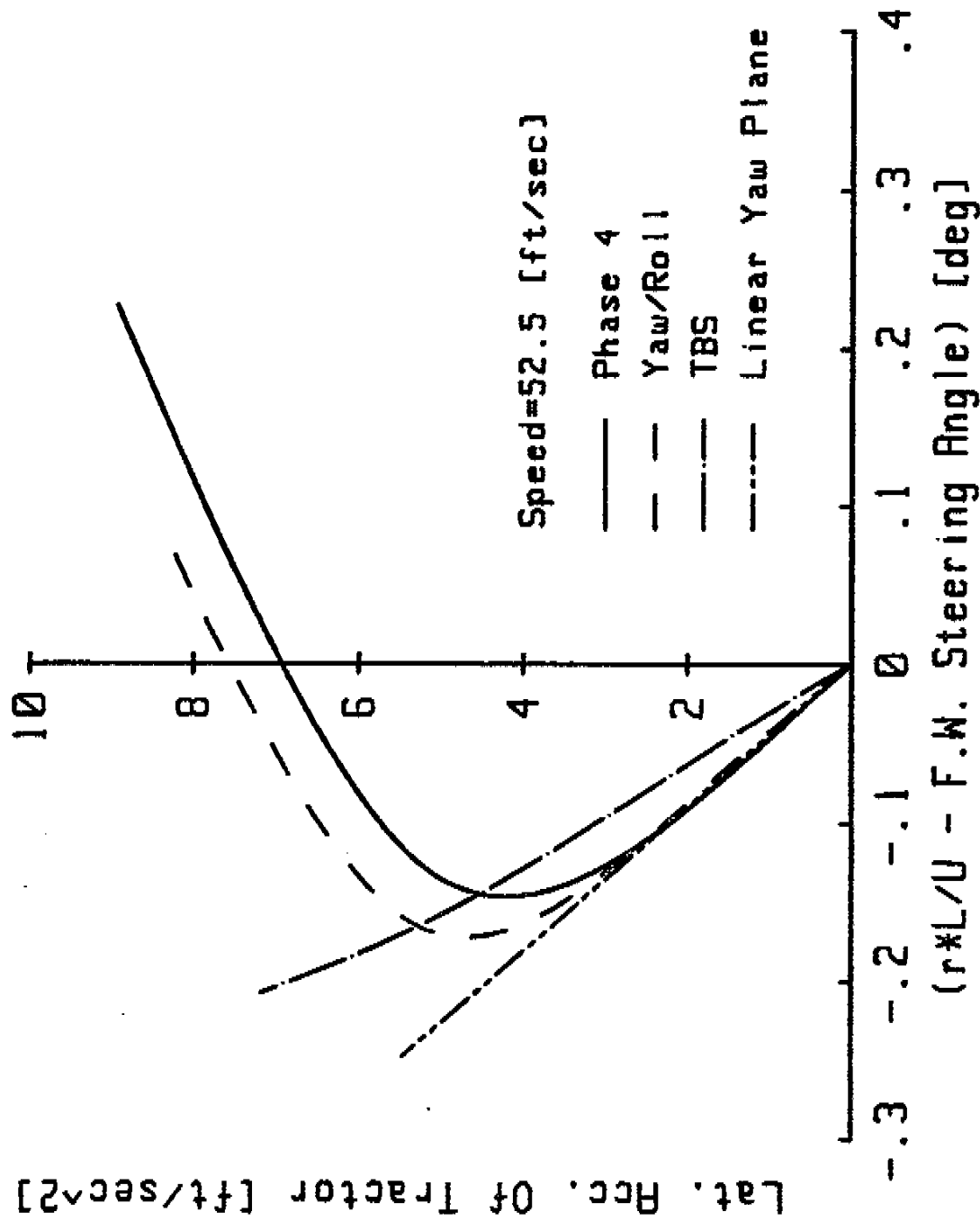


Fig. 3.16 Handling characteristics of Vehicle Configuration 5 predicted by various models

TABLE 3.5
VEHICLE CONFIGURATION 5

A. Phase 4 Model

δ_{av} (deg)	U (ft/sec)	r (deg)	A_y (ft/sec ²)	$r^{*l}/U-\delta_{av}$ (deg)	ϕ_1 (deg)	ϕ_2 (deg)	Γ_1 (deg)
0.5	52.5	1.82	1.80	-0.084	-0.92	-0.73	1.27
1.0	52.71	3.79	3.37	-0.137	-1.81	-1.49	2.62
1.5	52.51	6.01	5.42	-0.126	-2.73	-2.40	4.23
1.75	52.5	7.64	6.93	-0.0037	-3.34	-2.99	5.31
2.0	52.52	9.75	8.94	+0.228	-4.51	-4.02	6.82

B. Yaw/Roll Model

δ_{av} (deg)	U (ft/sec)	r (deg)	A_y (ft/sec ²)	$r^{*l}/U-\delta_{av}$ (deg)	ϕ_1 (deg)	ϕ_2 (deg)	Γ_1 (deg)
0.5	52.5	1.86	1.70	-0.075	-0.64	-0.70	1.29
1.0	52.5	3.73	3.41	-0.147	-1.3	-1.42	2.59
1.5	52.5	5.85	5.35	-0.163	-2.04	-2.23	4.07
1.75	52.5	6.95	6.80	-0.161	-2.55	-2.85	5.1
2.0	52.5	9.10	8.33	+0.08	-3.32	-3.64	6.36

C. TBS Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*l/U - \delta_{av}$ (deg)	Γ_1 (deg)
0.5	52.5	1.94	1.77	- 0.057	1.30
1.0	52.5	3.87	3.55	- 0.115	2.59
1.5	52.51	5.83	5.35	- 0.168	3.90
1.75	52.5	6.83	6.26	- 0.189	4.53
2.0	52.49	7.84	7.19	- 0.208	5.15

D. Linear Yaw Plane Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*l/U - \delta_{av}$ (deg)	Γ_1 (deg)
0.5	52.5	1.82	1.67	- 0.084	1.22
1.0	52.5	3.65	3.34	- 0.166	2.44
2.0	52.5	7.3	6.69	- 0.331	4.89

It can be seen from Fig. 3.16 that up to lateral acceleration of 0.1 g, the Phase 4 model, the yaw/roll model and the linear yaw plane model give practically the same prediction of understeer level, whereas the TBS model predicts lower level of understeer. The Phase 4 model predicts a transition from understeer to oversteer at a lateral acceleration of approximately 0.125 g, while the yaw/roll model predicts the transition occurring at a slightly higher lateral acceleration. The TBS model does not predict a transition below 0.25 g of lateral acceleration, while the linear yaw plane model is unable to predict any changes in the handling behaviour of the vehicle.

From Table 3.5, it can be noted that there are noticeable differences between the articulation angles predicted using the four models. The Phase 4 model gives the highest prediction, while the linear yaw plane model gives the lowest prediction. It can also be seen that the roll angles of the sprung masses of the tractor and semitrailer predicted using the Phase 4 model are generally higher than those predicted using the yaw/roll model.

3.6 Vehicle Configuration 6

This vehicle is a tractor-semitrailer-full trailer combination. The steady-state steering response of this vehicle configuration was simulated using the Phase 4 model, the yaw/roll model and the linear yaw plane model at a forward speed of 21.5 mph (31.5 ft/sec). The TBS model was not used in the simulation, as it is not designed for simulating this type of vehicle combination in its present form.

The steady-state lateral accelerations and yaw rates as functions of front-wheel steering angle of the tractor predicted using the three computer simulation models are shown in Figs. 3.17 and 3.18, respectively. The handling characteristics of the vehicle predicted using the various models are illustrated in Fig. 3.19. The predicted values are also listed in Table 3.6.

As can be seen from Figs. 3.17 and 3.18 and from Table 3.6, all three simulation models give practically the same predictions of lateral acceleration and yaw rate of the tractor up to front-wheel steering angle of 4.5 degrees (or lateral acceleration of approximately 0.25 g). The differences between the lateral acceleration predicted by the Phase 4 model and those by the yaw/roll model and the linear yaw plane model at front-wheel steering angle of 4.5 degrees are only 0.5 % and 4.7 % respectively.

5-Axle Double/27-Ft Trailers (Conf.6)

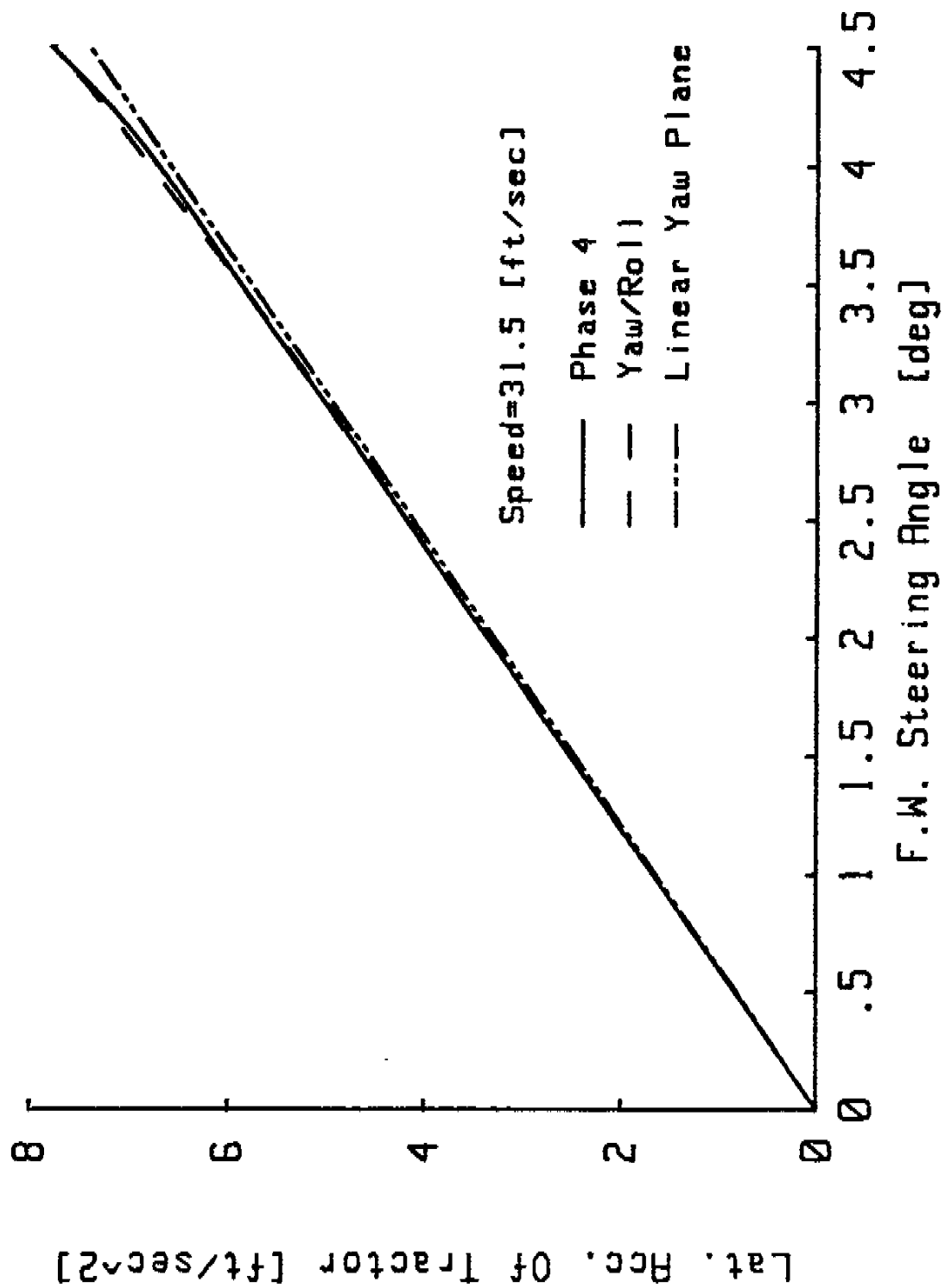


Fig. 3.17 Steady-state lateral acceleration response to steering input of Vehicle Configuration 6 predicted by various models

5-Axle Double/27-Ft Trailers (Conf. 6)

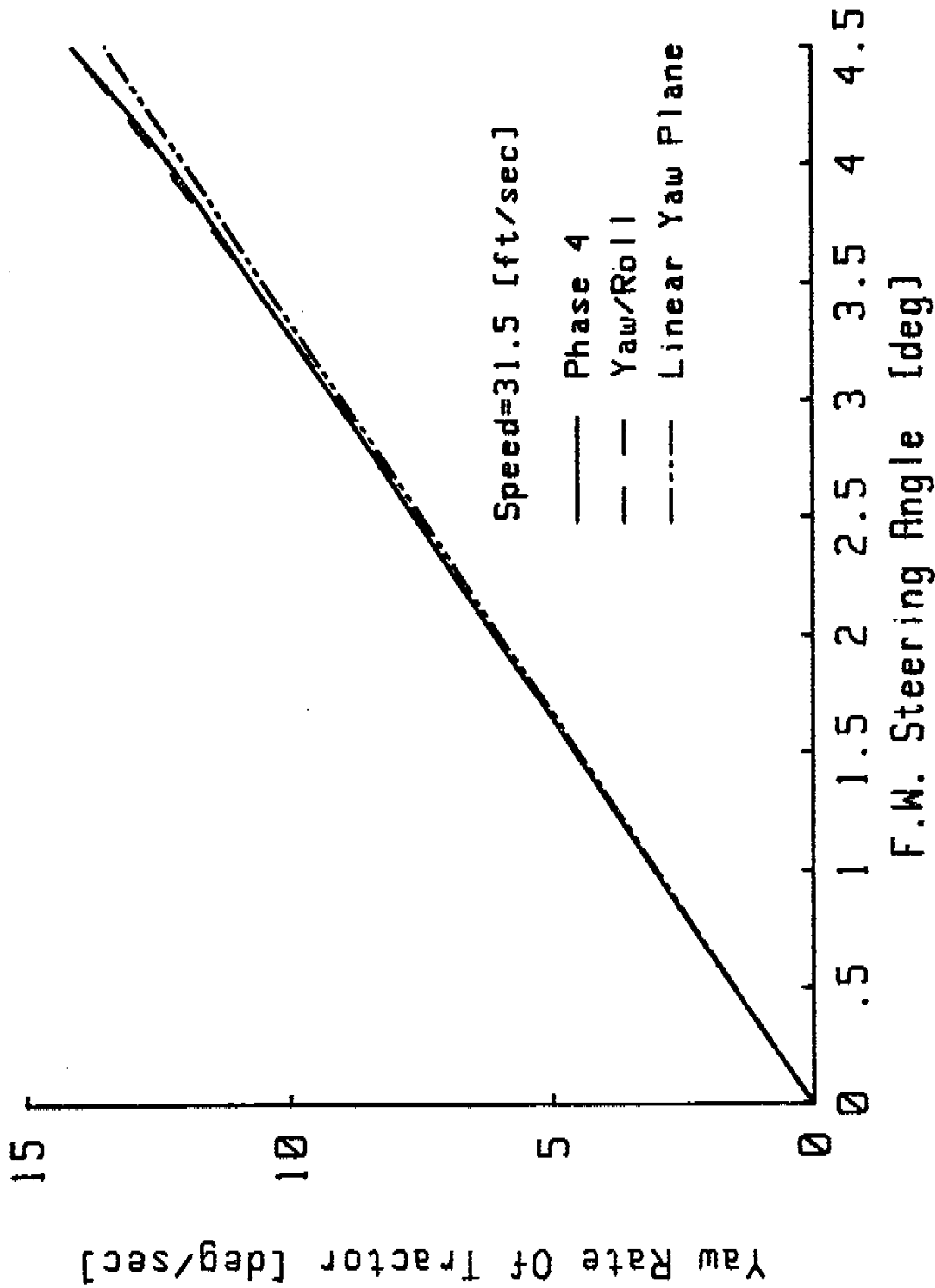


Fig. 3.10 Steady-state yaw rate response to steering input of Vehicle Configuration 6 predicted by various models

5-Axle Double/27-Ft Trailers (Conf. 6)

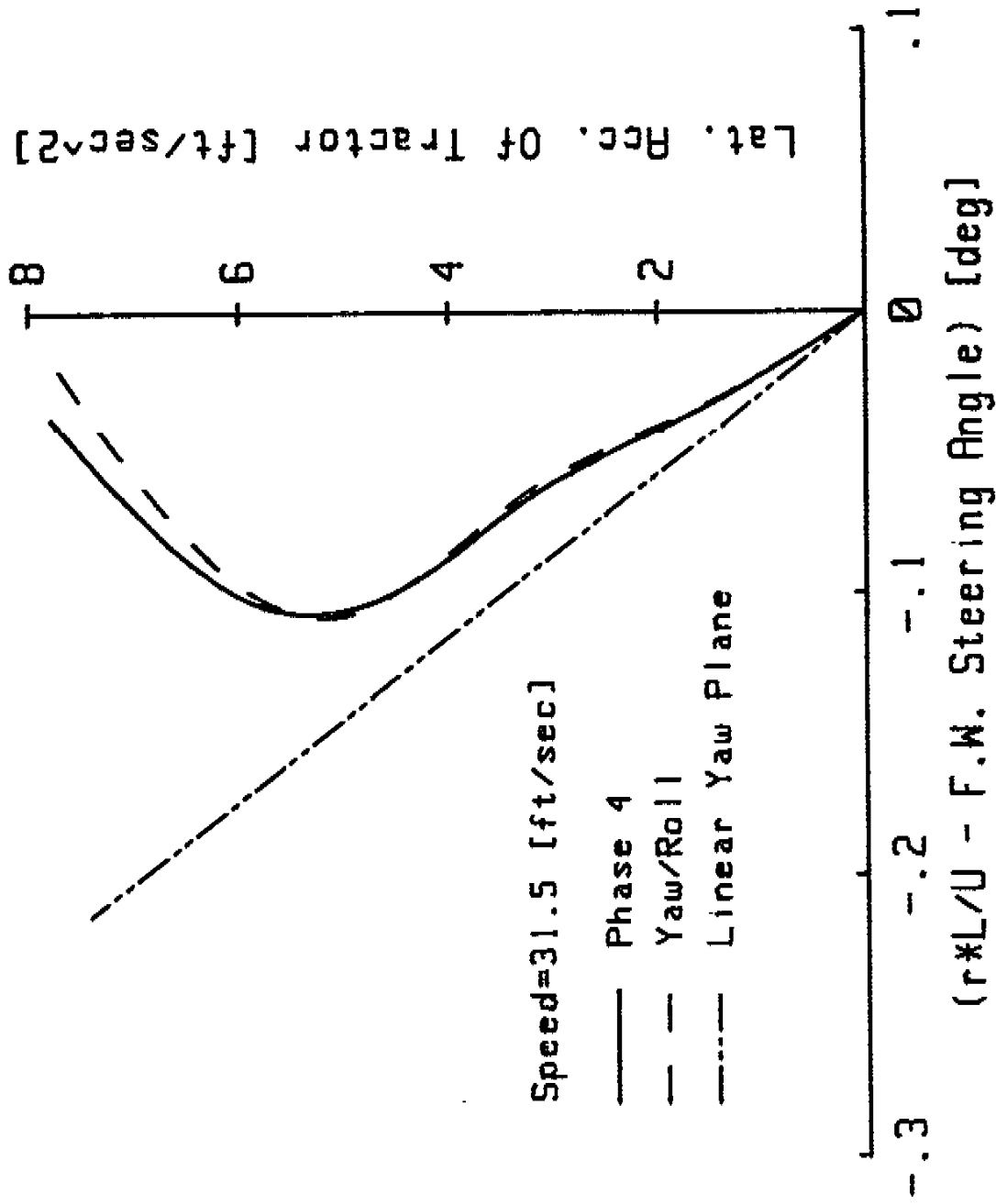


Fig. 3.19 Handling characteristics of Vehicle Configuration 6 predicted by various models

TABLE 3.6
VEHICLE CONFIGURATION 6

A. Phase 4 Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*z/U-\delta_{av}$ (deg)	ϕ_1 (deg)	ϕ_2 (deg)	ϕ_3 (deg)	Γ_1 (deg)	Γ_2 (deg)
1.0	31.53	3.04	4.67	- 0.036	- 0.51	- 0.43	- 0.35	1.93	2.89
2.0	31.55	6.09	3.36	- 0.069	- 1.25	- 1.09	- 0.88	3.880	5.83
2.5	31.7	7.63	4.19	- 0.093	- 1.63	- 1.42	- 1.20	4.88	7.47
3.0	31.51	9.14	5.03	- 0.098	- 2.07	- 1.79	- 1.48	5.82	8.99
3.5	31.5	10.7	5.88	- 0.103	- 2.45	- 2.15	- 1.79	6.79	10.56
4.0	31.5	12.28	6.72	- 0.101	- 2.94	- 2.61	- 2.10	7.82	14.04
4.5	31.68	14.14	7.80	- 0.037	- 3.96	- 3.14	- 2.60	8.90	

B. Yaw/Roll Model

δ_{av} (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r^*z/U-\delta_{av}$ (deg)	ϕ_1 (deg)	ϕ_2 (deg)	ϕ_3 (deg)	Γ_1 (deg)	Γ_2 (deg)
1.0	31.5	3.04	1.67	- 0.035	- 0.65	- 0.68	- 0.55	1.95	2.9
2.0	31.5	6.09	3.35	- 0.067	- 1.31	- 1.36	- 1.12	3.9	5.82
2.5	31.5	7.62	4.19	- 0.081	- 1.64	- 1.71	- 1.41	4.87	7.30
3.0	31.5	9.11	5.01	- 0.108	- 1.97	- 2.05	- 1.68	5.81	8.75
3.5	31.5	10.71	5.88	- 0.1	- 2.34	- 2.44	- 2.06	6.80	10.58
4.0	31.5	12.39	6.81	- 0.067	- 2.76	- 2.87	- 2.37	7.82	12.29
4.5	31.5	14.12	7.76	- 0.0175	- 3.18	- 3.32	- 2.74	8.88	14.07

C. Linear Yaw Plane Model

δ (deg)	U (ft/sec)	r (deg/sec)	A_y (ft/sec ²)	$r \cdot l / U - \delta_{av}$ (deg)	Γ_1 (deg)	Γ_2 (deg)
1.0	31.5	3.0	1.65	- 0.048	1.91	2.91
2.0	31.5	6.0	3.3	- 0.095	3.82	5.84
3.0	31.5	8.99	4.95	- 0.146	5.74	8.86
4.5	31.5	13.5	7.43	- 0.214	8.59	13.09

NOTE: ϕ_1 - roll angle of the tractor
 ϕ_2 - roll angle of the semitrailer
 ϕ_3 - roll angle of the full-trailer
 Γ_1 - articulation angle between the tractor and the semitrailer
 Γ_2 - articulation angle between the semitrailer and the full-trailer

As can be seen from Fig. 3.19, the Phase 4 model and the yaw/roll model give essentially the same prediction of the handling characteristics of the vehicle. Both models predict a transition from understeer to oversteer at a lateral acceleration of approximately 0.15 g. The linear yaw plane model predicts a higher level of understeer than the other two models. As mentioned previously, the linear yaw plane model is unable to predict changes in the handling behaviour of the vehicle.

From Table 3.6, it can be seen that all three models give similar predictions of the articulation angle between the tractor and semitrailer and that between the semitrailer and full-trailer. It can also be noted that the Phase 4 model and the yaw/roll model give similar predictions of the roll angles of the sprung masses of the tractor, semitrailer and full-trailer.

4. A COMPARISON OF VARIOUS COMPUTER SIMULATION MODELS FOR PREDICTING STEERING RESPONSES IN LANE-CHANGE TYPE TRANSIENT MANOEUVRES

This section examines the abilities of various computer simulation models in predicting the directional response to steering in lane-change (obstacle-avoidance) type transient manoeuvres. The lateral acceleration, yaw rate and articulation angle of Vehicle Configuration 1 in a moderate lane-change type transient manoeuvre were predicted using the Phase 4 model, the yaw/roll model, the TBS model and the linear yaw plane model. The simulated results were compared with the measured data reported in reference (7). In addition, the directional responses to steering of Vehicle Configurations 3 and 6 in a more severe lane-change manoeuvre were also simulated using the four computer simulation models. The results of this study provide quantitative information for evaluation the abilities of various computer models for simulating the transient directional behaviour of articulated vehicles.

4.1 Steering Response of Vehicle Configuration 1 in a Lane-Change Manoeuvre

The transient directional response to steering input of Vehicle Configuration 1 was predicted using the four computer simulation models. In the simulations, the left and right front-wheel angles as functions of time measured during a test, shown in Fig. 4.1, were used as inputs (7). The tractor lateral acceleration, semitrailer lateral acceleration, tractor yaw rate, semitrailer yaw rate, and articulation angle of Vehicle Configuration 1 as functions of time during the lane-change manoeuvre, at a forward speed of 43 mph (63.04 ft/sec), were predicted using the four models, and are shown in Figs. 4.2, 4.3, 4.4, 4.5 and 4.6, respectively. For comparison, the measured data reported in reference (7) were also shown in the figures.

It can be seen that the responses of the tractor and semitrailer predicted by the four models generally follow the same trend as that measured. However, there are differences between the predicted peak values and the measured ones. For instance, the differences between the measured peak value of tractor lateral acceleration and those predicted using the Phase 4 model, the yaw/roll model, the TBS model and the linear yaw plane model are approximately 16%, 10%, 33% and 46%, respectively, as shown in Fig. 4.2. The agreement between the measured peak value of semitrailer lateral acceleration and those predicted is better than that for the tractor lateral acceleration. The differences between the measured peak value of semitrailer lateral acceleration and those predicted using the Phase 4 model, the yaw/roll model, the TBS model and the linear yaw plane model are approximately 20%, 8%, 12% and 20%, respectively, as can be seen from Fig. 4.3.

Measured Front Wheel Steering Inputs

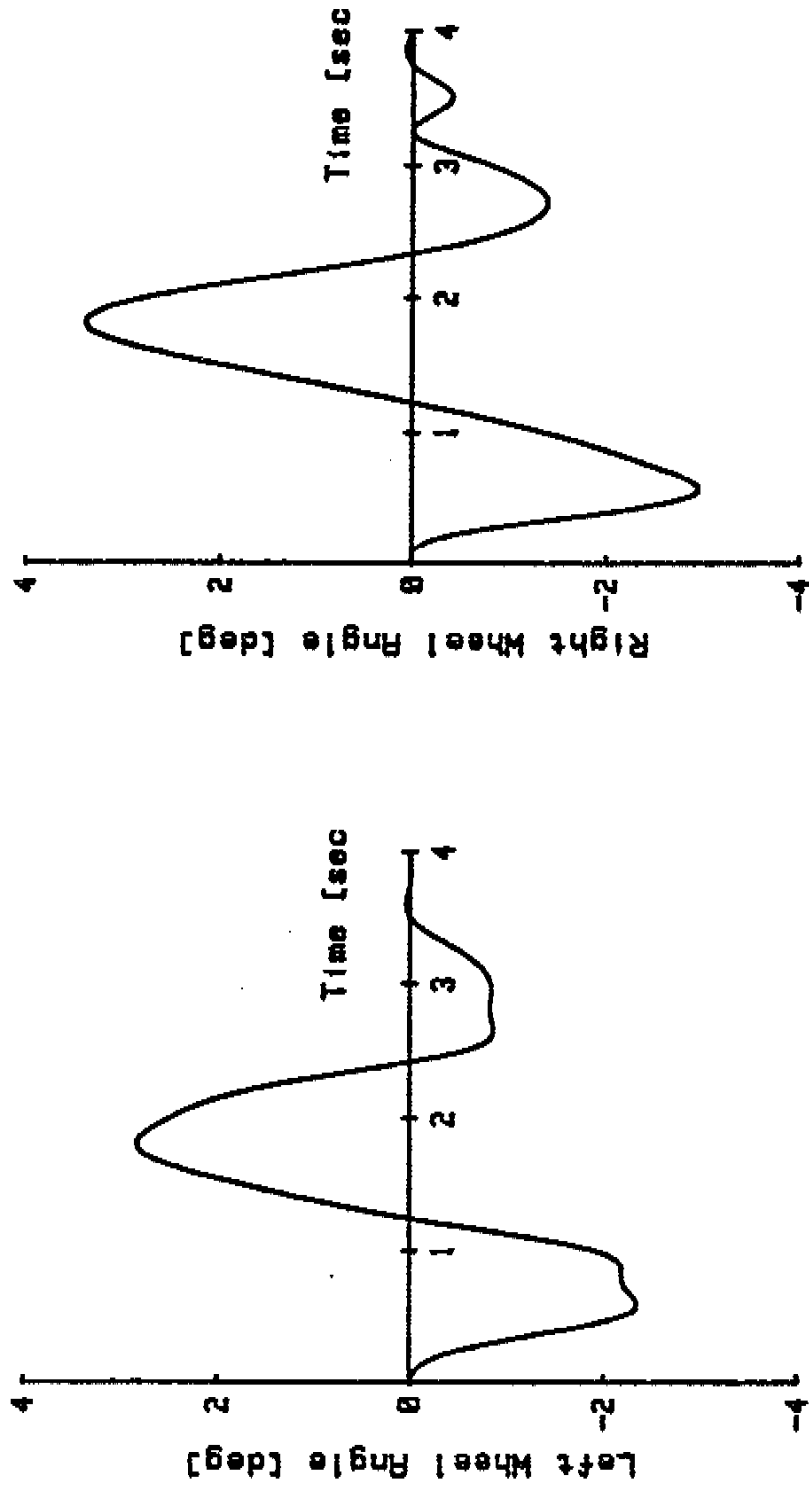


Fig. 4.1 Front-wheel steering inputs to the simulation of moderate lane-change manoeuvres

5-Axle Tractor-Semitrailer (Conf.1)

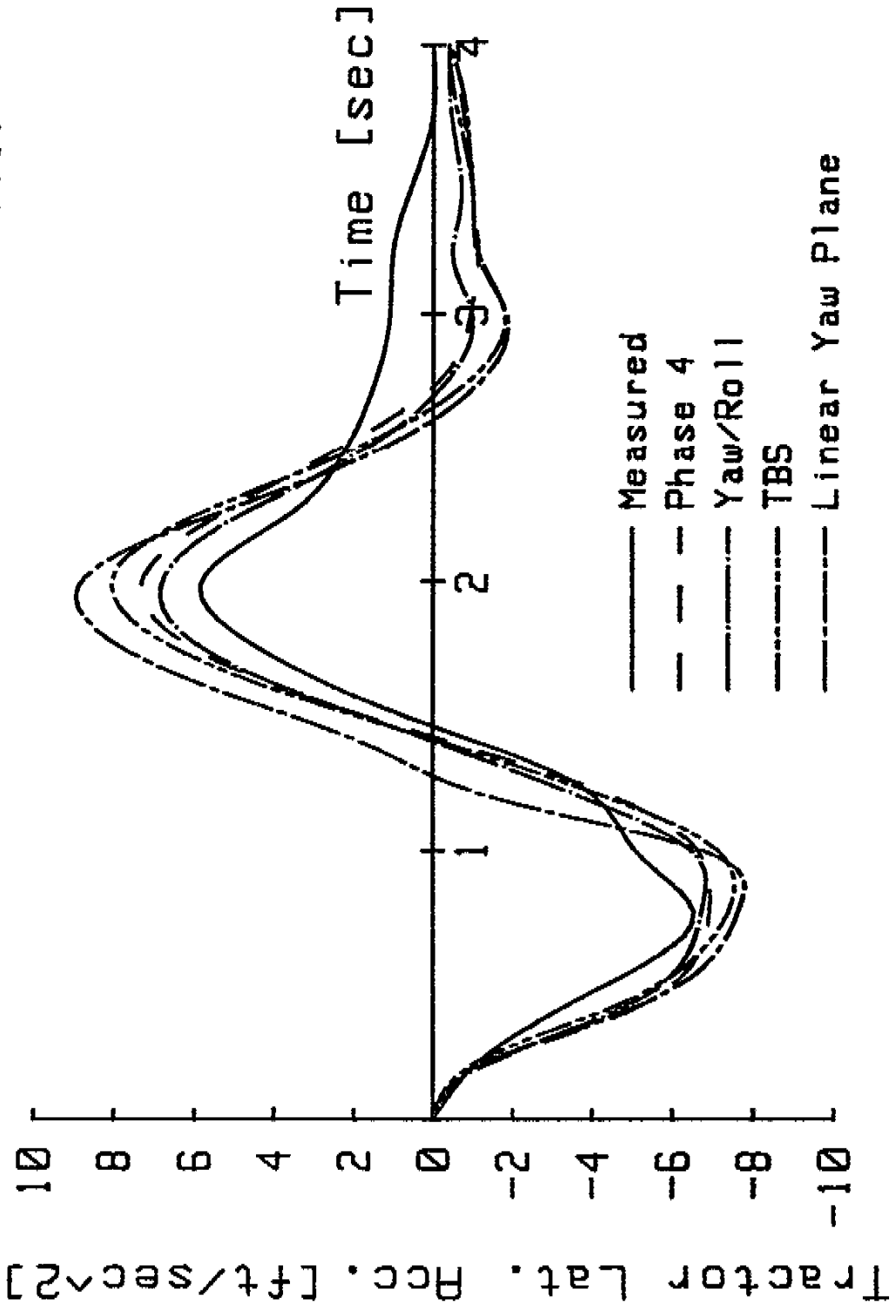


Fig. 4.2 Variation of tractor lateral acceleration with time of Vehicle Configuration 1 in a lane-change manoeuvre predicted by various models

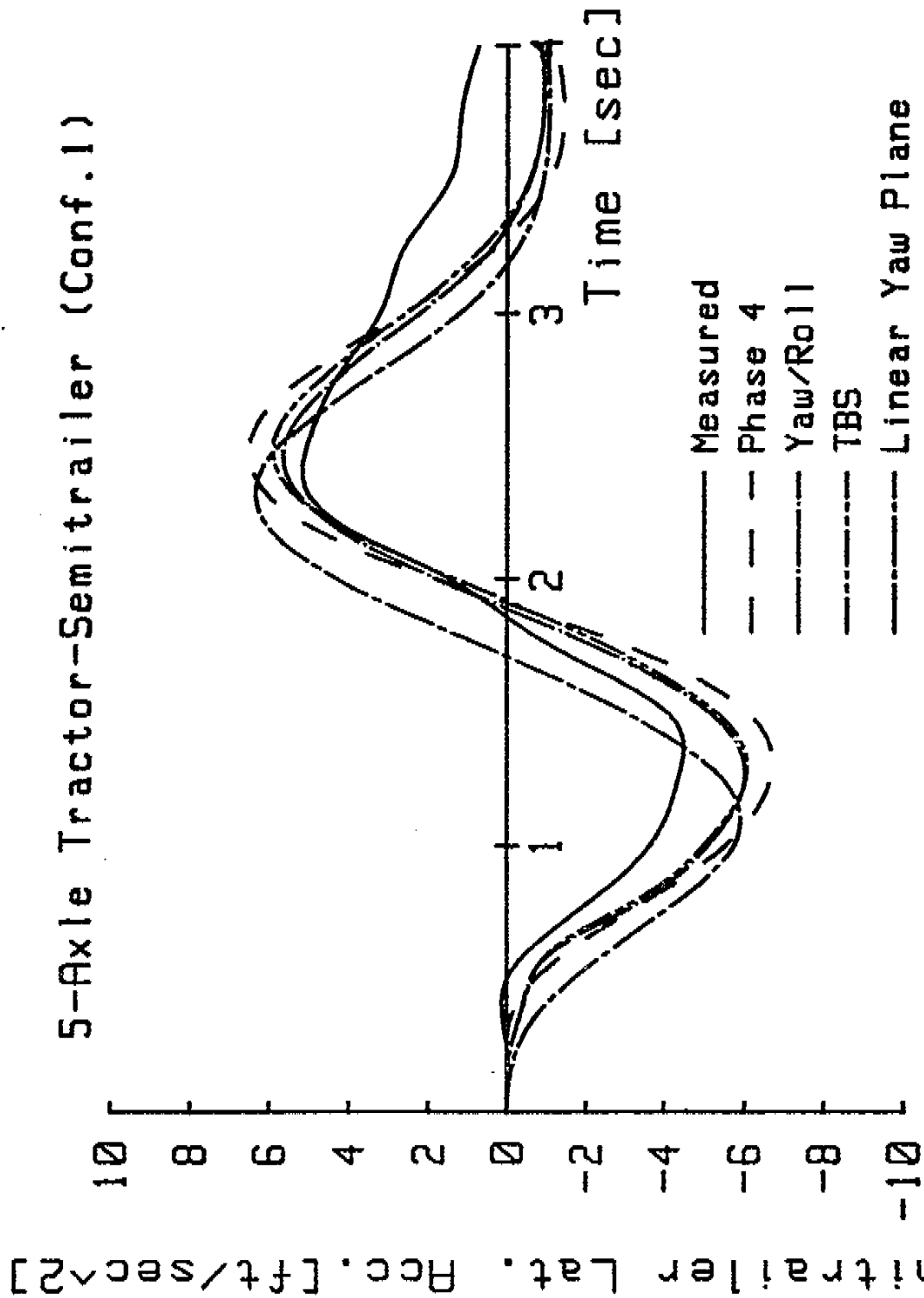


Fig. 4.3 Variation of semitrailer lateral acceleration with time Vehicle Configuration 1 in a lane-change manoeuvre predicted by various models

5-Axle Tractor-Semitrailer (Conf.1)

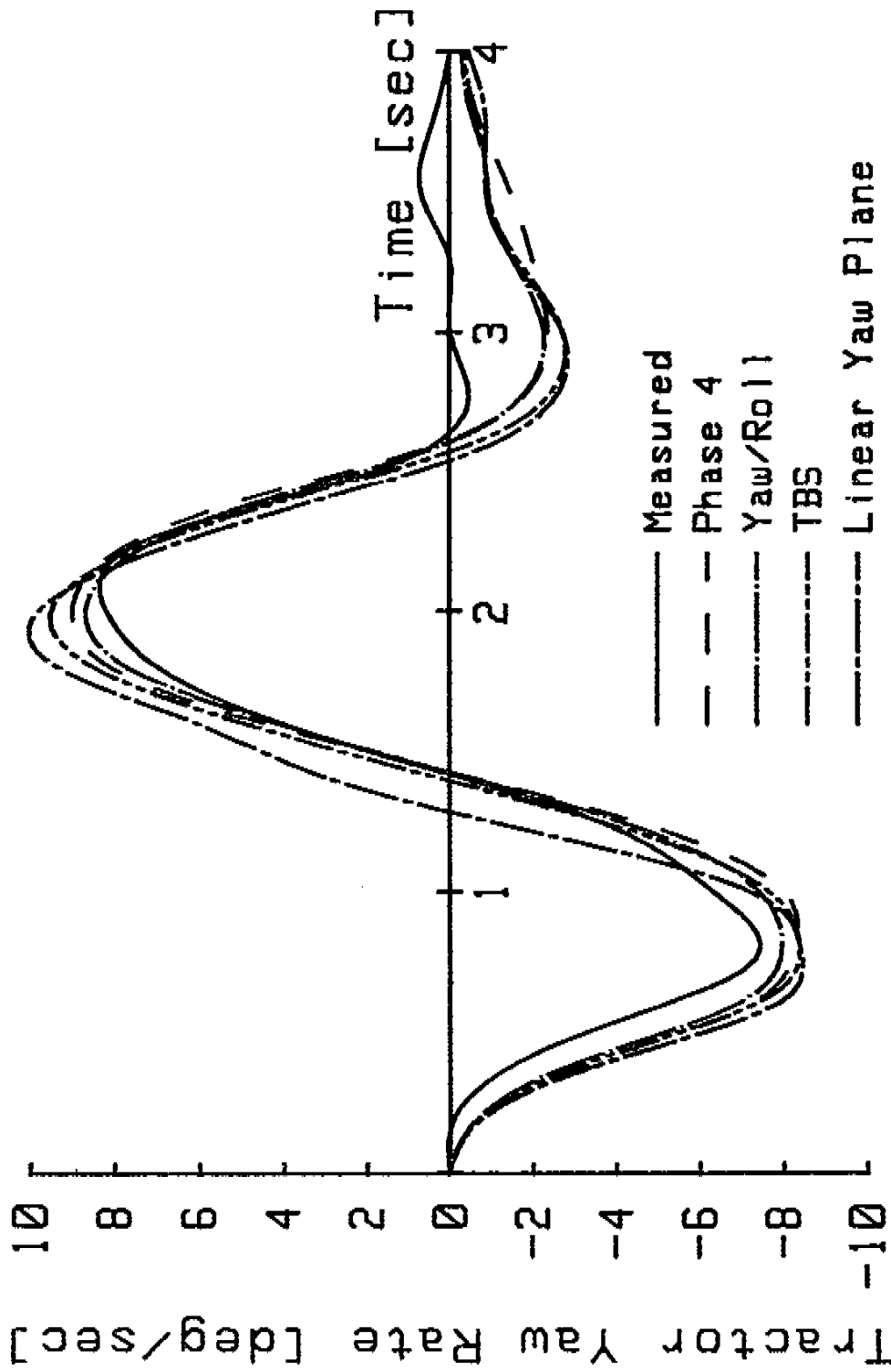


Fig. 4.4 Variation of tractor yaw rate with time of Vehicle Configuration 1 in a lane-change manoeuvre predicted by various models

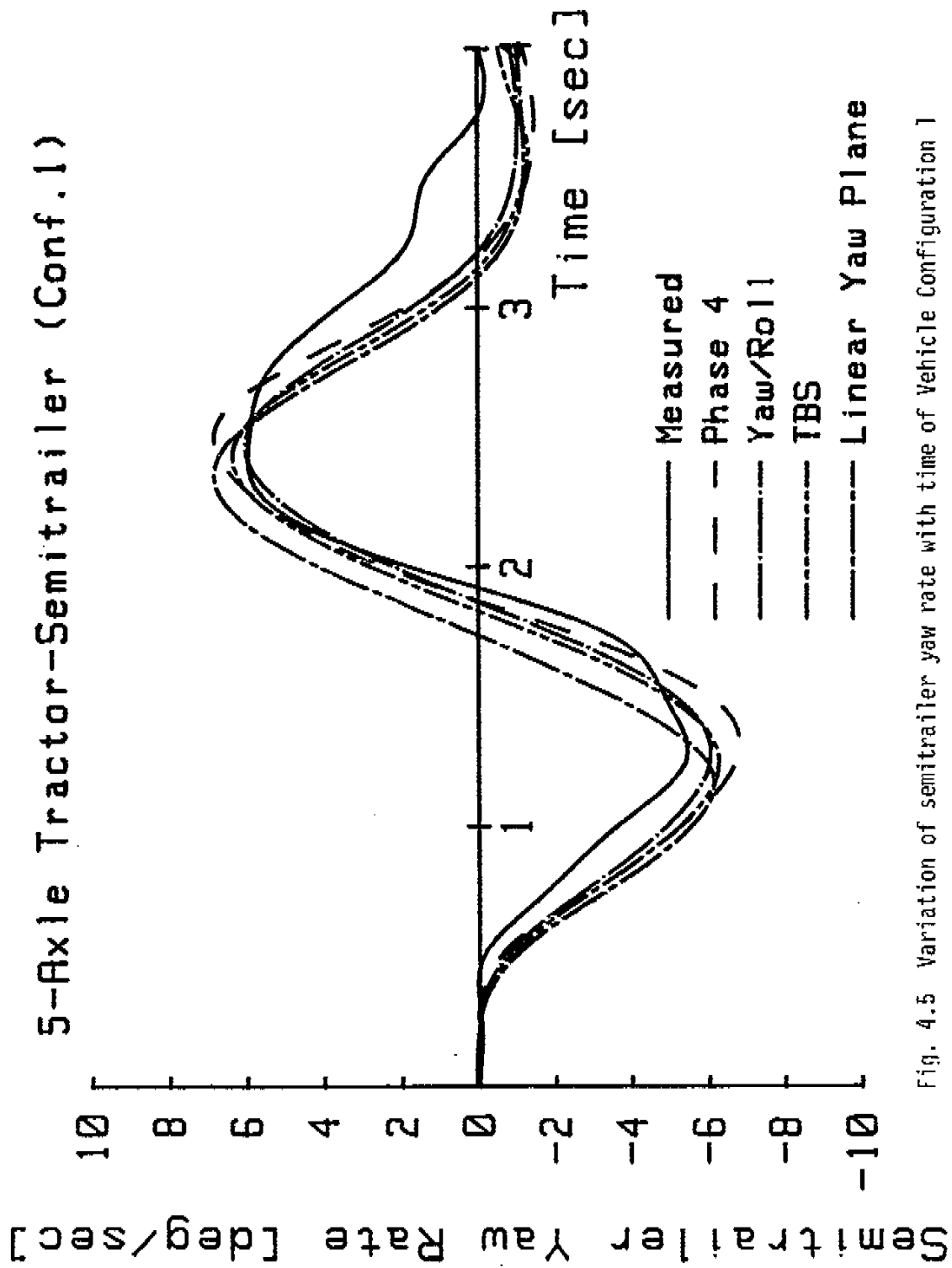


Fig. 4.5 Variation of semitrailer yaw rate with time of Vehicle Configuration 1 in a lane-change manoeuvre predicted by various models

5-Axle Tractor-Semitrailer (Conf.1)

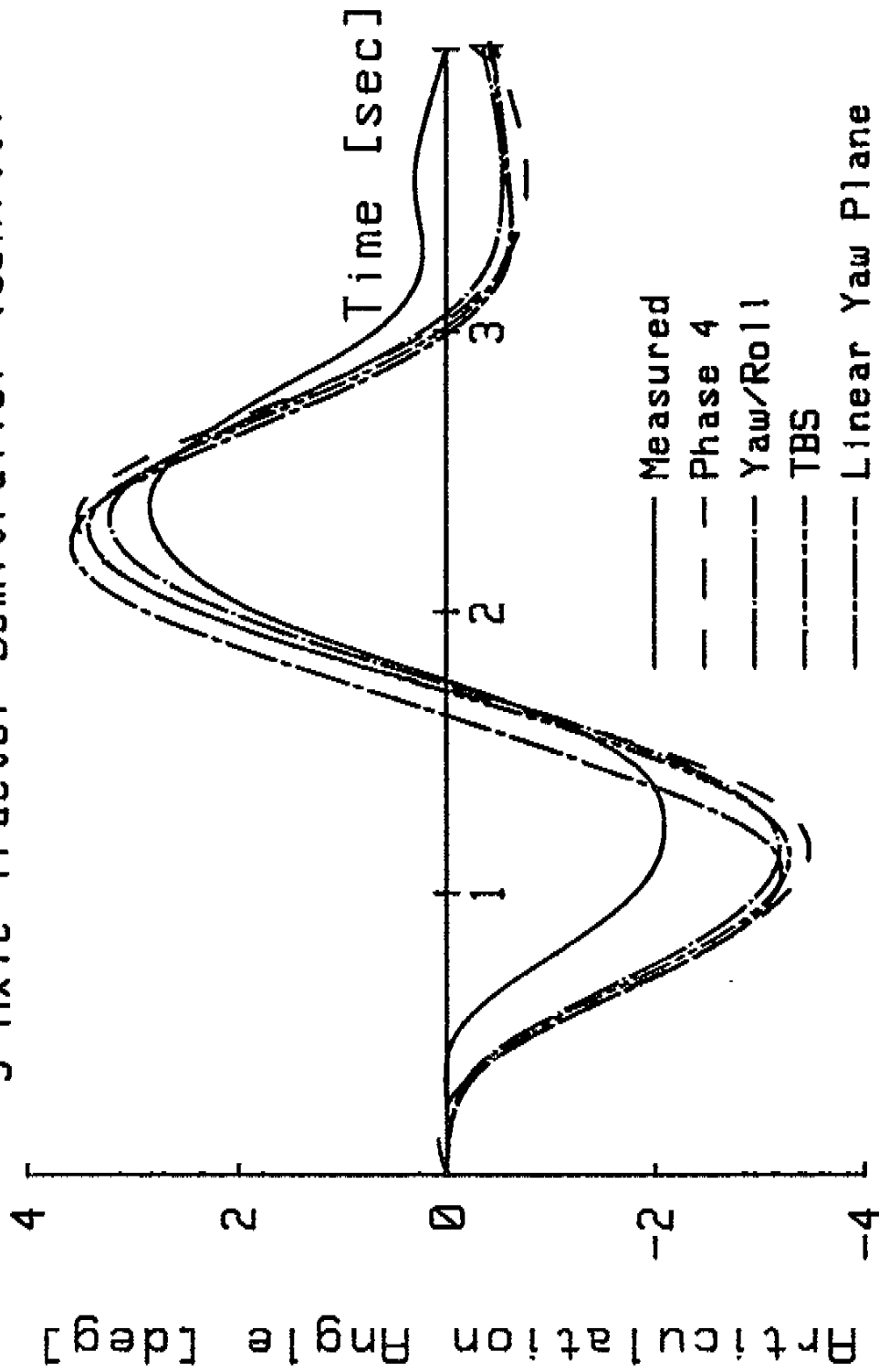


Fig. 4.6 Variation of articulation angle with time of Vehicle Configuration 1 in a lane-change manoeuvre predicted by various models

The agreement between the measured tractor yaw rate response and those predicted using the four models appears to be reasonable. The differences between the measured peak value of tractor yaw rate and those predicted using the Phase 4 model, the yaw/roll model, the TBS model, and the linear yaw plane model are approximately 9.8%, 4.9%, 15.8% and 21.9%, respectively, as can be seen from Fig. 4.4. The measured semitrailer yaw rate response and those predicted using the four models again show reasonable agreement. The differences between the measured peak value of semitrailer yaw rate and those predicted using the Phase 4 model, the yaw/roll model, the TBS model and the linear yaw plane model are approximately 13.3 %, 0 %, 3.3 %, and 13.3 %, respectively, as shown in Fig. 4.5. The articulation angle responses predicted using the four models are reasonably close. The differences between the peak values of articulation angle predicted using the four models are within 10 %. However, there is a noticeable difference between the measured and predicted peak values of articulation angle. For instance, the difference between the measured and the predicted peak value of articulated angle using the Phase 4 model is approximately 22 %, as can be seen from Fig. 4.6.

It should also be noted from the figures that there is a phase shift between the measured and predicted responses, and that there is a significant difference between the measured and predicted responses during the period from 2.5 to 4 seconds.

4.2 Steering Response of Vehicle Configuration 3 in a Severe Lane-Change Manoeuvre

The transient directional response to steering input of Vehicle Configuration 3 (a 5-axle tractor-semitrailer) in a severe lane-change (obstacle-avoidance) type manoeuvre at a forward speed of 35.8 mph (52.5 ft/sec) was predicted using the four computer simulation models. In the simulations, the time history of the average front-wheel steering angle shown in Fig. 4.7 was used as input to the computer simulation models. It can be noted from Fig. 4.7 that the amplitude of the front-wheel steering angle is 6 degrees and that the steering input in the lane-change manoeuvre is completed in 2 seconds. This represents a severe (rapid) lane-change type manoeuvre, as compared with that described in Section 4.1.

The tractor yaw rate, semitrailer yaw rate, tractor lateral acceleration and semitrailer lateral acceleration of Vehicle Configuration 3 predicted using various computer simulation models are shown in Figs. 4.8, 4.9, 4.10 and 4.11, respectively. There is no measured data available for comparison. The information shown in the figures, therefore, only serves the purposes of illustrating the difference in the predictions made by various models.

It can be seen from Figs. 4.8 and 4.9 that the yaw rate responses of the tractor and semitrailer predicted using the four computer simulation models are essentially the same. The differences in the peak values of yaw rate of the tractor predicted using the four models are less than 9.3 % while those of the semitrailer are within the range of 5.7 %.

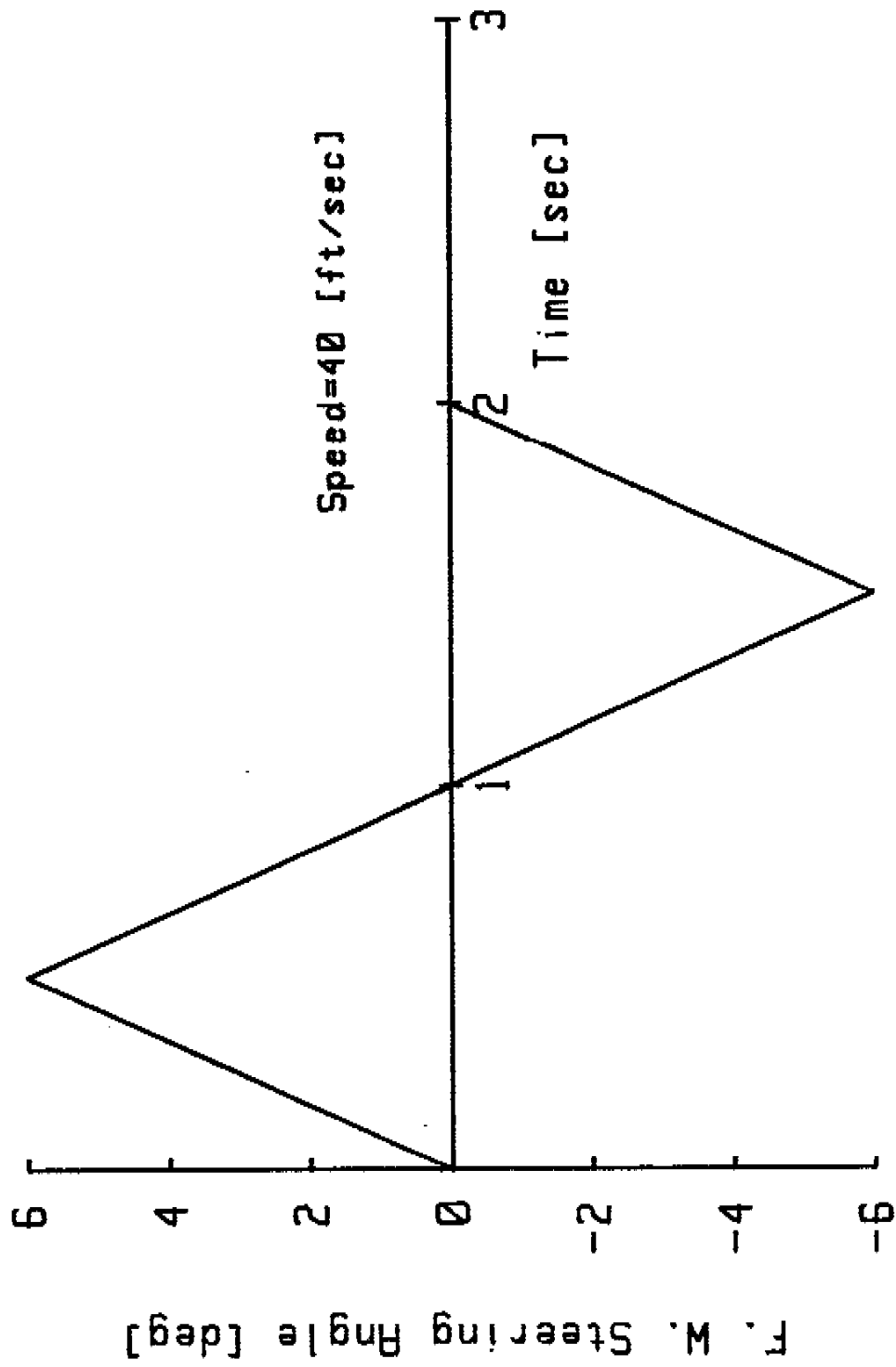


Fig. 4.7 Front-wheel steering inputs to the simulation of severe (rapid) lane-change manoeuvres

5-Axle Tractor-Semitrailer (Conf.3)

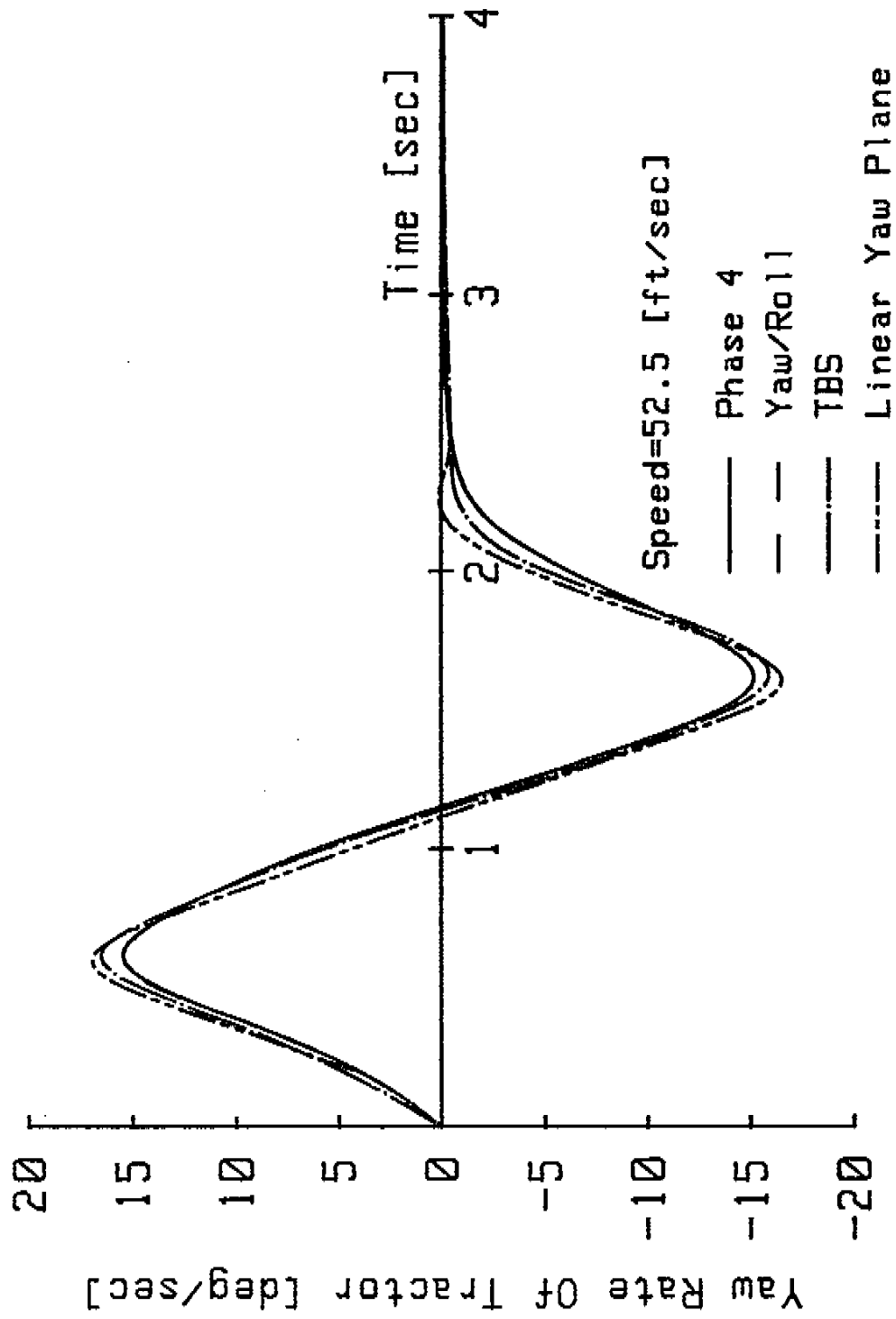


Fig. 4.8 Variation of tractor yaw rate with time of Vehicle Configuration 3 in a severe lane-change manoeuvre predicted by various models

5-Axle Tractor-Semitrailer (Conf.3)

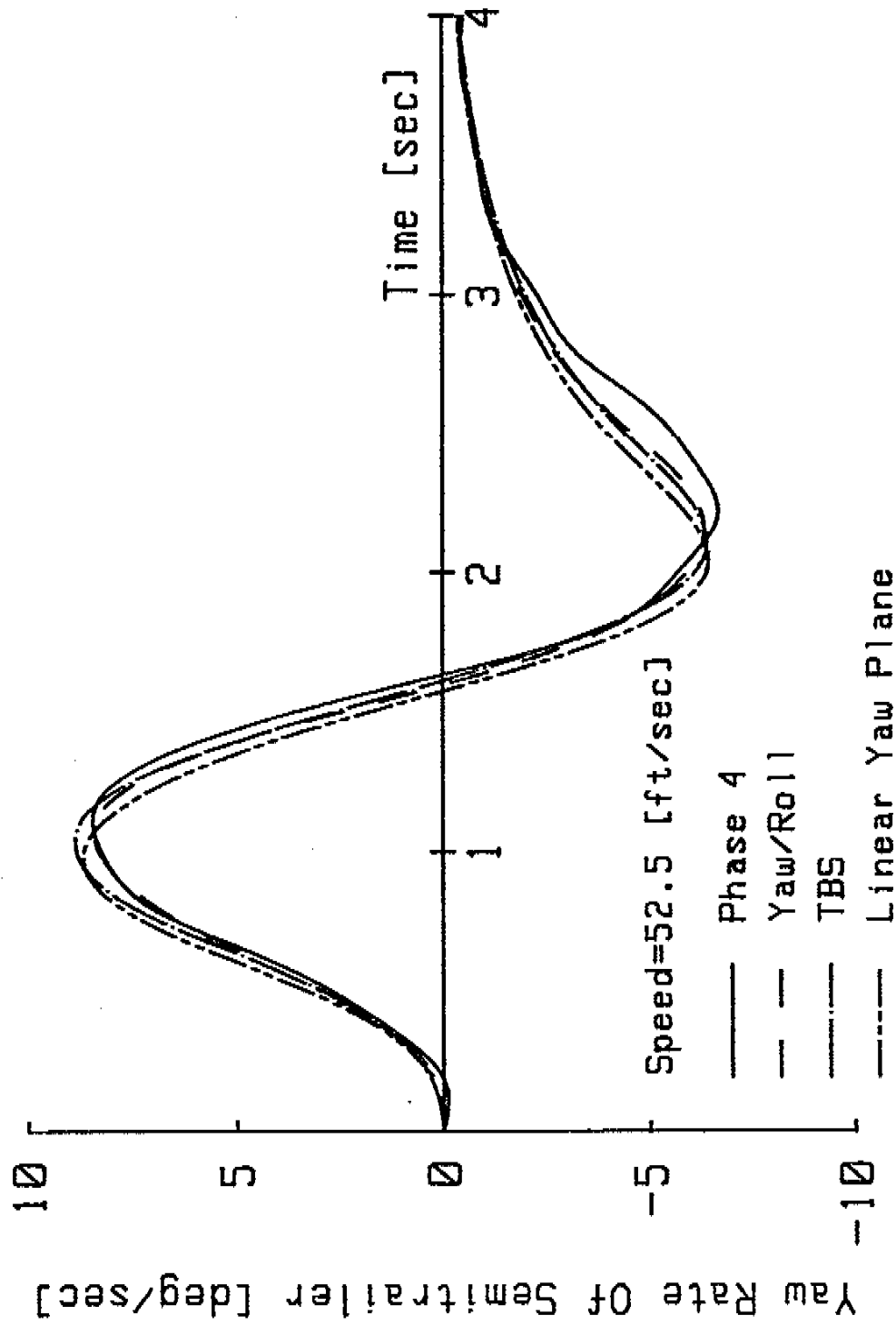


Fig. 4.9 Variation of semitrailer yaw rate with time of Vehicle Configuration 3 in a severe lane-change manoeuvre predicted by various models

5-Axle Tractor-Semitrailer (Conf.3)

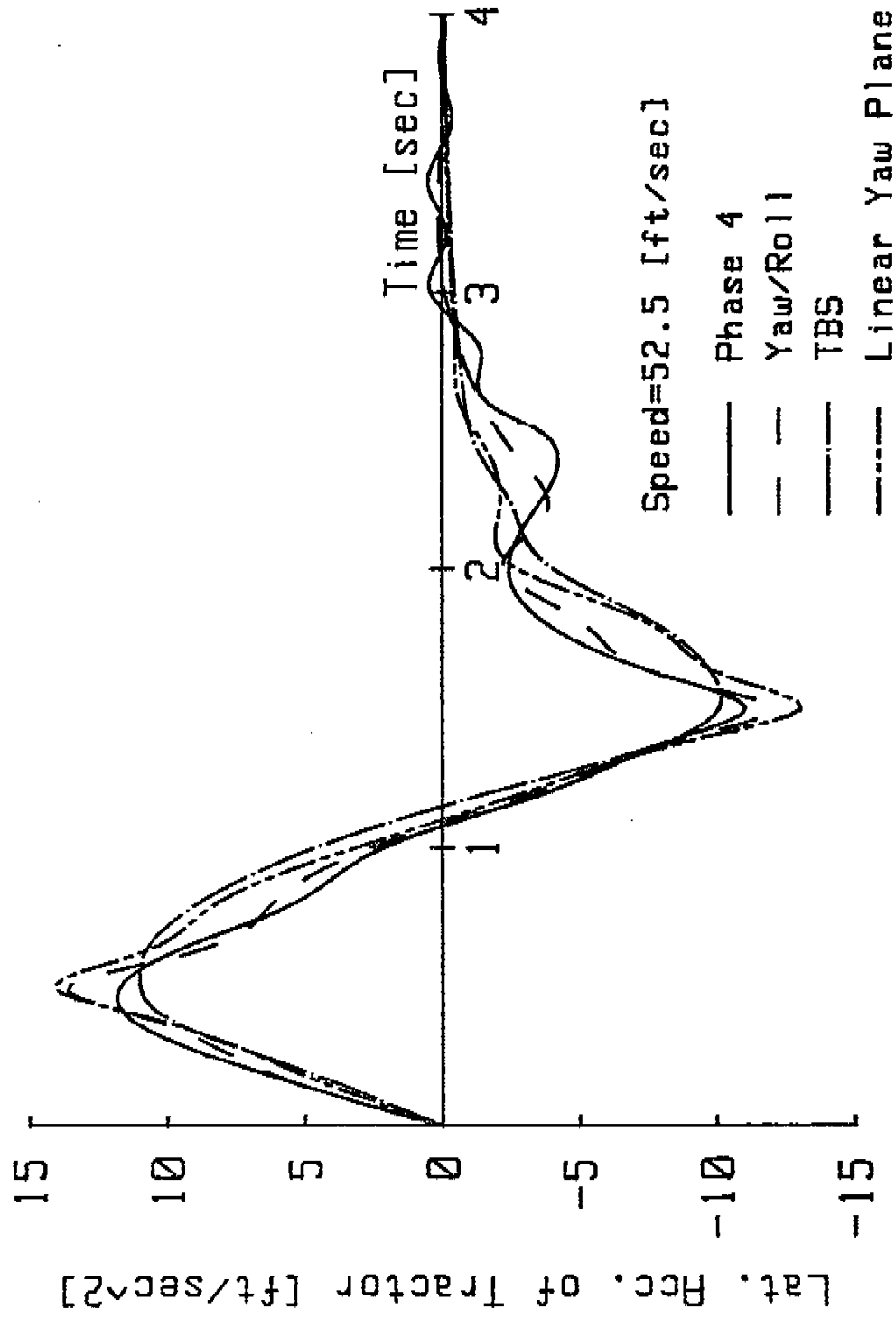


Fig. 4.10 Variation of tractor lateral acceleration with time of Vehicle Configuration 3 in a severe lane-change manoeuvre predicted by various models

5-Axle Tractor-Semitrailer (Conf.3)

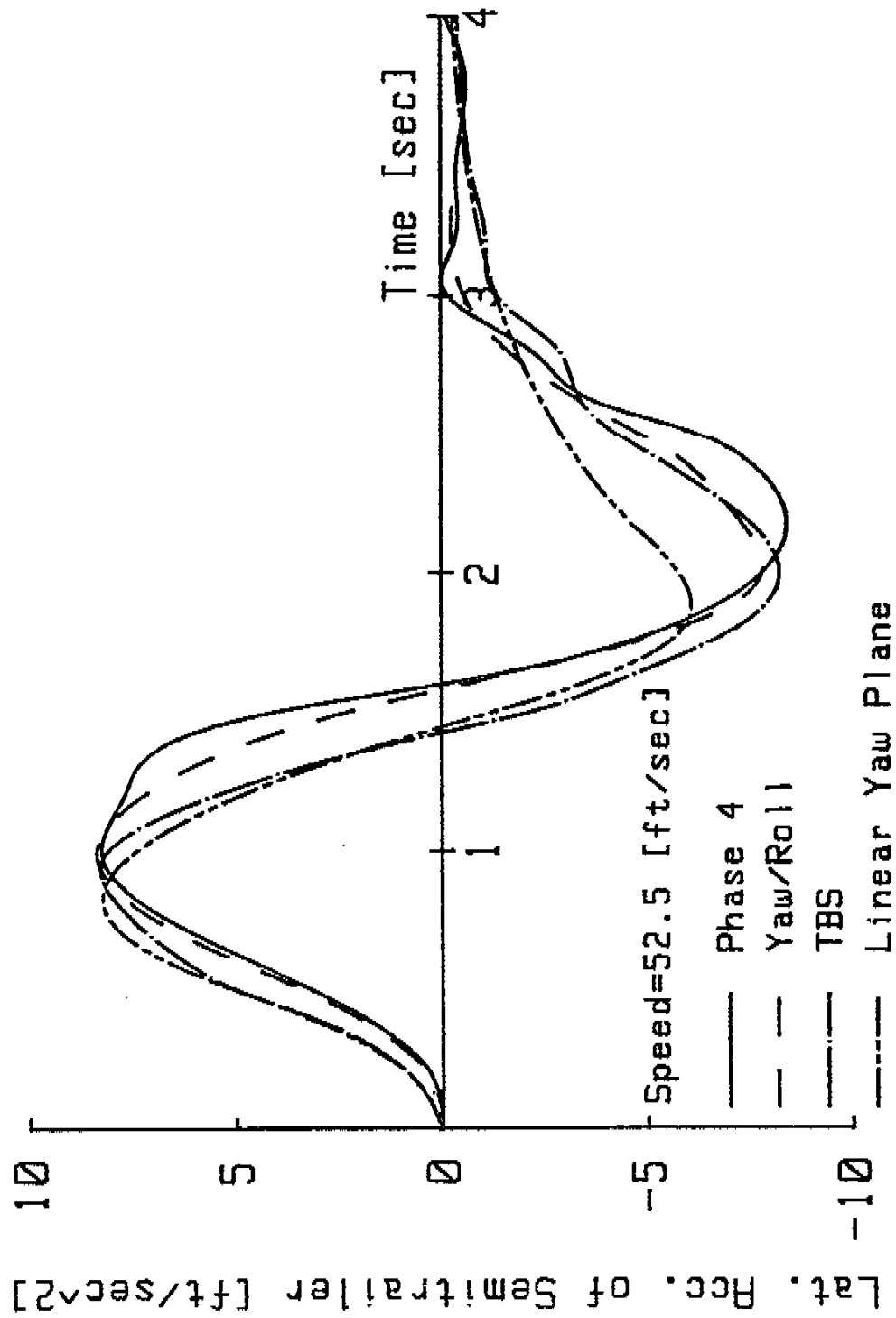


Fig. 4.11 Variation of semitrailer lateral acceleration with time of Vehicle Configuration 3 in a severe lane-change manoeuvre predicted by various models

As can be seen from Figs. 4.10 and 4.11, the characteristics of the lateral acceleration response of the tractor and semitrailer predicted using the four computer simulation models show noticeable differences in phase and in peak value. For instance, the differences in the peak value of tractor lateral acceleration predicted using the Phase 4 model and those predicted using the yaw/roll model, the TBS model and the linear yaw plane model are 15.2 %, 7.1 % and 19.2 %, respectively.

4.3 Steering Response of Vehicle Configuration 6 in a Severe Lane-Change Manoeuvre

The transient directional response to steering input of Vehicle Configuration 6 (a tractor-semitrailer-full trailer) in a severe lane-change manoeuvre at a forward speed of 27.3 mph (40 ft/sec), was predicted using the Phase 4 model, the yaw/roll model, and the linear yaw plane model. The TBS model was not used in the simulation, as it is not designed, in its present form, for simulating this type of vehicle combination. The steering input to the various simulation models is the same as that shown in Fig. 4.7.

The yaw rates of the tractor, semitrailer and full trailer (pup trailer) and the lateral accelerations of the tractor, semitrailer and full trailer of Vehicle Configuration 6 predicted using the three computer simulation models are shown in Figs. 4.12, 4.13, 4.14, 4.15, 4.16 and 4.17, respectively.

It can be seen from Figs. 4.12 and 4.13 that the yaw rate responses of the tractor and semitrailer predicted using the three computer simulation models are quite close. The differences in the peak values of yaw rate of the tractor predicted using the three models are less than 9.8 %, while those of the semitrailer are less than 2.8 %. The yaw rate responses of the full trailer (pup trailer) predicted using the Phase 4 model and the yaw/roll model are essentially identical, as can be seen from Fig. 4.14. However, there is a significant difference in the yaw rate response characteristics predicted using the linear yaw plane model and those predicted using the Phase 4 model and the yaw/roll model, and the difference in the peak value of yaw rate is approximately 15 %.

5-Axle Double/27-Ft Trailers (Conf.6)

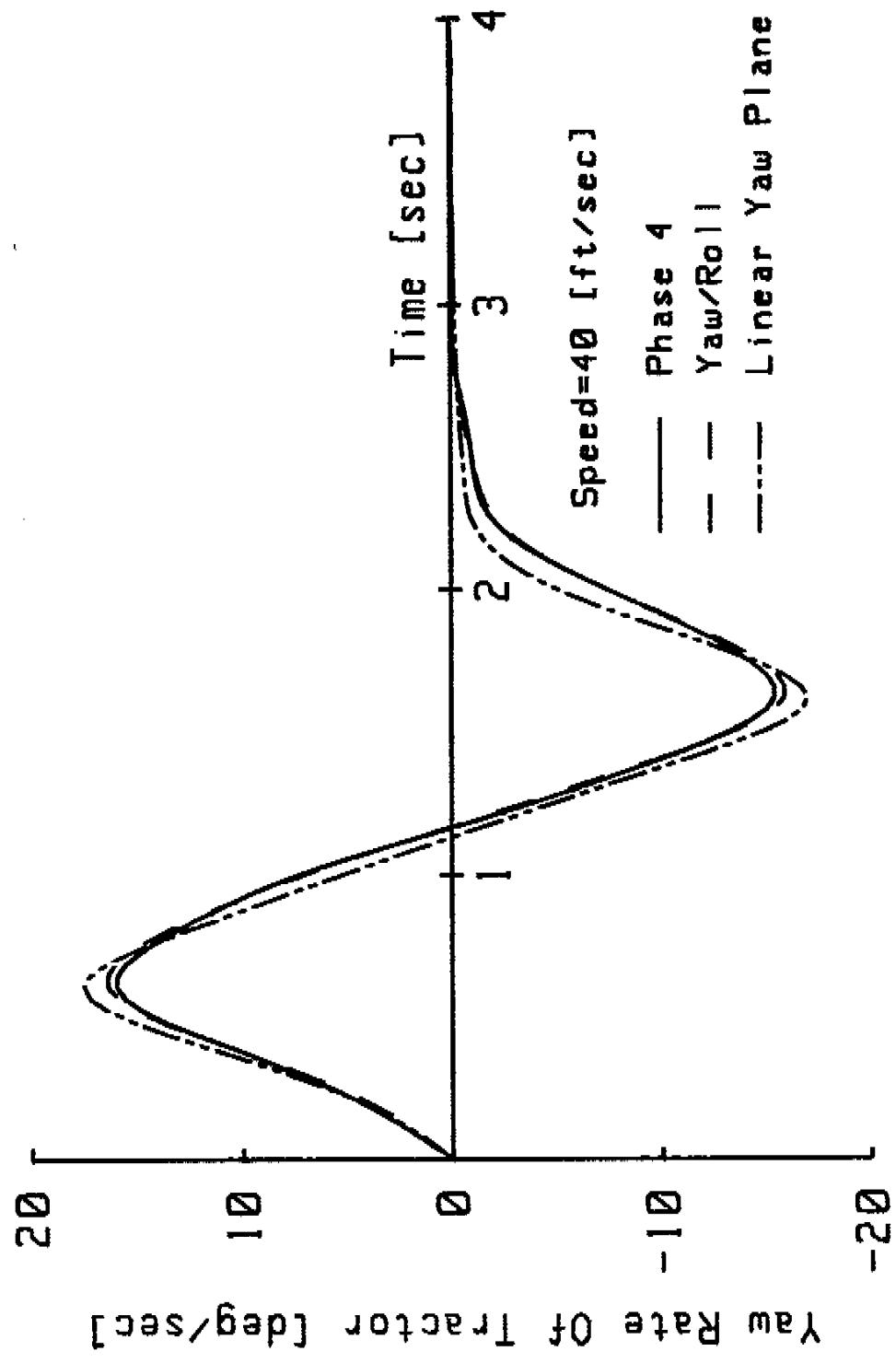


Fig. 4.12 Variation of tractor yaw rate with time of Vehicle Configuration 6 in a severe lane-change manoeuvre predicted by various models

5-Axle Double/27-Ft Trailers (Conf. 6)

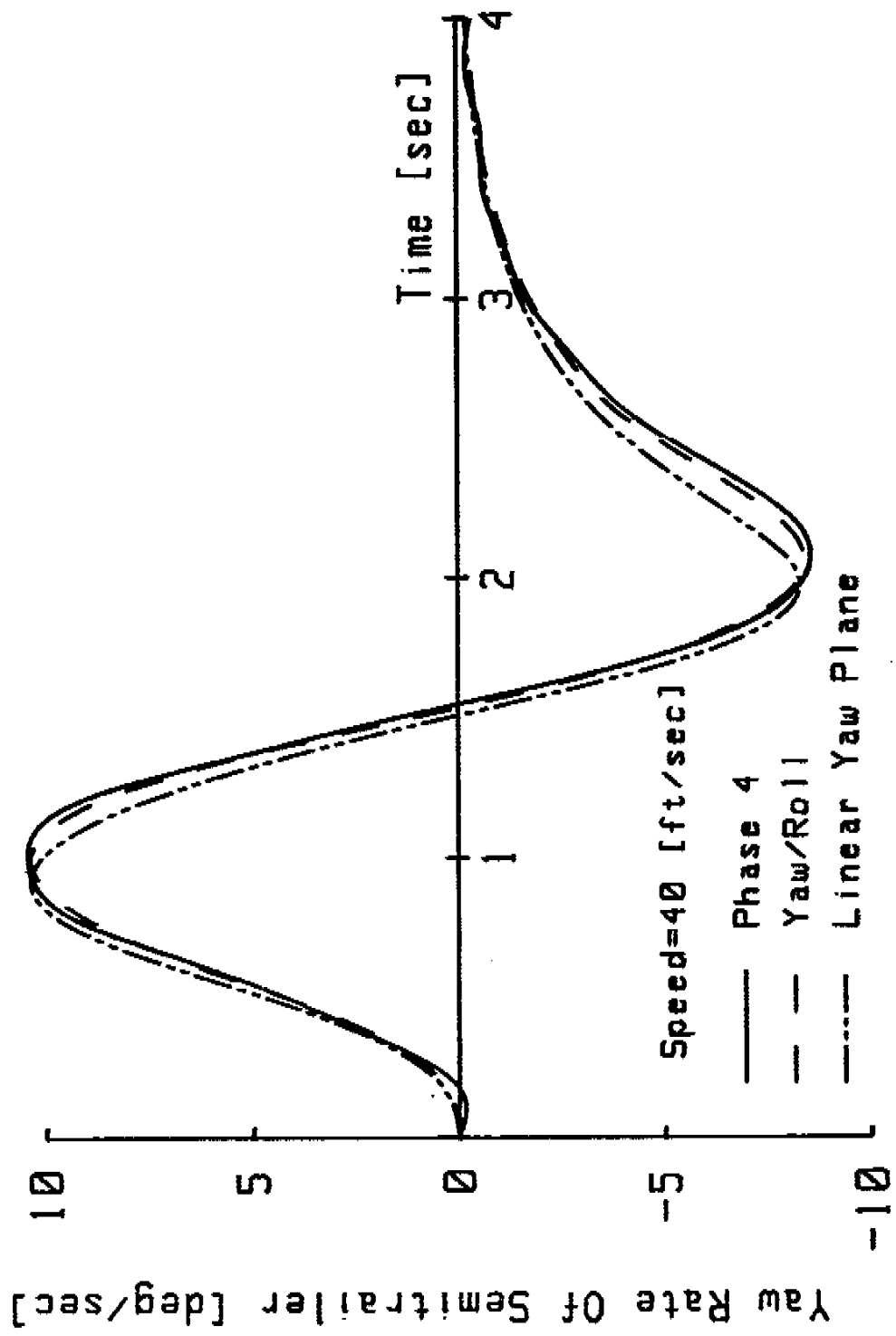


Fig. 4.13 Variation of semitrailer yaw rate with time of Vehicle Configuration 6 in a severe lane-change manoeuvre predicted by various models

5-Axle Double/27-Ft Trailers (Conf.6)

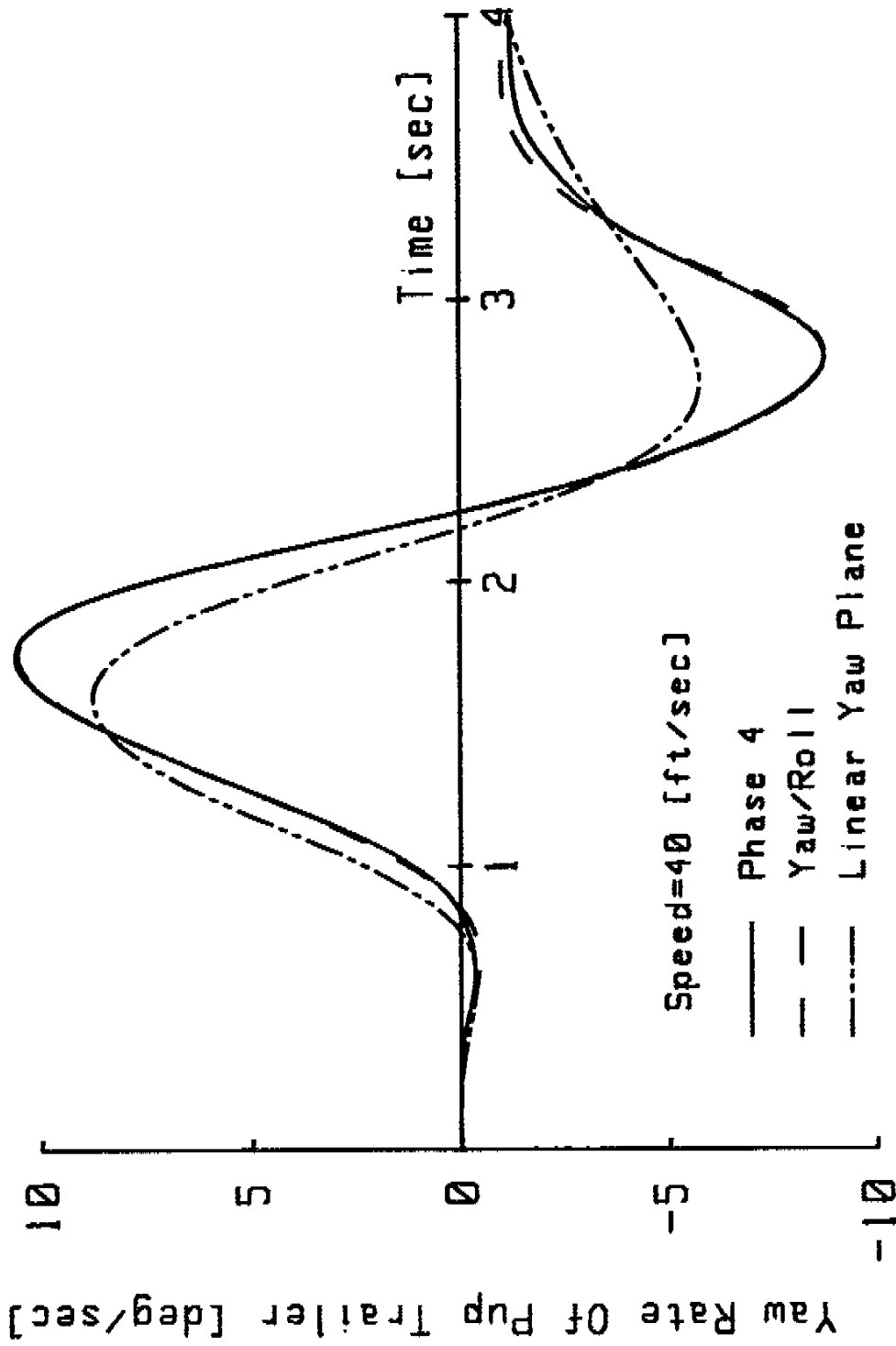


Fig. 4.14 Variation of pup trailer yaw rate with time of Vehicle Configuration 6 in a severe lane-change manoeuvre predicted by various models

5-Axle Double/27-Ft Trailers (Conf.6)

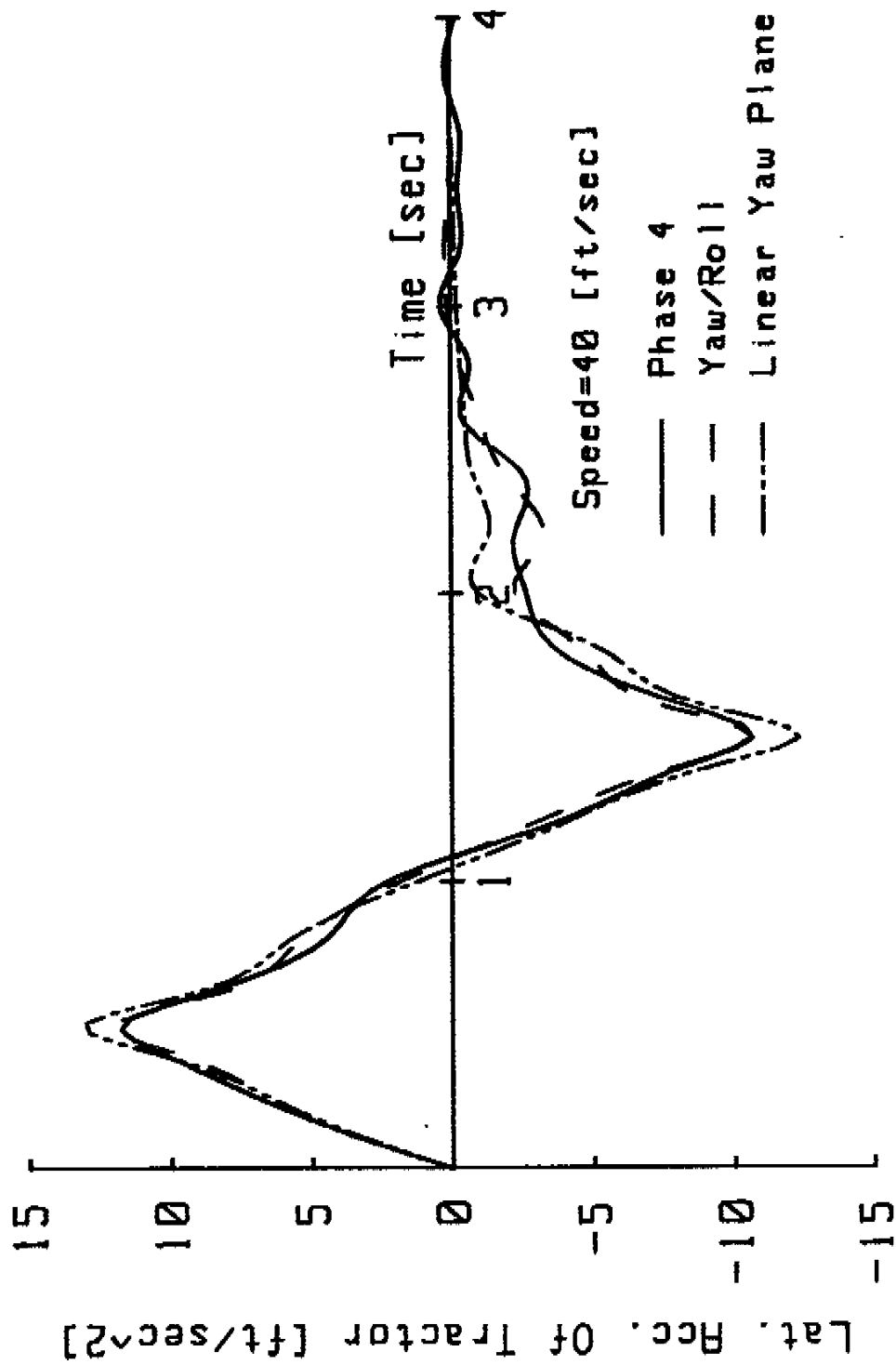


Fig. 4.15 Variation of tractor lateral acceleration with time of Vehicle Configuration 6 in a severe lane-change manoeuvre predicted by various models

5-Axle Double/27-Ft Trailers (Conf.6)

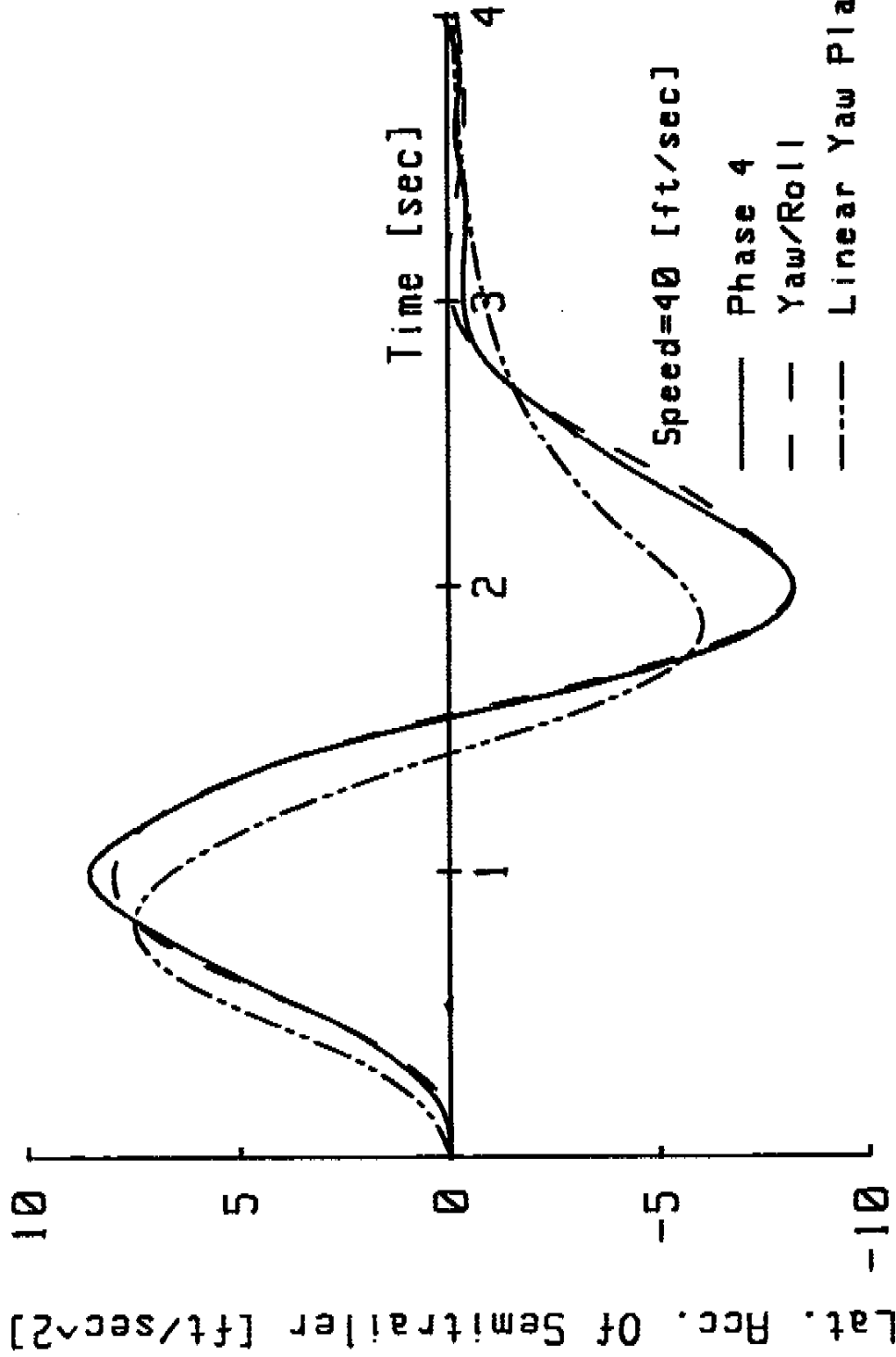


Fig. 4.16 Variation of semitrailer lateral acceleration with time of Vehicle Configuration 6 in a severe lane-change manoeuvre predicted by various models

5-Axle Double/27-Ft Trailers (Conf.6)

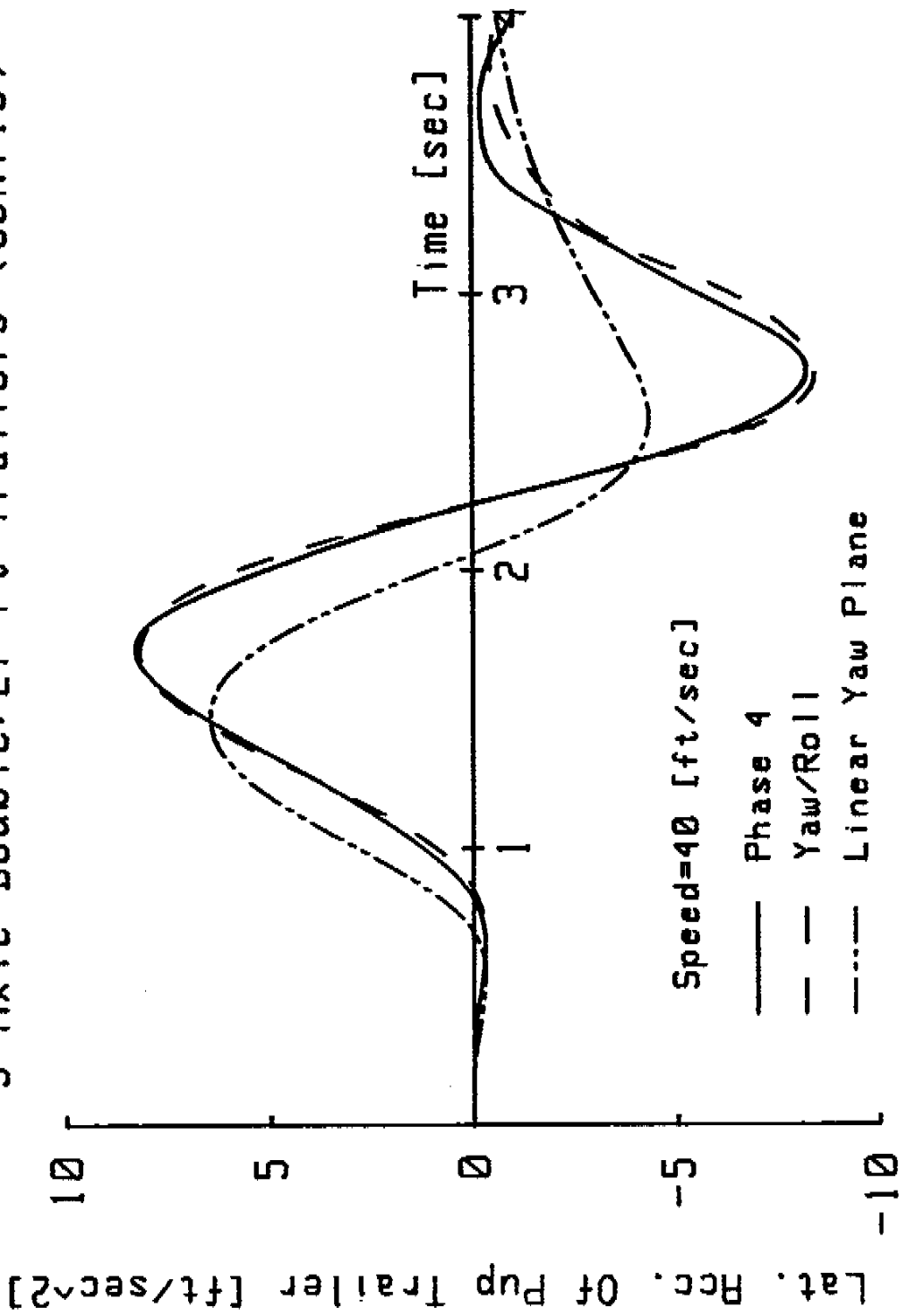


Fig. 4.17 Variation of pup trailer lateral acceleration with time for Vehicle Configuration 6 in a severe lane-change manoeuvre predicted by various models

From Fig. 4.15, it can be seen that the lateral acceleration responses of the tractor predicted using the three computer simulation models are similar, and that the differences in the peak value of lateral acceleration are within 9.9 %. The lateral acceleration responses of the semitrailer and of the full trailer (pup trailer) predicted using the Phase 4 model and the yaw/roll model are essentially the same, as can be seen from Figs. 4.16 and 4.17. However, there is a noticeable difference between the characteristics of the lateral acceleration responses of the semitrailer and the full trailer predicted using the linear yaw plane model and those predicted using the other two models. For instance, the difference between the peak value of lateral acceleration of the semitrailer predicted using the linear yaw plane model and that predicted using the other two models is approximately 13 %, while that for the full trailer is approximately 22.6 %. Furthermore, there is a significant phase shift between the responses predicted using the linear yaw plane model and those predicted using the Phase 4 model and the yaw/roll model.

5. A PARAMETRIC SENSITIVITY STUDY OF THE STATIC ROLL MODEL

As mentioned previously in Section 1.5, the static roll model was developed for the purpose of determining the rollover threshold of articulated vehicles during steady-state turning manoeuvres. This model is based on a number of simplifying assumptions. However, it requires a considerable amount of vehicle input data, some of which can only be obtained using special apparatus. For instance, the model requires, among others, the following vehicle parameters as inputs:

- A. Tractor frame torsional stiffness;
- B. Coulomb friction present in the tractor frame;
- C. Equivalent trailer structural and fifth wheel compliance;
- D. Separation of fifth wheel plates (Lash)

If no existing data are available for the vehicle to be simulated, then these parameters have to be measured. For some of the parameters, such as the equivalent tractor frame torsional stiffness, even if the equipment is available, there appears to be a lack of generally accepted procedures for measuring it, as the value of the equivalent torsional stiffness depends on the loading conditions as well as the type of constraint used in the tests. It appears, therefore, that while the model represents a simplification of the actual vehicle system, the acquisition of appropriate input data to the model could be quite involved. Thus, it seems useful to conduct an evaluation of the significance of certain input parameters to the simulated results. If it is found that the simulated results are not sensitive to certain input parameters, then the considerable effort that may be required to measure them may not be justified. This would also provide guidance

for the revision of the original model, so as to make it more useful to the practising engineer.

In this section, the sensitivity of the simulated results to the four input parameters mentioned above is evaluated. In the evaluation, a 5-axle dirt truck (from File 25 of a UMTR) magnetic tape dated November 25, 1981) was used. The basic parameters of this vehicle are given in Appendix G. In the study, the values of the four parameters are varied within a certain range and the corresponding simulated results are obtained. The results of the sensitivity study are described below.

5.1 Tractor Frame Torsional Stiffness

The effects of the equivalent torsional stiffness of the tractor frame on the rollover threshold, expressed in terms of the maximum lateral acceleration ($a_{y \max}$) allowed without causing rollover, were examined using the static roll model. Three values of the equivalent torsional stiffness: 40,000 (measured value for the 5-axle, dirt truck), 500,000 and 9,000,000 in-lb/deg (equivalent to a very rigid tractor frame) were used in the simulation. The results are shown in Table 5.1.

Table 5.1
Effects of Tractor Frame Torsional Stiffness

Tractor frame torsional stiffness, in-lb/deg	Rollover threshold, $a_{y \max}$, g	Roll angle of the first sprung mass, ϕ_1 , deg	Roll angle of second sprung mass, ϕ_2 , deg	Roll angle of third sprung mass, ϕ_3 , deg
40,000	0.35	6.01	5.40	5.78
500,000	0.35	5.5	5.42	5.80
9,000,000	0.35	5.47	5.42	5.80

It can be seen from Table 5.1 that within the range of 40,000 to 9,000,000 in-lb/deg, the torsional stiffness of the tractor frame has no effect whatsoever on the rollover threshold of the vehicle simulated. It has a minor effect on the simulated roll angle of the first sprung mass. However, the difference is less than 9 % when the torsional stiffness varies from 40,000 to 9,000,000 in-lb/deg. Table 5.1 also indicates that

the torsional stiffness of the tractor frame has essentially no effect on the simulated roll angles of the second and third sprung masses.

5.2 Coulomb Friction Present in the Tractor Frame

The effects of the Coulomb type friction present in the tractor frame on the rollover threshold of the vehicle were evaluated using the static roll model. Three values of Coulomb friction: 11,000 (measured value for the 5-axle, dirt truck), 5,500 and 0 lb, were used in the simulations. The results are given in Table 5.2.

Table 5.2

Effects of Coulomb Friction Present in the Tractor Frame

Coulomb friction, lb	Rollover threshold, $a_{y \max}$, g	Roll angle of first sprung mass, ϕ_1 , deg	Roll angle of second sprung mass, ϕ_2 , deg	Roll angle of third sprung mass, ϕ_3 , deg
11,000	0.35	6.01	5.4	5.78
5,500	0.35	6.11	5.4	5.78
0	0.35	6.22	5.4	5.78

As can be seen from Table 5.2, within the range of 0 to 11,000 lb, the Coulomb friction present in the tractor frame has no effect at all on the rollover threshold, and the roll angles of the second and third sprung masses of the vehicle simulated. It has a very slight effect on the simulated roll angle of the first sprung mass. However, the difference

is less than 3.5 %, when the Coulomb friction varies from 0 to 11,000 lb.

5.3 Equivalent Trailer Structural and Fifth Wheel Compliance

The effects of the equivalent trailer structural and fifth wheel compliance on the rollover threshold of the vehicle were assessed using the static roll model. Three values of the equivalent torsional stiffness of the trailer structure and fifth wheel: 1,000,000 (measured value for the 5-axle dirt truck), 500,000, and 9,000,000 in-lb/deg (equivalent to rigid), were used in the simulations. The results are summarized in Table 5.3.

Table 5.3
Effects of Equivalent Trailer Structural and Fifth Wheel Compliance

Equivalent torsional stiffness of trailer structure & 5th wheel, in-lb/deg	Rollover threshold, $a_y \text{ max } g$	Roll angle of the 1st sprung mass, ϕ_1 , deg.	Roll angle of the 2nd sprung mass, ϕ_2 , deg	Roll angle of the 3rd sprung mass, ϕ_3 , deg
1,000,000	0.35	6.01	5.4	5.78
500,000	0.35	5.72	5.02	5.78
9,000,000	0.35	6.26	5.74	5.78

As shown in Table 5.3, the equivalent trailer structural and fifth wheel compliance has no effect whatsoever on the rollover threshold and the roll angle of the third sprung mass. It has only a slight effect on

the simulated roll angles of the first and the second sprung masses, ϕ_1 and ϕ_2 . The difference in the simulated roll angle ϕ_1 is approximately 4.8 %, when the equivalent torsional stiffness is reduced from 1,000,000 to 500,000 in-lb/deg, while the difference is 4.2 %, when the stiffness is increased from 1,000,000 to 9,000,000 in-lb/deg. For the simulated roll angle ϕ_2 , the difference is approximately 7 %, when the torsional stiffness changes from 1,000,000 to 500,000 in-lb/deg, whereas the difference is 6.3 % when the stiffness varies from 1,000,000 to 9,000,000 in-lb/deg.

5.4 Separation of Fifth Wheel Plates (Lash)

The effects of the separation of fifth wheel plates (lash) on the roll behaviour of the vehicle were evaluated using the static roll model. In the simulation, the lash was varied from 0 (measured value for the 5-axle, dirt truck) to 2 in. It is found that within this range, the lash has practically no effect on the rollover threshold and the roll angles of the first, second, and third sprung masses.

The effects of the overturning stiffness of the tires on the roll behaviour of the vehicle were also examined. The measured values of the overturning stiffness of the tires on the first axle, second axle and third axle of the 5-axle, dirt truck, were 1,000, 2,000, and 2,000 in-lb/deg, respectively. No effect on the rollover threshold of the vehicle has been found by ignoring the overturning stiffness of the tires.

After the individual effects of the tractor frame torsional stiffness, Coulomb friction present in the tractor frame and trailer structural and fifth wheel compliance and separation of the fifth wheel plates had been

examined, their combined effects on the roll behaviour of the 5-axle dirt truck were evaluated. For the evaluation, certain parameters of the baseline vehicle were modified. The modified values of these parameters are: tractor frame torsional stiffness of 9,000,000 in-lb/deg (essentially a rigid frame), zero Coulomb friction, and equivalent torsional stiffness of trailer structure and fifth wheel of 9,000,000 in-lb/deg (essentially a rigid connection), no lash in the fifth wheel plates and zero overturning stiffness of the tires. The rollover threshold and the corresponding roll angles of the sprung masses of the modified vehicle were predicted using the static roll model and compared with that of the baseline vehicle with measured values shown in Tables 1, 2 and 3. The results are given in Table 5.4.

Table 5.4
A Comparison of the Roll Behaviour of
The Modified and The Baseline Vehicle

Vehicle Type	Rollover Threshold, $a_{y \max}$, g	Roll angle of first sprung mass, ϕ_1 , deg	Roll angle of second sprung mass, ϕ_2 , deg	Roll angle of third sprung mass, ϕ_3 , deg
Baseline Vehicle	0.35	6.01	5.40	5.78
Modified Vehicle	0.35	5.76	5.72	5.78

From Table 5.4, it can be seen that the changing of the tractor frame torsional stiffness, Coulomb friction present in the tractor frame, and trailer structural and fifth wheel compliance, lash in the fifth wheel plates and overturning stiffness of tires in the ranges shown, has no effect on the rollover threshold and the corresponding roll angle of the third sprung mass. Their combined effects on the roll angles of the first and second sprung masses are slight. For instance, the difference in the simulated roll angle of the first sprung mass between the modified and the baseline vehicle is only 4.2 %, and the difference in the simulated roll angle of the second sprung mass between the two vehicles is approximately 6 %.

6. DISCUSSIONS

Based on the results of this study, the following observations are made:

A. In comparison with the measured data available, the steady-state steering responses of tractor-semitrailers with different design features predicted using the Phase 4 model, the yaw/roll model, the TBS model, and the linear yaw plane model all have varying degrees of error (see Figs. 3.2, 3.3, 3.5 and 3.6.). It appears that a more sophisticated simulation model, such as the Phase 4 model, does not necessarily give a more accurate prediction than a simpler model, such as the TBS model or the linear yaw plane model, under certain circumstances. For instance, for Vehicle Configuration 2, of which the tractor is highly understeer, the simple model (i.e., the linear yaw plane model) appears to give the best overall prediction in the lateral acceleration range up to approximately 0.4 g (see Fig. 3.5).

For the six vehicle configurations examined in this study, it appears that there are no significant differences in the steady-state steering responses predicted using the four simulation models in the lateral acceleration range up to approximately 0.25 g.

B. There are significant differences in handling characteristics predicted using the four simulation models in most cases. Since the linear yaw plane model does not take into account the effects of load transfer and uses a linear tire model, it is not capable of predicting changes in handling behaviour with lateral acceleration. On the other hand, the Phase 4 model, the yaw/roll model, and the TBS model take into

account the effects of load transfer and the non-linear behaviour of tires to varying degrees. Consequently, these three models can predict changes in handling behaviour with lateral acceleration (see Figs. 3.4 and 3.7). It should be noted, however, that the predictions made by these three models are still noticeably different from the measured data available.

It should be pointed out that the parameter $(r\ell/U - \delta_{av})$ used to characterize vehicle handling behaviour is very sensitive to the errors in the values of yaw rate r , forward speed U , and the front wheel steering angle δ_{av} . A small error in the values of r , U , and δ_{av} will result in a significant error in the value of the parameter $(r\ell/U - \delta_{av})$. For example, if the wheelbase ℓ of a vehicle is 142 in., and the nominal values of r , U and δ_{av} are 10 deg/s, 63.07 ft/s, and 1.7 deg., respectively, then a $\pm 5\%$ error in these values will result in an error in the value of $(r\ell/U - \delta_{av})$ ranging from -150% to +160%. Even a $\pm 1\%$ error in these values will result in an error of $\pm 31\%$ in the value of $(r\ell/U - \delta_{av})$. This would cause problems in using this parameter to characterize the handling behaviour in practice.

C. The transient steering responses of tractor-semitrailers predicted using the four simulation models are qualitatively similar in many cases. However, in comparison with the measured data available, all the predictions have varying degrees of error, as can be seen from Figs. 4.2 to 4.6. It appears that a more sophisticated model, such as the Phase 4 model, is not necessarily better than a simpler model, such as the TBS model or the linear yaw plane model, in predicting the transient responses of tractor-semitrailers like Vehicle Configuration 1.

For tractor semitrailers in severe lane-change manoeuvres, the transient steering responses, particularly the yaw rate responses, predicted using various models are quite close, as can be seen from Figs. 4.8 and 4.9.

For doubles, such as Vehicle Configuration 6, in severe lane-change manoeuvres, the yaw rate responses of the tractor and semitrailers predicted

using the various models are similar (see Figs. 4.12 and 4.13). However, there is a noticeable difference between the yaw rate responses of the full trailer predicted using the linear yaw plane model and those predicted using the Phase 4 model and the yaw/roll model (see Fig. 4.14).

D. The results of a parametric sensitivity study of the static roll model indicate that some of the parameters, such as the tractor frame torsional stiffness, Coulomb friction in the tractor frame, equivalent trailer structural and fifth wheel compliance, separation of fifth wheel plates, and the overturning stiffness of tires, have little, if any, effects on the rollover threshold of the articulated vehicle examined in this study. This may indicate that the static roll model could be simplified, at least for certain applications. This would greatly reduce the number of input data required and hence the effort needed to obtain them.

E. To aid engineering practitioners in industry to utilize the various simulation models in a cost-effective manner, defining the appropriate areas of application of different models is of significance. This will provide guiding principles for the practitioner to select the appropriate model for a particular application. To achieve this objective, it appears that further work on the experimental evaluation of various models will be required.

F. Based on the results of this study, it appears that a sophisticated simulation model does not necessarily guarantee a more accurate prediction than a simpler one. On the other hand, a sophisticated model generally requires a large number of input data. Many of them can only be obtained using special measuring equipment. Quite often, even if the equipment is available, the cost of obtaining the required data is high. It appears that a comprehensive parametric sensitivity study of these sophisticated models may be useful. The objective is to evaluate the relative significance of various parameters to vehicle dynamic behaviour. If some of the parameters

are judged to have an insignificant effect, then they may be excluded. This will make it easier and less costly for the user of the models to obtain input data.

G. Some of the simulation models evaluated in this study have primarily been developed by researchers and for researchers. They are not structured in a "user-friendly" manner. The procedure for inputting data to these models is not particularly convenient to an ordinary user and considerable effort may be required to interpret the outputs. To make the simulation techniques more useful to engineering practitioners, further work on streamlining the structure of the models, particularly the input and output, is recommended.

H. Based on the results of this study and on the current state of the simulation techniques for the lateral dynamics of articulated vehicles, a more realistic goal, for the foreseeable future, for the development of computer simulation models is to provide a common basis for evaluating the dynamic performance of different vehicles on a relative basis, rather than to accurately reproduce their actual dynamic behaviour in minute detail.

REFERENCES

1. C. D. Winkler, C. Mallikarjunarao and C. C. MacAdam, Analytical test plan: Part I - description of simulation models, parametric analysis of heavy truck dynamic stability, Report of the University of Michigan Transportation Research Institute, April 1981.
2. J. Y. Wong and M. El-Gindy, Computer simulation of heavy vehicle dynamic behaviour, User's guide to the UMTRI models, Technical Report No. 3, Vehicle Weights and Dimensions Study, Roads and Transportation Association of Canada, June 1985.
3. F. Vlk, Lateral dynamics of commercial vehicle combinations, a literature survey, Vehicle System Dynamics, Vol. 11, pp. 305 - 324, 1982.
4. H. T. Moncarz, J. E. Bernard, and P. S. Fancher, A simplified, interactive simulation for predicting the braking and steering response of commercial vehicles, Report No. UM-HSRI-PF-75-8, The University of Michigan, Highway Safety Research Institute, August 1975.
5. R. D. Ervin, R. L. Nisonger, C. Mallikarjunarao, and T. D. Gillespie, The yaw stability of tractor-semitrailers during cornering, Report No. DOT HS-805 141. PB80-116775, U. S. Department of Commerce, National Technical Information Service, June 1979.
6. J. Y. Wong and J. Woodroffe, Course Notes for the "Introductory Workshop on Computer Simulation of the Handling and Braking of Heavy Vehicle Combinations", Roads and Transportation Association of Canada, July 1985.

7. P. S. Fancher, Jr., C. Mallikarjunarao, and R. L. Nisonger, Simulation of the directional response characteristics of tractor-semitrailer vehicles, Report No. UM-HSRI-79-9, PB80-189632, U. S. Department of Commerce, National Technical Information Service, March 1979.

APPENDIX A

Vehicle Configuration 1

Input Data Files

5-AXLE TRACTOR-SEMI TRAILER (CONF. 1)

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400	6900	1, 127	20300	27920	7, 1, 83
500	7000	3, 1, 337	20400	27922	10, 1, 968
600	7100	4, 1, 423	20500	27924	06
602	7200	7, 1, 617	20600	27926	0, 0
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606	7400	06	20800	27930	3, 1, 310
608	7500	0, 0	20900	27932	4, 1, 394
610	7600	1, 1, 092	21000	27936	7, 1, 593
612	7700	3, 1, 254	21100	27938	10, 1, 735
614	7800	4, 1, 323	21200	27940	06
616	8000	7, 1, 482	21300	27942	0, 0
618	8050	10, 1, 591	21400	27944	1, 1, 082
620	8100	01	21500	27946	3, 1, 229
622	8200	0	21900	27948	4, 1, 294
624	8400	01	22000	27952	7, 1, 439
626	8700	0	22100	27954	10, 1, 584
628	9700	1,	22200	27956	01
000	9800	28000	22300	27970	0
900	13000	0, 0	22400	27989	01
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1200	14100	5700	22600	27999	1,
1300	14200	20, 3	22700	27998	28000
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1600	14500	50,	23000	28200	3300,
1700	14600	50,	23100	28300	19, 5
1800	14700	0, 0	23200	28400	115,
1900	14800	1500,	23300	28500	13,
2000	17000	10,	23400	28600	-2,
2100	17100	250,	23500	28700	20000
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2400	17400	0, 1	25900	29000	3300,
2500	17500	0, 0	26000	29100	19, 5
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4700	18700	72	27100		
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4900	18900	13	27300		
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7900	21900	20, 3			
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8600	22600	9700			
8700	22700	20, 3			
8800	22800	115			
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9300	23300	06			
9400	23400	9700			
9500	23500	20, 3			
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2000, 4000, 7000

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 500 71.89,239.17
 600 1460 0.2760 0.2760 0.2460 0.2460 0.0.0
 650 0.0.0.0.0
 700 63.07,0.1.10.1.1.0
 800 220.400.400.400.400.400.0.0
 850 0.0.0.0.0
 900 28000.28000.28000.28000.0.0.0.0
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 1300 0.0.0.0
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APPENDIX B

Vehicle Configuration 2

Input Data Files

VAX/VMS RTAC
VAX/VMS RTAC
VAX/VMS RTAC

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P4CONF2 21-APR-1985 11:35 LPBO: 21-APR-1985 11:35
P4CONF2 21-APR-1985 11:35 LPBO: 21-APR-1985 11:35

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DISK\$VAXUSER1:(USER).RTAC:P4CONF2.DAT;1
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R R	T T	A A	C C
RRRR	T T	A A	C C
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R R	T T	A A	C C
R R	T T	A A	CCCC

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DD	AA	TT	1111	1111
DD	AA	TT	1111	1111
DD	AA	TT	1111	11
DD	AA	TT	1111	11
DD	AA	TT	1111	11
DD	AAAAA	TT	1111	11
DD	AAAAA	TT	1111	11
DD	AA	TT	11	11
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DDDDDDDD	AA	TT	11	111111
DDDDDDDD	AA	TT	11	111111

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R R	T T	A A	C C
RRRR	T T	A A	C C
R R	T T	AAAA	C C
R R	T T	A A	C C
R R	T T	A A	CCCC

P4CONF2 21-APR-1985 11:35 LPBO: 21-APR-1985 11:35
P4CONF2 21-APR-1985 11:35 LPBO: 21-APR-1985 11:35
P4CONF2 21-APR-1985 11:35 LPBO: 21-APR-1985 11:35

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DISK\$VAXUSER1:(USER).RTAC:P4CONF2.DAT;1

5-ALE TRACTOR-SEMITRAILER (CONF 2)

Year	Quantity	Description	Weight (lb)	Volume (cu ft)	Price (\$)	Weight (lb)	Volume (cu ft)	Price (\$)
100	1		8050	10	591	21500	0	27948
200	01		8100	01		21900	410	27932
300	65		8200	0		22000	6552 29	27934
400	003		8400	01		22100	1106 71	27936
500	0	0	8700	0		22200	69	27970
600	0 3--3	121--2 80	9700	1		22300	73000	27989
700	10 1--3	121--2 06	9800	21000		22400	789 69	27994
800	0 0		13000	0 0		22500	789 69	27997
900	0 0		13900	1320		22600	182	27998
1000	10 0		14100	3700		22800	64 5	28000
1200	6 0		14200	20 3		22900	37500	28200
1300	0 1		14300	103		23000	1727000	28300
1400	00		14400	01		23100	1727000	28400
1500	11100000		14500	50		23200	01	28500
1600	142		14600	50		23300	49 5	28600
1700	1077 93		14700	0 0		23400	50	28700
1800	7118 07		14800	1500		23500	0 0	28800
1900	39 7		17000	10		23600	9587 5	28900
2000	18166 6		17100	250		23800	10	29100
2100	69933		17200	4450		23900	950	29200
2200	69933		17300	22		26000	4100	29300
2300	0 0		17400	0 1		26100	25 6	29400
2400	0 0		17500	0 0		26200	0 1	29500
2500	40 5		17600	35		26300	0	29600
2600	120000		17700	72		26400	38	29700
2700	36		17800	2340		26500	72	29800
2800	1042 5		17900	1500		26600	1320	29900
4000	10		18000	10		26700	9507 5	29900
4100	900		18100	250		26800	0	30000
4200	3719		18200	4458		26900	1500	
4300	24 53		18300	22		27000	4100	
4400	0 00		18400	0 1		27100	25 6	
4500	109385		18500	78000		27200	0 1	
4600	32 6		18600	35		27300	0	
4700	00 5		18700	72		27400	38	
4800	1190		18800	2170 0		27500	72	
4900	0		18900	13		27600	1520	
5000	-1		19000	-1		27700	13	
5600	03		19100	28000		27800	-2	
5700	2000	6000 9000	19200	0 0		27900	03	
5800	01		19300	1200		27902	2000 6000 9000	
5900	63		19400	5700		27904	01	
6000	06		19500	20 3		27906	63	
6100	0 0		19600	115		27908	06	
6200	1 218		19700	13		27910	0 0	
6300	3 5325		19800	-1		27912	1 1 183	
6400	4 6555		19900	28000		27914	3 4 468	
6500	7 697		20000	0		27916	4 5 595	
6650	10 1 022		20900	5700		27920	7 1 183	
6700	06		20300	20 3		27922	10 1 968	
6800	0 0		20400	115		27924	06	
6900	1 127		20500	0		27926	0 0	
7000	3 337		20600	0 05		27928	1 1 114	
7100	4 423		20700	0 25		27930	3 4 310	
7300	7 617		20800	0		27932	4 5 394	
7350	10 1 737		20900	0		27936	7 1 593	
7400	06		20900	0		27938	10 1 735	
7500	0 0		21000	0 075		27940	06	
7600	1 072		21100	0 25		27942	0 0	
7700	3 234		21200	0		27944	1 1 902	
7800	4 351		21300	0 075		27946	3 1 229	
8000	7 402		21400	0 25				

3-AXLE TRACTOR-SEMITRAILER (CONF. 2)

100	0000	2000, 44, 77, 84, 85, 79, 59
200	63 07, 4, 1, 02	4000, 103, 203, 236, 252, 245, 187,
300	3, 2	6000, 153, 341, 376, 431, 435, 333
400	10316, 54881	8000, 205, 472, 550, 622, 600, 470,
500	10166, 111034 04	9000, 227, 537, 637, 716, 673, 550
600	69955, 2517592 06	0607
700	69955, 2517038	0, 1, 3, 4, 5, 7, 10,
800	34 7, 65, 671	7100, 200, 31, 44, 46, 54, 61, 39,
900	0097 929, 15781, 399, 15611, 379, 16823 137, 16823, 137	4000, 180, 143, 157, 109, 194, 158,
1000	1190, 2340, 2170, 1520, 1520	7300, 6000, 130, 261, 299, 354, 373, 329,
1100	3719, 4458, 4458, 4100, 4100,	8000, 179, 387, 459, 532, 562, 473,
1200	35, 9, -81, 1, -131, 1, -156, 6, -206, 1	9000, 200, 452, 533, 624, 650, 569
1300	20 3, 20, 3, 20, 3, 19, 5, 19, 5	7600 1,
1400	24, 55, 22, 22, 25, 6, 25, 6	7700 2
1500	16, 3, 17, 5, 17, 5, 19, 17,	7800 0, 0,
1600	40, 25, 36, 36, 36, 36	7900 5, -1, 5, -1, 5
1700	0, 0, 13, 13, 13, 13,	
1800	5700, 5700, 5700, 5300, 5300,	
1900	0, 1, 1, 1, 1, 1	
2000	109385, 0, 78000, 0, 0,	
2100	500, 250, 250, 950, 950,	
2200	10, 10, 10, 10, 10, 10	
2300	-106, 1, 229	
2400	48 5	
2500	9799997	
2600	01	
2700	03	
2800	0102020303	
2900	03	
3000	-10125, -10,	
3100	0, 0, 0, 0,	
3200	10125, 10,	
3300	03	
3400	-15000, -10	
3500	0, 0, 0, 0,	
3600	15000, 10	
3700	03	
3800	-95875, -10	
3900	0, 0, 0, 0,	
4000	95875, 10	
4100	02	
4200	0101010202	
4300	0607	
4400	0, 0, 1 0, 3, 4, 5, 7, 10	
4500	2000, 436, 1065, 1311, 1506, 1794, 2044,	
4600	4000, 635, 1657, 2072, 2430, 2957, 3442,	
4700	6000, 764, 2421, 2539, 3019, 3701, 4422,	
4800	8000, 831, 2525, 2627, 3384, 4190, 5086	
4900	9000, 830, 2281, 2909, 3487, 4341, 5319,	
5000	0607	
5100	0, 0, 1 0, 3, 4, 5, 7, 10,	
5200	2000, 365, 936, 1171, 1371, 1640, 1939,	
5300	4000, 556, 1503, 1910, 2203, 2614, 3400,	
5400	6000, 686, 1608, 2063, 2321, 3570, 4408,	
5500	8000, 737, 2025, 2576, 3135, 4012, 5030,	
5600	9000, 742, 2058, 2646, 3213, 4131, 5156,	
5700	02	
5800	0101010202	
5900	0607	
6000	0 0, 1, 0, 3, 4, 5, 7, 10,	
6100		
6200		
6300		

VAX/VMS
VAX/VMS
VAX/VMS

DISK#VAXUSER1: (USER) RTAC)TBSCONF2. DAT; 1
DISK#VAXUSER1: (USER) RTAC)TBSCONF2. DAT; 1
DISK#VAXUSER1: (USER) RTAC)TBSCONF2. DAT; 1

LPBO: 21-APR-1985 15:22
LPBO: 21-APR-1985 15:22
LPBO: 21-APR-1985 15:22

TDSCONF2 21-APR-1985 15:22
TDSCONF2 21-APR-1985 15:22
TDSCONF2 21-APR-1985 15:22

RTAC
RTAC
RTAC

RRRR TTTT AAA CCCC
R R T A A C
H R T A A C
RRRR T A A C
R R T A A A A C
R R T A A C
R R T A A C C C C C

TTTTTTTT DDBBBBB SSSSSSS CCCCCCC 00000 NN JFFFFFFF 22222
TTTTTTTT DDBBBBB SSSSSSS CCCCCCC 00000 NN JFFFFFFF 22222
TT DB DB SS CC CC UR NN FF 22
TT DB DB SS CC CC UB NN FF 22
TT DB DB SS CC CC UD NN FF 22
TT DDBBBBB SSSSS CC CC NN NN FF 22
TT DB DB SS CC CC NN NN FF 22
TT DB DB SS CC CC NN NN FF 22
TT DB DB SS CC CC NN NN FF 22
TT DDBBBBB SSSSSSS CCCCCCC 00000 NN FF 22
TT DDBBBBB SSSSSSS CCCCCCC 00000 NN FF 22

DDDDDDDD AAAA TTTTTTTT JJJ
DDDDDDDD AAAA TTTTTTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AAAA AAAA TT TTTT JJJ
DD AAAA AAAA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ
DD AA AA TT TTTT JJJ

RRRR TTTT AAA CCCC
R R T A A C
R R T A A C
RRRR T A A C
R R T A A A A C
R R T A A C

DISK#VAXUSER1: (USER) RTAC)TBSCONF2. DAT; 1
DISK#VAXUSER1: (USER) RTAC)TBSCONF2. DAT; 1
DISK#VAXUSER1: (USER) RTAC)TBSCONF2. DAT; 1

LPBO: 21-APR-1985 15:22
LPBO: 21-APR-1985 15:22
LPBO: 21-APR-1985 15:22

TDSCONF2 21-APR-1985 15:22
TDSCONF2 21-APR-1985 15:22
TDSCONF2 21-APR-1985 15:22

RTAC
RTAC
RTAC

VAX/VMS
VAX/VMS
VAX/VMS

100 05-AXLE TRACTOR-SEMITRAILER (CONF. 1 & 2)
 200 16016 0.07751.0
 300 192915 0.2775432 0
 400 63.11.53 07.103.09.147 08.196 58.0 0.0.0.0.0.0.0.0.0.0.0
 500 78.87.238.17
 600 1460 0.2760.0.2760.0.2460 0.2460.0.0.0
 650 0.0.0.0.0.
 700 63.07.0.1.10.0.1 0
 800 220.400.400.400.400.400.400.0.0
 850 0.0.0.0.0.
 900 28000.28000.28000.28000.28000.0.0.0.0
 950 0.0.0.0.0.
 1000 13.0.13.0.13 0.13.0.0.0.0.0.0.0.0.0.0.0.0.0.0
 1100 6.0.0.0.1.1
 1200 03
 1300 0.0.0.0
 1400 0.5-2.0
 1500 6.0-2.0

APPENDIX C

Vehicle Configuration 3

Input Data Files

VAX/VMS RTAC
VAX/VMS RTAC
VAX/VMS RTAC

P4CONF3 21-APR-1985 11:35 LP80: 21-APR-1985 11:36
P4CONF3 21-APR-1985 11:35 LP80: 21-APR-1985 11:36
P4CONF3 21-APR-1985 11:35 LP80: 21-APR-1985 11:36

DISK\$VAXUSER1: [USER1. RTAC]P4CONF3. DAT; 1
DISK\$VAXUSER1: [USER1. RTAC]P4CONF3. DAT; 1
DISK\$VAXUSER1: [USER1. RTAC]P4CONF3. DAT; 1

RRRR TTTT AAA CCCC
R R T A A C
R R T A A C
RRRR T A A C
R R T A A A A C
R R T A A C
R R T A A C C C C

PPPPPPP 44 44 CCCCCC 000000 NN FFFFFFFF 333333
PPPPPPP 44 44 CCCCCC 000000 NN FFFFFFFF 333333
PP 44 44 CC 00 00 NN NN FF 33
PP 44 44 CC 00 00 NN NN FF 33
PP 44 44 CC 00 00 NN NN FF 33
PP 44 44 CC 00 00 NN NN FF 33
PPPPPPP 44 44 44 44 44 44 CC 00 00 NN NN FFFFFFFF 33
PPPPPPP 44 44 44 44 44 44 CC 00 00 NN NN FFFFFFFF 33
PP 44 44 CC 00 00 NN NN NN NN FF 33
PP 44 44 CC 00 00 NN NN NN NN FF 33
PP 44 44 CC 00 00 NN NN NN NN FF 33
PP 44 44 CC 00 00 NN NN NN NN FF 33
PP 44 44 CCCCCC 000000 NN NN FF 33
PP 44 44 CCCCCC 000000 NN NN FF 333333

....
....
....

DDDDDDD AAAAA TTTTTTTT 1111 11
DDDDDDD AAAAA TTTTTTTT 1111 11
DD AA AA TT 1111 1111
DD AA AA TT 1111 1111
DD AA AA TT 1111 1111
DD AA AA TT 1111 1111
DD AAAAAAAA TT 1111 1111
DD AAAAAAAA TT 1111 1111
DD AA AA TT 11 11
DD AA AA TT 11 11
DDDDDDD AA AA TT 111111
DDDDDDD AA AA TT 111111

11
11
1111
1111
11
11
11
11
11
11
11
111111
111111

RRRR TTTT AAA CCCC
R R T A A C
R R T A A C
RRRR T A A C
R R T A A A A C
R R T A A C C C C

VAX/VMS RTAC
VAX/VMS RTAC
VAX/VMS RTAC

P4CONF3 21-APR-1985 11:35 LP80: 21-APR-1985 11:36
P4CONF3 21-APR-1985 11:35 LP80: 21-APR-1985 11:36
P4CONF3 21-APR-1985 11:35 LP80: 21-APR-1985 11:36

DISK\$VAXUSER1: [USER1. RTAC]P4CONF3. DAT; 1
DISK\$VAXUSER1: [USER1. RTAC]P4CONF3. DAT; 1
DISK\$VAXUSER1: [USER1. RTAC]P4CONF3. DAT; 1

3-AXLE TRACTOR-SEMITRAILER (CONF. 3)

100	6700	12.1.833	05	18900	23000	5623.1.1.
200	6900	06	0.	19000	13.	10123.1.5
300	6800	06	4.	17100	-1.	25200
400	6900	0.0.	8.	19200	-2.	13187.2.9
500	7000	1.1.143	12.	19300	0.0	23400
600	7100	2.1.252	16	19400	1200.	25500
700	7200	4.1.458	1.	19500	4500.	25600
800	7300	6.1.501	1.1.1.1.1.1.	19600	19.5	25700
900	7400	12.1.673	.75.75.75.75.75.1.	17700	115.	25800
1000	7500	06	3.1.5.6.9.75	19800	13.	25900
1100	7600	0.0.	4.4.45.85.95	19900	-1.	26000
1200	7700	1.1.107	0.0	20000	-2.	26100
1300	7800	2.1.194	0.0	20100	0.	26200
1400	7900	4.1.380	0.0.3.0.0.8.	20200	1200.	26300
1500	8000	6.1.510	4500.	20300	4500.	26400
1600	8100	12.1.685	19.5	20400	19.5	26500
1700	8200	03	14400	20500	115.	26600
1800	8300	0.	14500	20600	0.05	26700
1900	8400	.04	14600	20700	0.29	26800
2000	8500	.1	14700	20800	1000.	26900
2100	8600	.9	14800	20900	0.	27000
2200	8700	1.	14900	21000	0.	27100
2300	8800	05	15000	21100	0.075	27200
2400	8900	0.	15100	21200	0.25	27300
2500	9000	4.	15200	21300	1500.	27400
2600	9100	8.	15300	21400	0.075	27500
2700	9200	12.	15400	21500	0.25	27600
2800	9300	16.	15500	21600	1500.	27700
2900	9400	1.1.1.9.3.1	6500.1.9	21700	432.	27800
3000	9500	1.1.1.9.3.1	9500.2	21700	0.	27900
3100	9600	1.1.1.9.35.13	13000.2.5	21800	4500.	28000
3200	9700	1.1.1.9.42.17	17000.3.	21900	7500.	28100
3300	9800	1.1.1.9.48.22	30000.4.0	22000	60.0	28200
3400	9900	0.	0.02	22100	60000.	115.
3500	10000	03	16100	22200	750000.	13.
3600	10100	3000.4000.9000.	0.1.8	22300	750000.	13.
3700	10200	01	16300	22400	52500.	-1.
3800	10300	66.	16400	22400	52500.	-2.
3900	10400	09	16500	22500	213.94	0.
4000	10500	0.0.	5000.1.5	22600	85.0	1200.
4100	10600	1.1.68	0000.2	22700	132000	28800
4200	10700	2.1.80	16700	22800	3050000	19.5
4300	10800	3.1.77	16800	22900	3100000.	115.
4400	10900	1.0.53	16900	23000	01	29100
4500	11000	03	17000	23100	48.0	29200
4600	11100	0.0.	17100	23200	50.	29300
4700	11200	1.1.59	17200	23300	0.0	29400
4800	11300	2.1.75	17300	23400	-122.	29500
4900	11400	3.1.73	17400	23500	09	29600
5000	11500	1.1.50	17500	23600	0.1.5	29700
5100	11600	05	17600	23700	0.0.	29800
5200	11700	0.0.	17700	23800	3375.0.5	0.
5300	11800	1.1.44	17800	23900	7312.1.	24000
5400	11900	2.1.70	18000	24000	11812.1.5	24100
5500	12000	3.1.69	18100	24200	16973.2.	24200
5600	12100	1.1.45	18200	24300	22500.2.5	24300
5700	12200	05	18300	24400	56250.3.	24400
5800	12300	0.	18400	24500	0.02	24500
5900	12400	.04	18500	24600	-35000.11.	24600
6000	12500	.1	18600	24700	0.1.3	24700
6100	12600	.5	18700	24800	0.0.2	24800
6200	12700	1.	18800	24900	1687.0.5	24900

VAX/VMS
VAX/VMS
VAX/VMS

RTAC RTAC VRCNF3 21-APR-1985 11:55 LPD0: 21-APR-1985 11:55 D1S1#VAXUSER1: {USER1, RTACJYRCNF3, DAT1, 1
RTAC VRCNF3 21-APR-1985 11:55 LPD0: 21-APR-1985 11:55 D1S1#VAXUSER1: {USER1, RTACJYRCNF3, DAT1, 1
RTAC VRCNF3 21-APR-1985 11:55 LPD0: 21-APR-1985 11:55 D1S1#VAXUSER1: {USER1, RTACJYRCNF3, DAT1, 1

VAX/VMS
VAX/VMS
VAX/VMS

RRRR TTTT AAA CCCC
R R T A A C
R R T A A C
RRRR T A A C
R R T A A C
R R T A A C
R R T A A C

YY YY RRRRRR CCCCCC ODDDDD NN FFFFFFFF 303333
YY YY RRRRRR CCCCCC ODDDDD NN FFFFFFFF 303333
YY YY RR RR CC DD NN NN FF 33
YY YY RR RR CC DD NN NN NN FF 33
YY YY RR RR CC DD NN NN NN FF 33
YY YY RR RR CC DD NN NN NN FF 33
YY YY RRRRRR CC DD NN NN FFFFFFFF 33
YY YY RRRRRR CC DD NN NN FFFFFFFF 33
YY YY RR RR CC DD NN NN NN FF 33
YY YY RR RR CC DD NN NN NN FF 33
YY YY RR RR CC DD NN NN NN FF 33
YY YY RR RR CC DD NN NN NN FF 33
YY YY RR RR CCCCCC ODDDDD NN FF 33
YY YY RR RR CCCCCC ODDDDD NN FF 33

DDDDDD AAAA TTTTTTTT
DDDDDD AAAA TTTTTTTT
DD DD AA AA AA AA TTTT 1111
DD DD AA AA AA AA TTTT 1111
DD DD AA AA AA AA TTTT 1111
DD DD AA AA AA AA TTTT 1111
DD DD AA AA AA AA TTTT 1111
DD DD AA AA AA AA TTTT 1111
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DD DD AA AA AA AA TTTT 1111
DD DD AA AA AA AA TTTT 1111
DD DD AA AA AA AA TTTT 1111
DD DD AA AA AA AA TTTT 1111
DD DD AA AA AA AA TTTT 1111

RRRR TTTT AAA CCCC
R R T A A C
RRRR T A A C
R R T A A C
R R T A A C

VAX/VMS
VAX/VMS
VAX/VMS

RTAC RTAC VRCNF3 21-APR-1985 11:55 LPD0: 21-APR-1985 11:55 D1S1#VAXUSER1: {USER1, RTACJYRCNF3, DAT1, 1
RTAC VRCNF3 21-APR-1985 11:55 LPD0: 21-APR-1985 11:55 D1S1#VAXUSER1: {USER1, RTACJYRCNF3, DAT1, 1
RTAC VRCNF3 21-APR-1985 11:55 LPD0: 21-APR-1985 11:55 D1S1#VAXUSER1: {USER1, RTACJYRCNF3, DAT1, 1

VAX/VMS
VAX/VMS
VAX/VMS

5-AXLE TRACOR-SEMTRAILER (CONF. 3)

100 0005
 200 52 5. 6 . 1. 02
 400 00302
 500 7700, 61500.
 600 13000, 204440.
 700 75000, 3813523
 800 75000, 3850003.
 900 44, 01, 3
 1000 12000, 17000, 17000, 17000, 17000.
 1100 1300, 2300, 2300, 1500, 1500.
 1200 3719, 4458, 4458, 4100, 4100.
 1300 28. B, -91. 2, -139. 2, -190. 2, -238. 2
 1400 19, 5, 19, 5, 19, 5, 19, 5
 1500 23, 27, 27, 27, 27, 29
 1600 16, 19, 19, 19, 19
 1700 40, 27, 5, 29, 5, 29, 5, 29, 5
 1800 0, 13, 13, 13, 13
 1900 4500, 4500, 4500, 4500, 4500, 4500.
 2000 0, 0, 0, 0, 0
 2100 1500, 6000, 6000, 10000, 10000.
 2200 300, 1000, 1000, 1000, 1000.
 2300 0, 0, 0, 0, 0.
 2400 -100 05, 217, 8
 2500 48
 2600 1000000.
 2700 01
 2800 03
 2900 0102020303
 3000 04
 3100 -20000, -20
 3200 0, 0.
 3300 0645, 7, 2
 3400 25000, 7, 5
 3500 09
 3600 -22500, -11.
 3700 0, -1
 3800 0, 0.
 3900 3500, 1.
 4000 3750, 1, 5
 4100 0750, 2.
 4200 12250, 2, 5
 4300 16250, 3
 4400 45000, 4.
 4500 09
 4600 -32500, -11.
 4700 0, -1, 5
 4800 0, 0.
 4900 2531, 0, 5
 5000 6469, 1.
 5100 10969, 1, 5
 5200 16031, 2.
 5300 21656, 2, 5
 5400 50625, 3
 5500 01
 5600 0101010101
 5700 0404
 5800 0, 1, 0, 2, 0, 4, 0, 4, 0, 12, 0
 5900 3000, 540, 990, 1710, 2130, 2470.
 6000 4000, 4140, 1500, 02700, 3900, 4140
 6100 7000, 790, 1710, 3420, 4680, 6210.

6200 02
 6300 0102020202
 6400 0407
 6500 0, 0, 1, 0, 3, 0, 4, 0, 5, 0, 7, 0, 10, 0
 6600 3000, 33, 12, 100, 120, 123, 100.
 6700 6000, 130, 261, 300, 354, 373, 332.
 6800 9000, 200, 452, 533, 625, 650, 565.
 6900 0403
 7000 0, 1, 2, 3, 4.
 7100 3000, 29, 42, 44, 38
 7200 6000, 92, 150, 157, 146.
 7300 9000, 152, 269, 329, 335
 7400 1.
 7600 003
 7700 0, 0, 0, 0
 7800 0, 5, 2, 5, 2, 5
 7900 10, 2, 5, 2, 5

09:54 APR 22 '85 TBSCONF3.FBDELGIP

N
 Y
 Y
 05
 000
 1111
 15500,
 64500,
 214217,
 4202900,
 48,
 48,
 60.76
 83.24
 227.72
 204.2
 14.35
 40,
 36,
 36,
 48,
 34.83
 78.43
 0.0
 .11
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 0.0
 37.
 8,
 30,
 800,
 620,
 620.
 Y
 0.9
 0.0
 0.0
 0.0
 0.
 02
 0.0,0.0,0.0,0.0,0.0,
 5.0,0.0,0.0,0.0,0.0,
 02
 0.0,0.0
 .5r2.5
 N
 N
 N
 Y
 0.0
 N
 N
 N
 N
 N
 N
 N
 N
 06
 04,08,03,07,05,21
 0.2

0.1
N
Y
N

100 05-AXLE TRACTOR-SEMITRAILER (CONF. 3 & 4)
 200 15500 , 64500
 300 214217 , 4202400
 400 60.76, 59.24, 107.24, 180 28,228, 28,0 , 0,0 , 0,0 , 0,0 , 0,
 500 68,89,227,723
 600 1600 , 2480 , 2480 , 2400 , 2480 , 0,
 700 0,0 , 0,0 , 0,
 800 52.5, 1,10, 1,05
 900 267,400 , 400 , 400 , 400 , 0
 1000 0,0 , 0,0 , 0,
 1100 28000 , 28000 , 28000 , 28000 , 0,0 , 0,
 1200 0,0 , 0 , 0,
 1300 13,13,13,13,0,0,0,0,0,0,0,0,
 1400 B., 0011,1
 1500 03
 1600 0,10
 1700 .5,2 6
 1800 10,2 6

APPENDIX D
Vehicle Configuration 4
Input Data Files

3-WALE TRACTOR-SEMI TRAILER (CONF. 4)

100	01	6700	12. . . 833	12600	05	18900	2300.	25000	5625. . 1.
200	04. 5	6800	06	12700	0.	19000	13.	25100	10125. . 1. 5
300	003	6900	0. 0.	13000	4.	19100	-1.	25200	13187. . 2.
400	0. 0.	7000	1. . . 143	13100	B.	19200	-2	25300	20812. . 2. 5
500	0. 5. 2. 5. 2. 5	7100	2. . . 232	13200	12.	19300	0. 0	25400	45030. . 3.
600	10. . 2. 5. 2. 5	7200	4. . . 458	13300	16.	19400	1200.	25500	0. 0. 02
700	04	7300	6. . . 501	13400	1. . . 1. . . 1. . . 1.	19500	4500.	25600	0. 0
800	0. 0	7400	12. . . 693	13500	1. . . 1. . . 1. . . 1.	19600	19. 3.	25700	0. 0
900	2. 5. 0.	7500	06	13600	. 75. . 75. . 75. . 95. . 1.	19700	113.	25800	4100.
1000	2. 6. 0.	7600	0. 0.	13700	. 5. . 5. . 6. . 9. . 95.	19800	13.	25900	29.
1100	10. . 0.	7700	1. . . 107	13800	. 4. . 4. . 45. . 05. . 93	19900	-1.	26000	0.
1200	0.	7800	2. . . 194	13900	0. 0	20000	-2.	26100	0. 0
1300	0. 1	7900	4. . . 300	14000	-1600.	20100	0.	26200	38.
1400	00	8000	6. . . 510	14100	0. . 0. . 3. 0. 0. B.	20200	1200.	26300	72.
1500	11100000	8100	12. . . 685	14200	4500.	20300	4300.	26400	1500.
1600	1700	8200	03	14300	19. 3	20400	19. 5	26500	-122.
1700	0760.	8300	0.	14400	103.	20500	113.	26600	0.
1800	6540.	8400	. 04	14500	01	20600	0. 05	26700	0.
2000	44.	8500	. 1	14600	40.	20700	0. 29	26800	4100.
2100	15000.	8600	. 5	14700	50	20800	1000.	26900	29.
2200	75000.	8700	1.	14800	0. 0	20900	0	27000	0.
2300	75000.	8800	03	14900	-121.	21000	0	27100	0.
2400	0. 0	8900	0.	15000	09	21100	0. 075	27200	38.
2500	14. 35	9000	4.	15100	-20000. . -11.	21200	0. 25	27300	72.
2600	40. 0	9100	0.	15200	0. . -1.	21300	1300.	27400	1500.
2700	50000.	9200	12.	15300	0. . 0.	21400	0. 073	27500	13.
2800	-119.	9300	16.	15400	4000. . 1. 5	21500	0. 25	27600	-1.
2900	04	9400	1. . . 1. . . 9. . 3. . 1	15500	6500. . 1. 5	21600	1500.	27700	-2.
3000	-20000. . -20.	9500	1. . . 1. . . 9. . 3. . 1	15600	9500. . 2	21700	432.	27800	0.
3100	0. 0.	9600	1. . . 1. . . 9. . 35. . 13	15700	13000. . 2. 5	21800	4500.	27900	1200.
3200	9250. . 7. 2	9700	1. . . 1. . . 9. . 42. . 17	15800	17000. . 3.	21900	7500	28000	4500.
3300	25000 . 7. 5	9800	1. . . 1. . . 9. . 40. . 22	15900	50000. . 4. 0	22000	60. 0	28100	19. 5
3400	0. 08	9900	-2.	16000	0. 02	22100	60000.	28200	113.
3500	0. 0	10000	03	16100	-25000. . -11.	22200	750000.	28300	13
3600	-20000. . -20.	10100	3000. . 6000 . 7000.	16200	0. . - . B	22300	750000.	28400	-1.
3700	0. 0	10200	01	16300	0. . 0. . 2	22400	32500.	28500	-2.
3800	0040. . 7. 2	10300	66.	16400	3000. . 1.	22500	213. 94	28600	0.
3900	25000 . 7. 5	10400	03	16500	5000. . 1. 5	22600	83. 0	28700	1200.
4000	0. 08	10500	0. 0.	16600	0000. . 2.	22700	132000.	28800	4500.
4100	0.	10600	1. . 60	16700	11500. . 2. 5	22800	3050000.	28900	19. 5
4200	0.	10700	. 2. . 80	16800	15500. . 3.	22900	3100000.	29000	115.
4300	3719.	10800	3. . 77	16900	40000. . 4	23000	01	29100	0. 175
4400	23.	10900	1. 0. . 55	17000	0. 02	23100	48. 0	29200	. 25
4500	0. 00	11000	05	17100	0. 0	23200	50.	29300	1500.
4600	0. 0	11100	0. 0.	17200	0. 0	23300	0. 0	29400	0. 175
4700	32.	11200	. 1. . 39	17300	4450.	23400	-122.	29500	. 23
4800	00. 0	11300	. 2. . 75	17400	29.	23500	09	29600	1500.
4900	1200.	11400	. 3. . 73	17500	0. 0	23600	-30000. . -11.	29700	-1
5000	0. 0	11500	1. . . 50	17600	0. 0	23700	0. . -1. 5	29800	00
5100	-1	11600	05	17700	38.	23800	0. . 0.		
5200	3000. . 6000. . 7000.	11700	0. . 0.	17800	72.	23900	3375. . 0. 5		
5300	01	11800	. 1. . 44	17900	2300.	24000	7312. . 1.		
5400	66.	11900	. 2. . 70	18000	-121.	24100	11812. . 1. 5		
5500	0. 0.	12000	. 3. . 69	18100	0.	24200	16875. . 2		
5600	0. 0.	12100	1. . . 45	18200	0	24300	22500. . 2. 5		
5700	03	12200	05	18300	4450.	24400	36250. . 3		
5800	1. . . 103	12300	0.	18400	29.	24500	0. 02		
5900	2. . . 333	12400	. 04	18500	0.	24600	-35000. . -11.		
6000	4. . 575	12500	. 1	18600	78000.	24700	0. . -1. 3		
6100	6. . 708	12600	. 5	18700	38.	24800	0. . 0. 2		
6200		12700	. 1	18800	72	24900	1417. . 0. 5		

VAX/VMS RTAC
VAX/VMS RTAC
VAX/VMS RTAC

YRCONF4 21-APR-1985 11:57 LPB0: 21-APR-1985 11:57
YRCONF4 21-APR-1985 11:57 LPB0: 21-APR-1985 11:57
YRCONF4 21-APR-1985 11:57 LPB0: 21-APR-1985 11:57

VAX/VMS
VAX/VMS
VAX/VMS

```
RRRR TTTT AAA CCCC  
R R T A A C  
R R T A A C  
RRRR T A A C  
R R T A A C  
R R T A A C  
R R T A A C
```

```
YY YRCONF4 21-APR-1985 11:57 LPB0: 21-APR-1985 11:57  
YY YRCONF4 21-APR-1985 11:57 LPB0: 21-APR-1985 11:57  
YY YRCONF4 21-APR-1985 11:57 LPB0: 21-APR-1985 11:57  
YY  
YY  
YY  
YY  
YY  
YY  
YY  
YY  
YY  
YY  
YY
```

```
RRRRRRRR CCCCCCCC DDDDDD NN FFFFFFFF 44 44  
RRRRRRRR CCCCCCCC DDDDDD NN FFFFFFFF 44 44  
RR RR CC DD NN FF 44 44  
RR RR CC DD NN FF 44 44  
RR RR CC DD NN NN 44 44  
RRRRRRRR CCCCCCCC DDDDDD NN NN FFFFFFFF 44 44  
RR RR CC DD NN NN NN NN NN NN FFFFFFFF 44 44  
RR RR CC DD NN NN NN NN NN NN NN NN FFFFFFFF 44 44  
RR RR TR CC DD NN NN NN NN NN NN NN NN FFFFFFFF 44 44  
RR RR RR CC DD DD DDDDDD NN NN FF 44 44  
RR RR CCCCCCCC DDDDDD NN NN FF 44 44  
RR RR CCCCCCCC DDDDDD NN NN FF 44 44  
RR CCCCCCCC DDDDDD NN NN FF 44 44
```

```
DDDDDDDD AAAAAA TTTTTTTTT TTTT  
DDDDDDDD AAAAAA TTTTTTTTT TTTT  
DD AA AA TTT  
DD AA AA TTT  
DD AA AA TTT  
DD AA AA TTT  
DD AA AA TTT  
DD AAAAAA TTT  
DD AAAAAA TTT  
DD AA AA TTT  
DD AA AA TTT  
DDDDDDDD AA AA TTT  
DDDDDDDD AA AA TTT
```

```
RRRR TTTT AAA CCCC  
R R T A A C  
R R T A A C  
RRRR T A A C  
R R T A A C  
R R T A A C  
R R T A A C
```

VAX/VMS RTAC
VAX/VMS RTAC
VAX/VMS RTAC

YRCONF4 21-APR-1985 11:57 LPB0: 21-APR-1985 11:57
YRCONF4 21-APR-1985 11:57 LPB0: 21-APR-1985 11:57
YRCONF4 21-APR-1985 11:57 LPB0: 21-APR-1985 11:57

VAX/VMS
VAX/VMS
VAX/VMS

5-AXLE TRACOR-SEMITRAILER (CONF 4)

100	12000	17000	17000	17000	17000
200	1200	2300	2300	4500	4500
300	52	5.6	1.1	02	
400	7700	61500			
500	15000	204440			
600	75000	3812523			
700	75000	3650083			
800	44	81	3		
900	12000	17000	17000	17000	17000
1000	1200	2300	2300	4500	4500
1100	3719	4458	4458	4100	4100
1200	28.8	91.2	137.2	190	21-238.2
1300	19	5.19	5.19	5.19	5.19
1400	23	29	29	29	29
1500	16	19	19	19	19
1600	40	29	5.27	5.27	5.27
1700	0	13	13	13	13
1800	4500	4500	4500	4500	4500
1900	0	0	0	0	0
2000	0	0	78000	0	0
2100	300	1000	1000	1000	1000
2200	0	0	0	0	0
2300	100	85	217	0	
2400	4B				
2500	1000000				
2600	01				
2700	03				
2800	04				
2900	-20000	1-20			
3000	0	0			
3100	8645	7	2		
3200	25000	17.5			
3300	07				
3400	-23500	1-11			
3500	0	1-1			
3600	0	0			
3700	3500	11			
3800	5750	1	5		
3900	0750	12			
4000	4200	12250	12	5	
4100	16250	13			
4200	4400	45000	14		
4300	09				
4400	-32500	1-11			
4500	4700	0	1-1	5	
4600	0	0			
4700	2531	0	5		
4800	6467	1			
4900	10987	1	5		
5000	16031	12			
5100	21656	12	5		
5200	50625	13			
5300	01				
5400	0101010101				
5500	0406				
5600	0	1	0	7	0
5700	3060	540	996	1710	2130
5800	6000	0440	1500	2760	3400
5900	4000	970	1710	3320	4210
6000					
6100					

6200 02
6300 0102020202
6400 0407
6500 0 0.1 0.3 0.4 0.3 0.7 0.10 0
6600 3000.55.92.100.120.125.100.
6700 6000.130.261.300.334.373.332.
6800 9000.200.452.533.625.650.565.
6900 0405
7000 0.1 2.3 4.
7100 3000.29.42.44 38.
7200 6000.92.150.157.146.
7300 9000.152.249.329.335
7400 1.
7500 003
7600 0.0 0.
7700 0.5.2 5.2 5
7800 10.2 5.2 5
7900 10.2 5.2 5

VAX/VMS RTAC
VAX/VMS RTAC
VAX/VMS RTAC

TBSCDNF4 30-APR-1985 12:54
TBSCDNF4 30-APR-1985 12:54
TBSCDNF4 30-APR-1985 12:54

LPB0: 30-APR-1985 12:55
LPB0: 30-APR-1985 12:55
LPB0: 30-APR-1985 12:55

TBSCONF4.DAT:1
TBSCONF4.DAT:1
TBSCONF4.DAT:1

VAX/V
VAX/V
VAX/V

RRRR TTTTT AAA CCCC
R R T A A C
R R T A A C
RRRR T A A C
R R T A A A C
R R T A A C
R R T A A C

TTTTTTTT DDDDDDBB SSSSSSSS CCCCCCCC DDDDDD NN FFFFFFFF 44 44
TTTTTTTT DDDDDDBB SSSSSSSS CCCCCCCC DDDDDD NN FFFFFFFF 44 44
TT DB SS SS SS CC CC DD NN FF 44 44
TT DB BB SS SS CC CC DD NN FF 44 44
TT DB BB SS SS CC CC DD NN FF 44 44
TT DB BB SS SS CC CC DD NN FF 44 44
TT DB BB SS SS CC CC DD NN FF 44 44
TT DDDDDDBB SSSSSS CC CC DD NN NN FFFFFFFF 4444444444
TT DDDDDDBB SSSSSS CC CC DD NN NN FFFFFFFF 4444444444
TT BB BB BB BB SS CC CC DD NN NN NN NN FF 44
TT DB BB BB SS CC CC DD NN NN NN NN FF 44
TT DB BB BB SS CC CC DD NN NN NN NN FF 44
TT DB BB BB SS CC CC DD NN NN NN NN FF 44
TT DDDDDDBB SSSSSSSS CCCCCCCC DDDDDD NN NN NN FF 44
TT DDDDDDBB SSSSSSSS CCCCCCCC DDDDDD NN NN NN FF 44

DDDDDDDD AAAAAA
DDDDDDDD AAAAAA
DD AA AA
DD AA AA
DD AA AA
DD AA AA
DD AA AA
DD AA AA
DD AAAAAAAA
DD AAAAAAAA
DD AA AA
DD AA AA
DDDDDDDD AA AA
DDDDDDDD AA AA

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RRRR TTTTT AAA CCCC
R R T A A C
R R T A A C
RRRR T A A C
R R T A A A C
R R T A A C

VAX/VMI RTAC
VAX/VMS RTAC
VAX/VMS RTAC

TBSCDNF4 30-APR-1985 12:54
TBSCDNF4 30-APR-1985 12:54
TBSCDNF4 30-APR-1985 12:54

LPB0: 30-APR-1985 12:55
LPB0: 30-APR-1985 12:55
LPB0: 30-APR-1985 12:55

TBSCONF4.DAT:1
TBSCONF4.DAT:1
TBSCONF4.DAT:1

VAX/V
VAX/V
VAX/V

09:55 APR 22 '85 TRSCUHF 4.FBBELGIP

0.1
M
Y
N

N	
Y	
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05	
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1111	
15500.	
64500.	
214217.	
4202900.	
48.	
48.	
60.76	
83.24	
227.72	
204.2	
14.35	
40.	
36.	
36.	
48.	
34.83	
78.43	
0.0	
.06	
0.0	
0.0	
37.	
8.	
30.	
800.	
620.	
620.	
Y	
0.9	
0.0	
0.0	
0.	
02	
0.0,0.0,0.0,0.0,0.0,0.0,	
5.0,0.0,0.0,0.0,0.0,0.0,	
02	
0.0,0.0	
.5,2.5	
N	
N	
N	
Y	
0.0	
N	
N	
N	
N	
N	
N	
N	
06	
04,08,03,07,05,21	
0.2	

100 05-AXLE TRACTOR-SEMITRAILER (CONF 3 & 4)
 200 15500 , 64300
 300 214217 , 4202703
 400 60.76, 59.24, 107.24, 180.28, 220.28, 0., 0., 0., 0., 0., 0., 0., 0.
 500 68.89, 527.723
 600 1600 , 2480. , 2400 , 2480. , 2480. , 0.
 700 0., 0. , 0., 0. , 0.
 800 52.5, 1, 10., 1. 05
 900 267 , 400 , 400 , 400. , 400. , 0.
 1000 0., 0. , 0., 0. , 0.
 1100 28000. , 28000. , 20000 , 28000. , 0. , 0.
 1200 0., 0. , 0., 0.
 1300 13 , 13. , 13 , 13 , 0. , 0. , 0. , 0. , 0. , 0. , 0. , 0.
 1400 8. , 1001. , 1
 1500 03
 1600 0., 0.
 1700 5, 2. 6
 1800 10. , 2. 6

APPENDIX E

Vehicle Configuration 5

Input Data Files

VAX/VMS RTAC
VAX/VMS RTAC
VAX/VMS RTAC

P4CONF3 21-APR-1985 14:19 LPB0: 21-APR-1985 14:19
P4CONF5 21-APR-1985 14:19 LPB0: 21-APR-1985 14:19
P4CONF9 21-APR-1985 14:19 LPB0: 21-APR-1985 14:19

DISK\$VAXUSER1: (USER1, RTACJP4CONF3, DAT, 1
DISK\$VAXUSER1: (USER1, RTACJP4CONF5, DAT, 1
DISK\$VAXUSER1: (USER1, RTACJP4CONF9, DAT, 1

RRRR TTTT AAA CCCC
R R T A A C
R R T A A C
RRRR T A A C
R R T A A A A C
R R T A A C
R R T A A CCCC

PPPPPP 44 44 CCCCCC 000000 NN FFFFFFFF 5555555555
PPPPPP 44 44 CCCCCC 000000 NN FFFFFFFF 5555555555
PP 44 44 CC 00 00 NN FF 55
PP 44 44 CC 00 00 NN FF 55
PP 44 44 CC 00 00 NN FF 555555
PP 44 44 CC 00 00 NN FF 555555
PPPPPP 4444444444 CC 00 00 NN NN FFFFFFFF 55
PPPPPP 4444444444 CC 00 00 NN NN FFFFFFFF 55
PP 44 44 CC 00 00 NN NN NN NN FF 55
PP 44 44 CC 00 00 NN NN NN NN FF 55
PP 44 44 CC 00 00 NN NN NN NN FF 55
PP 44 44 CCCCCC 000000 NN NN FF 555555
PP 44 44 CCCCCC 000000 NN NN FF 555555

DDDDDD 444444 TTTTTTTT 1111 11
DDDDDD 444444 TTTTTTTT 1111 11
DD DD AA AA TT 1111 1111
DD DD AA AA TT 1111 1111
DD DD AA AA TT 11 11
DD DD AA AA TT 1111 11
DD DD AA AA TT 1111 11
DD DD AA AA TT 1111 11
DD DD AA AA TT 11 11
DD DD AA AA TT 11 11
DDDDDD 444444 TTTTTTTT 111111
DDDDDD 444444 TTTTTTTT 111111

RRRR TTTT AAA CCCC
R R T A A C
R R T A A C
RRRR T A A C
R R T A A A A C
R R T A A C
R R T A A CCCC

VAX/VMS RTAC
VAX/VMS RTAC
VAX/VMS RTAC

P4CONF3 21-APR-1985 14:19 LPB0: 21-APR-1985 14:19
P4CONF5 21-APR-1985 14:19 LPB0: 21-APR-1985 14:19
P4CONF9 21-APR-1985 14:19 LPB0: 21-APR-1985 14:19

DISK\$VAXUSER1: (USER1, RTACJP4CONF3, DAT, 1
DISK\$VAXUSER1: (USER1, RTACJP4CONF5, DAT, 1
DISK\$VAXUSER1: (USER1, RTACJP4CONF9, DAT, 1

100	5-AXLE TRACTOR-SEMITRAILER (CONF. 5 1	12000	18900	23000	25000	5625.1.1
200	01 6700 12.1.1.033	12900 0.	19000 13.	23100 13.	25100 13.	10125.1.1
300	53.5 6800 06	13100 0	19100 -1	23200 -2	25200 0.0	15187.1.2
400	003 6900 0.0	13200 12.	19200 0.0	23300 0.0	25300 0.0	20312.1.2
500	0 0. 7000 1.1.143	13300 16.	19300 12.	23400 1200.	25400 1200.	45000.1.3
600	0 5.1.5.1.5	13400 1.1.1.1.1.1.	19400 1.1.1.1.1.1.	23500 4500.	25500 4500.	0.0
700	10.1.1.5.1.5	13500 1.1.1.1.1.1.	19500 1.1.1.1.1.1.	23600 19.5	25600 19.5	0.0
800	04 7300 6.1.501	13600 75.75.75.95.1.	19600 75.75.75.95.1.	23700 115	25700 115	23000 4100.
900	0 0. 7400 12.1.683	13700 5.5.6.9.95	19700 5.5.6.9.95	23800 13.	25800 13.	29.29.
1000	2.5.0. 7500 06	13800 4.1.45.85.95	19800 4.1.45.85.95	23900 -1.	25900 -1.	26000 0.
1100	2 6.0. 7600 0.0	13900 0.0	19900 0.0	24000 -2	26000 -2	26100 0.0
1200	10.0. 7700 1.1.107	14000 -1600.	20000 -1600.	24100 0.	26100 0.	26200 38.
1300	0. 7800 2.1.194	14100 0.0.5.0.0.0.0.	20100 0.0.5.0.0.0.0.	24200 1200.	26200 1200.	26300 72
1400	0.1 7900 4.1.380	14200 4500.	20200 4500.	24300 4500.	26300 4500.	1500.
1500	00 8000 6.1.318	14300 19.5	20300 19.5	24400 19.5	26400 19.5	-122.
1600	11100000	14400 103	20400 103	24500 115	26500 115	0.
1700	144. 8200 03	14500 01	20500 01	24600 0.05	26600 0.05	0.
1800	0960. 8300 0.	14600 48.	20600 48.	24700 0.25	26700 0.25	4100.
1900	6540. 8400 .04	14700 50.	20700 50.	24800 1000.	26800 1000.	29.
2000	44. 8500 .1	14800 0.0	20800 0.0	24900 0	26900 0	27000 0.
2100	15000. 8600 .3	14900 -121.	20900 -121.	25000 0	27000 0	37100 0.
2200	75000. 8700 1.	15000 09	21000 09	25100 0.075	27100 0.075	38.
2300	75000. 8800 05	15100 -20000.1.11.	21100 -20000.1.11.	25200 0.25	27200 0.25	72
2400	0 0 8900 0.	15200 0.1.1	21200 0.1.1	25300 1500.	27300 1500.	1500.
2500	0. 9000 4.	15300 0.0	21300 0.0	25400 0.075	27400 0.075	13.
2600	40.0 9100 8.	15400 4000.1.1	21400 4000.1.1	25500 0.25	27500 0.25	-1.
2700	50000. 9200 12.	15500 6500.1.5	21500 6500.1.5	25600 432	27600 432	-2.
2800	36. 9300 16.	15600 9500.2.	21600 9500.2.	25700 1900.	27700 1900.	27800 0.
2900	-119. 9400 1.1.1.9.3.1	15700 13000.2.5	21700 13000.2.5	25800 4500.	27800 4500.	1200.
3000	04 9500 1.1.1.9.3.1	15800 17000.3	21800 17000.3	25900 7900.	27900 7900.	4500.
3100	-20000.1.20. 9600 1.1.1.9.35.13	15900 50000.4.0	21900 50000.4.0	26000 60.0	28000 60.0	19.5
3200	0.0. 9700 1.1.1.9.42.17	16000 0.02	22000 0.02	26100 60000.	28100 60000.	115.
3300	9250.7.2 9800 1.1.1.9.48.22	16100 -25000.1.11.	22100 -25000.1.11.	26200 790000.	28200 790000.	13.
3400	25000.17.5 9900 0.	16200 0.1.8	22200 0.1.8	26300 0.	28300 0.	-1.
3500	0.08 10100 3000.6000.9000.	16300 0.0.2	22300 0.0.2	26400 0.	28400 0.	-2.
3600	-20000.1.20. 10200 01	16400 3000.1.1	22400 3000.1.1	26500 213.94	28500 213.94	0.
3700	0.0. 10300 66.	16500 5000.1.5	22500 5000.1.5	26600 85.0	28600 85.0	1200.
3800	8040.7.2 10400 05	16600 8000.2	22600 8000.2	26700 132000.	28700 132000.	4500.
3900	25000.17.5 10500 0.0.	16700 11500.2.5	22700 11500.2.5	26800 19.5	28800 19.5	115.
4000	0.08 10600 1.1.68	16800 13500.3	22800 13500.3	26900 3100000.	28900 3100000.	0.175
4100	0. 10700 2.80	16900 40000.4	22900 40000.4	23000 01	29000 01	.25
4200	0. 10800 3.77	17000 0.02	23000 0.02	29100 48.0	29200 48.0	1500.
4300	3719. 10900 1.0.55	17100 0.0	23100 0.0	29300 50.	29300 50.	0.175
4400	23. 11000 03	17200 0.0	23200 0.0	29400 0.0	29400 0.0	.25
4500	0.0 11100 0.0.	17300 4450.	23300 4450.	29500 1500.	29500 1500.	1500.
4600	0.0 11200 1.1.59	17400 29.	23400 29.	29600 -122.	29600 -122.	-1
4700	32. 11300 2.75	17500 0.0	23500 0.0	29700 -30000.1.11.	29700 -30000.1.11.	00
4800	80.0 11400 3.73	17600 0.0	23600 0.0	29800 0.0.	29800 0.0.	3375.0.5
4900	1200. 11500 1.1.50	17700 38.	23700 38.	29900 7312.1.	29900 7312.1.	11812.1.5
5000	0.0 11600 03	17800 72.	23800 72.	24000 16875.2.	24000 16875.2.	22500.2.5
5100	-1. 11700 0.0.	17900 2300.	23900 2300.	24100 36230.3.	24100 36230.3.	0.02
5200	03 11800 1.1.44	18000 -121	24000 -121	24200 0.02	24200 0.02	-35000.1.11.
5300	3000.6000.9000. 11900 2.70	18100 0	24100 0	24300 0.1.3	24300 0.1.3	0.0.2
5400	01 12000 3.69	18200 0	24200 0	24400 1687.0.5	24400 1687.0.5	1687.0.5
5500	66. 12100 1.1.45	18300 4436	24300 4436	24500 0.	24500 0.	0.0.2
5600	0.0. 12200 03	18400 27.	24400 27.	24600 78000.	24600 78000.	0.0.2
5700	03 12300 0.	18500 0.	24500 0.	24700 0.1.3	24700 0.1.3	0.0.2
5800	1.1.183 12400 .04	18600 38	24600 38	24800 1687.0.5	24800 1687.0.5	1687.0.5
5900	2.1.333 12500 .1	18700 72.	24700 72.	24900 0.0.2	24900 0.0.2	0.0.2
6000	4.1.575 12600 .3	18800 72.	24800 72.	24900 1687.0.5	24900 1687.0.5	1687.0.5
6100	06 12700 1.					

VAX/VMS
 VAX/VMS
 VAX/VMS

DISK4VAXUSER1 : (USER1. RTACJYRCONF1. DAT1.)
 DISK4VAXUSER1 : (USER1. RTACJYRCONF1. DAT1.)
 DISK4VAXUSER1 : (USER1. RTACJYRCONF1. DAT1.)

LPD0. 21-APR-1985 11:39
 LPD0. 21-APR-1985 11:39
 LPB0 21-APR-1985 11:39

YRCONF1 21-APR-1985 11:39
 YRCONF1 21-APR-1985 11:39
 YRCONF1 21-APR-1985 11:39

RTAC
 RTAC
 RTAC

RRRR TTTT AAA CCCC
 R R T A A C
 R R T A A C
 RRRR T A A C
 R R T AAAAA C
 R R T A A C
 R R T A A CCCC

YY	RRRRRRR	CCCCCCC	DDDDDD	NN	FFFFFFFFF
YY	RRRRRRR	CCCCCCC	DDDDDD	NN	FFFFFFFFF
YY	RR	CC	DD	NN	FF
YY	RR	CC	DD	NN	FF
YY	RR	CC	DD	NN	FF
YY	RR	CC	DD	NN	FF
YY	RR	CC	DD	NN	FF
YY	RRRRRRR	CCCCCCC	DDDDDD	NN	FFFFFFFFF
YY	RRRRRRR	CCCCCCC	DDDDDD	NN	FFFFFFFFF
YY	RR	CC	DD	NN	FF
YY	RR	CC	DD	NN	FF
YY	RR	CC	DD	NN	FF
YY	RR	CC	DD	NN	FF
YY	RR	CC	DD	NN	FF
YY	RR	CC	DD	NN	FF
YY	RR	CC	DDDDDD	NN	FF
YY	RR	CC	DDDDDD	NN	FF

DDDDDDDD	AAAAA	TTTTTTTTT	111	11
DDDDDDDD	AAAAA	TTTTTTTTT	111	11
DD	AA	TT	111	111
DD	AA	TT	111	111
DD	AA	TT	111	111
DD	AA	TT	111	111
DD	AA	TT	111	111
DD	AA	TT	111	111
DD	AA	TT	111	111
DD	AAAAA	TTTT	11	11
DD	AAAAA	TTTT	11	11
DD	AA	TT	11	11
DD	AA	TT	11	11
DD	AA	TT	11	11
DD	AA	TT	11	11
DD	AA	TT	11	11
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DD	AA	TT	11	11
DD	AA	TT	11	11
DD	AA	TT	11	11
DD	AA	TT	11	11
DD	AA	TT	11	11
DD	AA	TT	11	11

RRRR TTTT AAA CCCC
 R R T A A C
 R R T A A C
 RRRR T A A C
 R R T AAAAA C
 R R T A A C
 R R T A A CCCC

DISK4VAXUSER1 : (USER1. RTACJYRCONF1. DAT1.)
 DISK4VAXUSER1 : (USER1. RTACJYRCONF1. DAT1.)
 DISK4VAXUSER1 : (USER1. RTACJYRCONF1. DAT1.)

LPD0. 21-APR-1985 11:39
 LPD0. 21-APR-1985 11:39
 LPB0 21-APR-1985 11:39

YRCONF1 21-APR-1985 11:39
 YRCONF1 21-APR-1985 11:39
 YRCONF1 21-APR-1985 11:39

RTAC
 RTAC
 RTAC

VAX/VMS
 VAX/VMS
 VAX/VMS

5-AXLE TRACOR-SEMITRAILER (CONF 5)

100	0205	0102020202	6300
200	52.3.8.1.1.02	0407	6400
300	0302	0.0.1.0.3.0.4.0.5.0.7.0.10.0	6500
400	7700.61500	3000.55.92.100.120.125.100	6600
500	15000.204440	6000.130.261.300.354.373.332	6700
600	75000.3012573	9000.200.432.333.625.630.365	6800
700	75000.3950083	0405	6900
800	44.81.3	0.1.1.2.3.4	7000
900	8960.18320.18320.17000.17000.	3000.29.42.44.30.	7100
1000	1500.2300.2300.1500.1500.	6000.92.150.157.146	7200
1100	3719.4438.4438.4100.4100.	9000.152.269.329.335.	7300
1200	26.8.91.2.139.2.190.2.-238.2	1	7400
1300	19.5.19.5.19.5.19.5.19.5	7600.003	7500
1400	23.29.29.29.29	7700.0.0.0.	7600
1500	16.19.19.19.19.	7800.0.5.175.175	7700
1600	40.29.5.29.5.29.5.29.5	7900.10.1.75.1.75	7800
1700	0.13.13.13.13		7900
1800	0.13.13.13.13		
1900	4500.4500.4500.4500.4500.4500.		
2000	0.0.0.0.0.		
2100	0.0.78000.0.0.		
2200	300.1000.1000.1000.1000.1000		
2300	0.0.0.0.0.		
2400	-115.2.217.8		
2500	48		
2600	2400.1000000.		
2700	01		
2800	03		
2900	0102020303		
3000	04		
3100	-30000.-20		
3200	0.0		
3300	0645.7.2		
3400	23000.7.5		
3500	09		
3600	-22200.-11.		
3700	0.-1		
3800	0.0.		
3900	3300.1.		
4000	5750.1.5		
4100	8750.2		
4200	12250.2.5		
4300	16250.3		
4400	43000.4.		
4500	09		
4600	-32500.-11.		
4700	0.-1.5		
4800	0.0		
4900	2531.0.5		
5000	6469.1		
5100	10969.1.5		
5200	-16031.-2.		
5300	21656.2.5		
5400	50625.3.		
5500	01		
5600	0101010101		
5700	0405		
5800	0.1.0.2.0.4.0.6.0.12.0		
5900	3000.540.990.1710.2130.2490.		
6000	4600.860.1500.2760.3400.4140.		
6100	8000.1990.1710.3440.4480.5210.		
6200	02		

VAX/VMS RTAC
 VAX/VMS RTAC
 VAX/VMS RTAC

TBSCONF5 21-APR-1985 15:25
 TBSCONF5 21-APR-1985 15:25
 TBSCONF5 21-APR-1985 15:25

LPBO: 21-APR-1985 15:28
 LPBO: 21-APR-1985 15:28
 LPBO: 21-APR-1985 15:28

TBSCONF5.DAT:1
 TBSCONF5.DAT:1
 TBSCONF5.DAT:1

VAX/
 VAX/
 VAX/

RRRR TTTT AAA CCCC
 R R T A A C
 R R T A A C
 RRRR T A A C
 R R T A A A A C
 R R T A A C
 R R T A A C

TTTTTTTTT	DDDDDDDD	SSSSSSSS	CCCCCCCC	DDDDDD	NN	FFFFFFFFF	SSSSSSSSS
TTTTTTTTT	DDDDDDDD	SSSSSSSS	CCCCCCCC	DDDDDD	NN	FFFFFFFFF	SSSSSSSSS
TT	DD	SS	CC	DD	NN	FF	SS
TT	DD	SS	CC	DD	NN	FF	SS
TT	DD	SS	CC	DD	NNNN	NN	SSSSSS
TT	DD	SS	CC	DD	NNNN	NN	SSSSSS
TT	DD	SSSSSS	CCCC	DD	NN	NN	SS
TT	DD	SSSSSS	CCCC	DD	NN	NN	SS
TT	DD	SS	CC	DD	NNNN	NN	SS
TT	DD	SS	CC	DD	NN	NN	SS
TT	DD	SS	CC	DD	NN	NN	SS
TT	DD	SSSSSS	CCCC	DD	NN	NN	SSSSSS
TT	DD	SSSSSS	CCCC	DD	NN	NN	SSSSSS
TT	DD	SSSSSS	CCCC	DD	NN	NN	SSSSSS
TT	DD	SSSSSS	CCCC	DD	NN	NN	SSSSSS

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DDDDDDDD	AAAAAA	TTTTTTTTT	SS
DD	AA	TT	SS
DD	AA	TT	SS
DD	AA	TT	SS
DD	AA	TT	SS
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DD	AA	TT	SS
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DD	AA	TT	SS
DD	AA	TT	SS
DD	AA	TT	SS
DD	AA	TT	SS
DD	AA	TT	SS
DD	AA	TT	SS

RRRR TTTT AAA CCCC
 R R T A A C
 R R T A A C
 RRRR T A A C
 R R T A A A A C
 R R T A A C
 R R T A A C

VAX/VMS RTAC
 VAX/VMS RTAC
 VAX/VMS RTAC

TBSCONF5 21-APR-1985 15:25
 TBSCONF5 21-APR-1985 15:25
 TBSCONF5 21-APR-1985 15:25

LPBO: 21-APR-1985 15:28
 LPBO: 21-APR-1985 15:28
 LPBO: 21-APR-1985 15:28

TBSCONF5.DAT:1
 TBSCONF5.DAT:1
 TBSCONF5.DAT:1

VAX/
 VAX/
 VAX/

09:55 APR 22 '85 TBSCONF5.F08ELOCJP

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15500.	
64500.	
214217.	
4202900.	
48.	
48.	
60.76	
83.24	
227.72	
204.2	
0.0	
40.	
36.	
36.	
48.	
34.83	
78.43	
0.0	
.06	
0.0	
0.0	
35.85	
8.	
30.	
700.	
720.	
620.	
Y	
0.9	
0.0	
0.0	
0.	
02	
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5.0,0.0,0.0,0.0,0.0.	
02	
0.0,0.0	
.51.5	
N	
N	
N	
Y	
0.0	
N	
N	
N	
N	
N	
N	
06	
04,08,03,07,05,21	
0.2	

0.1
N
Y
N

VAX/VMS RTAC RTAC LPDO: 21-APR-1985 14:18 VAX.
VAX/VMS RTAC LYPDNF5 21-APR-1985 14:18 DISK#VAXUSER1:[USER1.RTAC]LYPCDNF5.DAT;1 VAX.
VAX/VMS RTAC LYPDNF5 21-APR-1985 14:18 LPBO: 21-APR-1985 14:18 DISK#VAXUSER1:[USER1.RTAC]LYPCDNF5.DAT;1 VAX.
VAX/VMS RTAC LYPDNF5 21-APR-1985 14:18 LPBO: 21-APR-1985 14:18 DISK#VAXUSER1:[USER1.RTAC]LYPCDNF5.DAT;1 VAX.

RRRR TTTT AAA CCCC
R R T A A C
R R T A A C
RRR T A A C
R R T A A A C
R R T A A C
R T A A C C C C

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LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5
LL YY P P P P P P P P C C C C C C C C NN NN F F F F F F F F F 5 5 5 5 5 5 5 5

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DDDDDDDD AAAAAA TTTTTTTT 1111 11
DD AA AA AA AA TTTT 1111 11
DD AA AA AA AA TTTT 1111 11
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DD AAAAAAAAAA TTTT 1111 11
DD AAAAAAAAAA TTTT 1111 11
DD AA AA AA AA TTTT 11 11
DD AA AA AA AA TTTT 11 11
DDAAADDD AA AA AA AA TTTT 11 11 11 11
DDDDDDDD AA AA AA AA TTTT 11 11 11 11

```

RRRR TTTT AAA CCCC
R R T A A C
R R T A A C
RRR T A A C
R R T A A A C
R R T A A C
R T A A C C C C

VAX/VMS RTAC RTAC LPDO: 21-APR-1985 14:18 VAX.
VAX/VMS RTAC LYPDNF5 21-APR-1985 14:18 DISK#VAXUSER1:[USER1.RTAC]LYPCDNF5.DAT;1 VAX.
VAX/VMS RTAC LYPDNF5 21-APR-1985 14:18 LPBO: 21-APR-1985 14:18 DISK#VAXUSER1:[USER1.RTAC]LYPCDNF5.DAT;1 VAX.
VAX/VMS RTAC LYPDNF5 21-APR-1985 14:18 LPBO: 21-APR-1985 14:18 DISK#VAXUSER1:[USER1.RTAC]LYPCDNF5.DAT;1 VAX.

	65-AXLE TRACTOR-SEMITRAILER (CONF. 5)
100	15500 .64500
200	214217 .4202700
300	60 76.59 24.107 24.100 28.228 20.0 0.0 0.0 0.0
400	03.241.277.773
500	1400 .2880 .2800 .2480 .2400
600	0 .0 .0 .0 .0
700	52.5 .1 .10 .1 .05
800	240 .420 .420 .400 .400
900	0 .0 .0 .0 .0
1000	20000 .28000 .28000 .28000 .0 .0
1100	0 .0 .0 .0 .0
1200	13 .13 .13 .13 0 .0 .0 .0 .0 .0
1300	8 .001 .1
1400	03
1500	0 .0
1600	5 .5
1700	10 .5
1800	

APPENDIX F

Vehicle Configuration 6

Input Data Files

VAX/
VAX/
VAX/

DISK1\$VAXUSER1:USER1 RTACJP4CONF.6.DAT:1
DISK1\$VAXUSER1:USER1 RTACJP4CONF.6.DAT:1
DISK1\$VAXUSER1:USER1 RTACJP4CONF.6.DAT:1

30-APR-1985 12:53 LPB0: 30-APR-1985 12:53
30-APR-1985 12:53 LPB0: 30-APR-1985 12:53
30-APR-1985 12:53 LPB0: 30-APR-1985 12:53

VAX/VMS RTAC
VAX/VMS RTAC
VAX/VMS RTAC

RRRR TTTT AAA CCCC
R R T A A C
R R T A A C
RRRR T A A C
R R T A A A A C
R R T A A C
R R T A A C C C C C

PPPPPPP 44 44 CCCCCCCC DDDDD NN FFFFFFFF 666666
PPPPPPP 44 44 CCCCCCCC DDDDD NN FFFFFFFF 666666
PP 44 44 CC DD DD NN NN FF 66
PP 44 44 CC DD DD NN NN FF 66
PP 44 44 CC DD DD NN NN FF 66
PP 44 44 CC DD DD NN NN FF 66
PPPPPPP 4444444444 CC DD DD NN NN FFFFFFFF 66666666
PPPPPPP 4444444444 CC DD DD NN NN FFFFFFFF 66666666
PP 44 44 CC DD DD NN NN NN NN FF 66
PP 44 44 CC DD DD NN NN NN NN FF 66
PP 44 44 CC DD DD NN NN NN NN FF 66
PP 44 44 CC DD DD NN NN NN NN FF 66
PP 44 44 CCCCCCCC DDDDD NN NN FF 666666
PP 44 44 CCCCCCCC DDDDD NN NN FF 666666

DDDDDDDD AAAAA YTTTTTTT 11 11
DDDDDDDD AAAAA YTTTTTTT 11 11
DD DD AA TT TTTT 1111 1111
DD DD AA TT TTTT 11 11
DD DD AA TT TTTT 11 11
DD DD AA TT TTTT 11 11
DD DD AAAAAAAA TT TTTT 11 11
DD DD AAAAAAAA TT TTTT 11 11
DD DD AA TT TTTT 11 11
DD DD AA TT TTTT 11 11
DDDDDDDD AA AA TT TTTT 111111
DDDDDDDD AA AA TT TTTT 111111

RRRR TTTT AAA CCCC
R R T A A C
R R T A A C
RRRR T A A C
R R T A A A A C
R R T A A C C C C C

DISK1\$VAXUSER1:USER1 RTACJP4CONF.6.DAT:1
DISK1\$VAXUSER1:USER1 RTACJP4CONF.6.DAT:1
DISK1\$VAXUSER1:USER1 RTACJP4CONF.6.DAT:1

30-APR-1985 12:53 LPB0: 30-APR-1985 12:53
30-APR-1985 12:53 LPB0: 30-APR-1985 12:53
30-APR-1985 12:53 LPB0: 30-APR-1985 12:53

VAX/VMS RTAC
VAX/VMS RTAC
VAX/VMS RTAC

5-AXLE DOUBLE / 27-FT TRAILERS (CONF. 6)

100	0.0	6700	12.3.833	12800	05	18900	0
200	33.5	6800	06	12900	0	19000	0.075
300	003	6900	0.0	13000	4	19100	0.25
400	0.0	7000	1.1.143	13100	6	19200	1500
500	0.5.4.5.4.5	7100	2.1.252	13200	12	19300	252
600	10.4.5.4.5	7200	4.1.458	13300	16	19400	2250
700	0.0	7300	6.1.581	13400	1.1.1.1.1.1.1	19500	3750
800	0.0	7400	12.1.693	13500	1.1.1.1.1.1.1	19600	60.0
900	2.5.0	7500	06	13600	.75.75.75.95.1	19700	30000
1000	2.6.0	7600	1.1.107	13700	.5.5.6.9.95	19800	93750
1100	0.0	7700	2.1.194	13800	.4.4.43.85.95	19900	93750
1200	10.0	7800	4.1.380	13900	0.0	20000	25800
1300	8	7900	12.1.685	14000	-1600	20100	117.7
1400	0.1	8000	6.1.518	14100	0.0.5.0.0.6	20200	89.0
1500	00	8100	12.1.685	14200	4500	20300	65000
1600	11100000	8200	05	14300	19.5	20400	375000
1700	120	8300	0	14400	103	20500	375000
1800	8960	8400	.04	14500	00	20600	36
1900	4240	8500	.1	14600	-151	20700	44
2000	44	8600	.5	14700	09	20800	00
2100	15000	8700	1	14800	-26600.11	20900	-132
2200	75000	8800	05	14900	0.1.1	21000	09
2300	75000	8900	0	15000	0.0	21100	-37000.11
2400	0.0	9000	4	15100	5300.1	21200	0.1.5
2500	6.73	9100	8	15200	8650.1.5	21300	0.0
2600	48.0	9200	12	15300	12650.2	21400	3750.0.5
2700	20000	9300	16	15400	17300.2.5	21500	8125.1
2800	36	9400	1.1.1.9.3.1	15500	22600.3	21600	13100.1.5
2900	-119	9500	1.1.1.9.3.1	15600	66000.4.0	21700	18750.2.5
3000	04	9600	1.1.1.9.35.13	15700	0.02	21800	25000.2.5
3100	-20000.20	9700	1.1.1.9.42.17	15800	-33000.11	21900	62000.3
3200	9250.7.2	9800	1.1.1.9.48.22	15900	0.1.2	22000	0.02
3300	25000.7.5	9900	-2	16000	0.1.2	22100	-44000.11
3400	0.00	10000	03	16100	4000.1	22200	0.1.3
3500	-20000.20	10100	3000.6000.9000	16200	4650.1.5	22300	0.0.2
3600	0.0	10200	01	16300	10650.2	22400	1875.0.3
3700	0.0	10300	64	16400	13300.2.5	22500	6250.1
3800	8040.7.2	10400	03	16500	20600.3	22600	11250.1.5
3900	25000.7.5	10500	0.0	16600	53000.4	22700	16875.2.5
4000	0.08	10600	1.5.68	16700	0.02	22800	23125.2.5
4100	0	10700	.2.60	16800	0.0	22900	50000.3
4200	0	10800	.3.77	16900	0.0	23000	0.02
4300	3719	10900	1.0.55	17000	4456	23100	0.0
4400	23	11000	05	17100	29	23200	0.0
4500	0.00	11100	0.0	17200	0.0	23300	4100
4600	1500	11200	1.59	17300	8000	23400	29
4700	32	11300	.2.75	17400	38	23500	0
4800	80.0	11400	.3.73	17500	72	23600	10000
4900	1200	11500	1.1.50	17600	2300	23700	38
5000	0.0	11600	05	17700	13	23800	72
5100	-1	11700	0.0	17800	-1	23900	1500
5200	0.00	11800	1.1.44	17900	-2	24000	13
5300	3000.6000.9000	11900	.2.70	18000	0.0	24100	-1
5400	01	12000	.3.69	18100	1200	24200	-2
5500	64	12100	1.1.45	18200	4300	24300	0
5600	0.0	12200	05	18300	19.5	24400	1200
5700	0.0	12300	0	18400	115	24500	4300
5800	1.1.103	12400	.04	18500	0.05	24600	19.5
5900	2.1.333	12500	.1	18600	0.25	24700	115
6000	4.1.575	12600	.5	18700	1000	24800	0.175
6100	6.1.708	12700	1	18800	0	24900	.25

1500.
31100 1500.
31200 -1
31300 00

25000 1500.
25100 01
25200 80.
25300 0.
25400 48.
25500 252.
25600 4250.
25700 4250.
25800 60.0
25900 36000.
26000 115000.
26100 115000.
26200 26500.
26300 126.
26400 85.0
26500 65000.
26600 375000.
26700 375000.
26800 00
26900 -132.
27000 0.0
27100 0.0
27200 4100.
27300 29.
27400 0.
27500 10000.
27600 38.
27700 72.
27800 1500.
27900 13.
28000 -1.
28100 -2.
28200 0.
28300 1200.
28400 4500.
28500 19.5
28600 113.
28700 00
28800 -132.
28900 0.0
29000 0.0
29100 4100.
29200 29.
29300 0.
29400 10000.
29500 38.
29600 72.
29700 1500.
29800 13.
29900 -1.
30000 -2.
30100 0.
30200 1200.
30300 4500.
30400 19.5
30500 115.
30600 0.223
30700 .25
30800 1500.
30900 0.273
31000 .25

5-AXLE DOUBLE / 27-FT TRAILERS (CONF. 6)

Item No.	Description	Price	Code	Notes	
100	10000.17500.17500.17500.17500.				
200	1200.2300.1500.1500.1500.				
300	3719.4458.4100.4100.4100.				
400	24.96.119.0.126.				
500	19.5.19.5.19.5.19.5.				
600	16.19.19.19.19.				
700	40.29.5.29.5.29.5.				
800	0.13.13.13.13.				
900	0.0.0.0.0.				
1000	1500.8000.10000.10000.10000.				
1100	300.1000.1000.1000.1000.				
1200	0.0.0.0.0.				
1300	87.27.133.07.154.93.80.0.126.				
1400	48.44.48				
1500	1000000.0.1000000.				
1600	010304				
1700	03				
1800	0102030303				
1900	04				
2000	20000.20.				
2100	0.0.				
2200	8645.7.2				
2300	25000.7.5				
2400	07				
2500	29000.11.				
2600	0.1.				
2700	0.0.				
2800	4650.1.				
2900	7650.1.5				
3000	11650.2.				
3100	16300.2.5				
3200	21600.3				
3300	4400.59500.4.				
3400	07				
3500	40500.11.				
3600	0.1.5				
3700	0.0.				
3800	2812.0.5				
3900	7100.1.				
4000	12175.1.5				
4100	17913.2				
4200	24043.2.5				
4300	56000.3.				
4400	01				
4500	0101010101				
4600	0406				
4700	0.1.0.2.0.4.0.6.0.12.0				
4800	3090.540.990.1710.2130.2490.				
4900	6000.840.1500.2760.3480.4140.				
5000	9000.990.1710.3420.4680.6210.				
5100					
5200					
5300					
5400					
5500					
5600					
5700					
5800					
5900					
6000					
6100					
6200					
6300					
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7200					
7300					
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9100					
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9300					
9400					
9500					
9600					
9700					
9800					
9900					

100	3-AXLE DOUBLE / 27-FT TRAILER (CONF. 6)
200	13200.,47800.,2300.,32500.
300	132646.64,525908.56,2560.,621588.25
400	38.545,81.435,0.,113.323,0.,0.
500	0.,0.,126.,0.,0.
600	72.725,138.677,149.323,80.,0.,.126.
700	1500.,2800.,0.,2800.,0.,0.
800	2800.,0.,2800.,0.,0.
900	31.5,0.1,10.,1.05
1000	266.7,400.,0.,400.,0.,0.
1100	400.,0.,400.,0.,0.
1200	28000.,0.,28000.,0.,0.,28000.
1300	0.,28000.,0.,0.
1400	13.,0.,13.,0.,0.,13.,0.,13.,0.,0.
1500	8.,001.,1
1600	03
1700	0.,0.
1800	.5,2.
1900	10.,2.

APPENDIX G

Basic Parameters of a 5-axle, Dirt Truck

WU1	=	1500	(lb)	Weight of first unsprung mass
WU2	=	3000	(lb)	Weight of second unsprung mass
WU3	=	4000	(lb)	Weight of third unsprung mass
WAX1	=	18,000	(lb)	Vertical load on the first axle
WAX2	=	26,000	(lb)	Vertical load on the second axle
WAX3	=	26,000	(lb)	Vertical load on the third axle
T1	=	40.25	(in.)	Half track width of the inner tires on the first axle
T2	=	29	(in.)	Half track width of the inner tires on the second axle
T3	=	29	(in.)	Half track width of the inner tires on the third axle
A1	=	0	(in.)	Dual tire spacing on the first axle
A2	=	13	(in.)	Dual tire spacing on the second axle
A3	=	13	(in.)	Dual tire spacing on the third axle
S1	=	16	(in.)	Half spring spacing at the first axle
S2	=	19	(in.)	Half spring spacing at the second axle
S3	=	19	(in.)	Half spring spacing at the third axle
ZS1	=	44	(in.)	Height of c.g. of the first sprung mass, above ground level
ZS2	=	44	(in.)	Height of c.g. of the second sprung mass, above ground level
ZS3	=	84.6	(in.)	Height of c.g. of the third sprung mass, above ground level
R1	=	21	(in.)	Rolling radius of tires on the first axle
R2	=	20	(in.)	Rolling radius of tires on the second axle
R3	=	20	(in.)	Rolling radius of tires on the third axle
HR1	=	22	(in.)	Height of roll centre of the first suspension above ground level
HR2	=	29	(in.)	Height of roll centre of the second suspension above ground level
HR3	=	29	(in.)	Height of roll centre of the third suspension above ground level

ZS	=	48	(in.)	Height of the fifth wheel centre above ground level
MFR	=	40,000	(lb/deg.)	Tractor Frame torsional stiffness
ZFR	=	34	(in.)	Tractor frame torsional axis height above ground level
KT11	=	8000	(lb/in.)	Vertical stiffness of tires per side on the first axle
KT21	=	10,000	(lb/in.)	Vertical stiffness of tires per side on the second axle
KT31	=	10,000	(lb/in.)	Vertical stiffness of tires per side on the third axle
KRS1	=	0	(lb/in./deg.)	Auxiliary roll stiffness of the first suspension
KRS2	=	20,000	(lb/in./deg.)	Auxiliary roll stiffness of the second suspension
KRS3	=	0	(lb/in./deg.)	Auxiliary roll stiffness of the third suspension
LASH5	=	0.1	(in.)	Lash in the fifth wheel
COULFR	=	11,000	(in.lb/deg.)	Coulomb friction present in the tractor frame
M5	=	1,000,000	(in./lb/deg.)	Torsional stiffness of the fifth wheel
MOMSEP	=	900,000	(in./lb)	Roll moment that causes separation of the fifth wheel plates
WS	=	30,000	(lb)	Vertical load on the fifth wheel
WS2	=	500	(lb)	Weight of the second sprung mass
KOVT1	=	1000	(in./lb/deg.)	Overturning stiffness of the tires on the first axle
KOVT2	=	2000	(in./lb/deg.)	Overturning stiffnesses of the tires on the second axle
KOVT3	=	2000	(in./lb/deg.)	Overturning stiffnesses of the tires on the third axle

a) First Suspension Spring Table

<u>Force (lb)</u>	<u>Deflection (in.)</u>
-10,000	-5
14,250	7.13
40,000	7.25

b) Second Suspension Spring Table

<u>Force (lb)</u>	<u>Deflection (in.)</u>
-20,000	-10
20,000	10

c) Third Suspension Spring Table

<u>Force (lb)</u>	<u>Deflection (in.)</u>
-15,000	-1.75
0	-0.75
0	0
15,000	1